FIELD MANUAL NO 34-40-9 HEADQUARTERS DEPARTMENT OF THE ARMY Washington, DC, 29 August 1991

DIRECTION FINDING OPERATIONS

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PREFACE

Direction finding (DF) involves determining the direction of arrival of a radio wave. Since the conception of signals intelligence (SIGINT) gathering, direction finding has been an important part of the intelligence cycle. Direction finding is used to support other intelligence information. It is normally integrated with other sources of intelligence such as communications and noncommunications intercept to determine the approximate location, movement, and relocation of threat emitters. Direction finding bearings and locations are used in developing threat order of battle (OB) information to support national and tactical intelligence information.

This field manual provides direction finding doctrine, procedures, techniques, and theory for personnel conducting strategic and tactical operations. It is written for military intelligence (MI) organizations; supported commanders and their staffs; echelons above corps (EAC) conducting direction finding operations; strategic joint operations personnel needing direction finding information; intelligence analysts; and direction finding supervisors, operators, and analysts.

The subject area of *strategic systems* refers to DF systems at a permanently fixed or semifixed site that have long-range DF capability. The area of *tactical systems* refers to semipermanent or mobile DF systems on the battlefield. These systems have a short- to medium-range DF capability.

The words *target* or *target area* are used for the purpose of brevity. These terms are synonymous with *target transmitting antenna*. The transmitting antenna may be far removed from the actual location of the transmitter.

The proponent of this publication is Headquarters, United States Army Training and Doctrine Command (TRADOC). Send comments and recommendations on DA Form 2028 directly to the Commander, United States Army Intelligence School, Fort Devens (USAISD), ATTN: ATSI-ETD-PD, Fort Devens, Massachusetts 01433-6301.

Unless this publication states otherwise, masculine nouns and pronouns do not refer exclusively to men.

CHAPTER 1

ELEMENTS

Direction finding involves determining the direction of arrival of a radio wave. Direction finding equipment will indicate the approximate direction along an imaginary line on which a transmitting antenna lies. This is commonly referred to as a line of bearing (LOB). The information obtained by a single direction finding site is seldom accurate enough to pinpoint a location. However, the direction of a distant transmitter's antenna can be determined (depending on the training and expertise of the DF personnel and the DF equipment used) to an accuracy of plus or minus 2 degrees. With the exception of the single station locator (SSL), one DF site can only indicate the approximate direction of a transmitter's antenna (Figure 1-1).

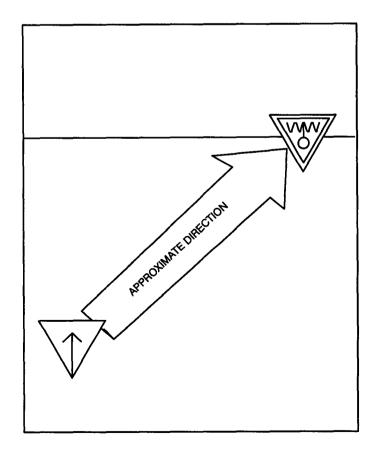


Figure 1-1. LOB of a distant transmitter's antenna.

Two DF sites, however, can indicate the general location of a transmitter's antenna by providing a *cut* (Figure 1-2).

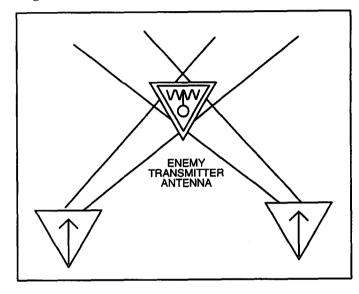


Figure 1-2. General location of a distant transmitter's antenna (cut).

Three or more DF sites can provide the fix location of a desired transmitter's antenna (Figure 1-3).

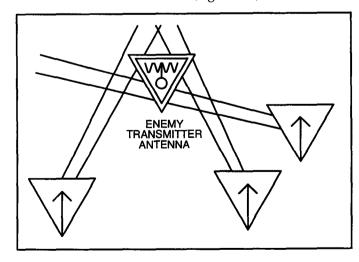


Figure 1-3. Fix location of a distant transmitter's antenna.

The theory of direction finding has remained reasonably static since the early history of the study of electromagnetic (EM) wave phenomena. Early radio communications were directional in nature. This was because the radio transmitters were relatively low powered. They were inefficient in their output, and the receivers were relatively insensitive. Efforts were undertaken to *direct* the transmitted wave toward the receiving device. This was done to ensure communications rather than to determine location. Therefore, the useful applications of DF were obtained almost simultaneously with the effort to direct the radio transmissions.

Direction finding has many uses. It can be used as a navigational aid. In this capacity, the DF equipment is either used alone or in combination with other DF systems. This depends on the service which is to be provided. Such service includes positioning, controlling, and homing of ground, sea, and air forces. DF equipment is also used by rescue personnel as an essential part of air-sea rescue. Also, crash beacons on

downed aircraft or disabled ships provide a signal which can be located (or *homed-in* on) by DF equipment.

The extensive use of military radio communications has increased the value of DF in the production of SIGINT. Even if a military force is extremely careful, radio and radar transmissions can be intercepted and the locations of the transmitter's antennas determined. Direction finding can provide enemy transmitter antenna locations to intelligence personnel for the construction of enemy order of battle and fusion into other intelligence activities. Specifically, direction finding can also be used to assist in determining—

- Enemy troops or equipment movements which may indicate a possible attack.
- Locations of transmitting antennas associated with various weapon systems (to help determine enemy capabilities).
- New, and confirming known, transmitter antenna locations.
- Possible targets for jamming or intercept.

CHAPTER 2

RADIO WAVE PROPAGATION

Radio direction finding (RDF) deals with the direction of arrival of radio waves. Therefore, it is necessary to understand the basic principles involved in the

propagation of radio waves from the transmitting station to the DF equipment.

CHARACTERISTICS

The distance between two points of corresponding phase in consecutive cycles is known as a wavelength. A wavelength can be expressed in any unit of measure. However, it is normally expressed in meters. The number of complete waves that move past a given point in one second is called frequency. A unit of frequency is called Hertz (Hz). One unit is equal to one cycle per second (Figure 2-1). The radio wave's strength or

intensity is called its amplitude. The radio wave, which is electromagnetic in nature. consists of an electrical field (E field) and a magnetic field (H field). Each field supports the other, and neither can be propagated by itself. Table 2-1, page 2-2, lists frequency bands. their designators. and the commonly accepted limits of each band.

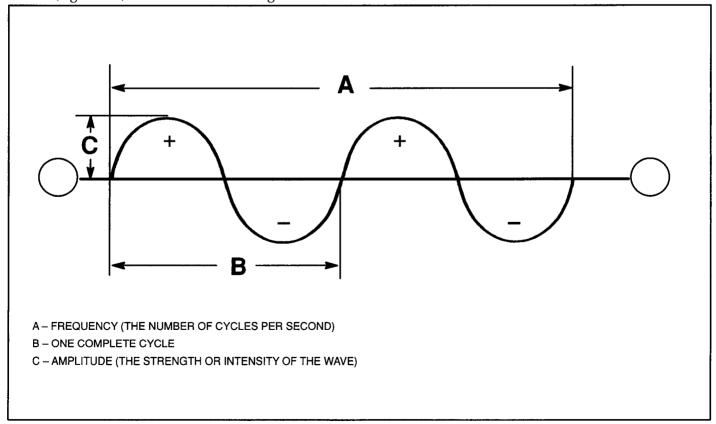


Figure 2-1. Wavelength characteristics.

| FREQUI | ENCY RANGE | BAND DESIGNATOR |
|----------|-----------------|--------------------------------|
| 3-30 | kilohertz (kHz) | very low frequency (VLF) |
| 30-300 | kHz | low frequency (LF) |
| 300-3000 | kHz | medium frequency (MF) |
| 3-30 | megahertz (MHz) | high frequency (HF) |
| 30-300 | MHz | very high frequency (VHF) |
| 300-3000 | MHz | ultra high frequency (UHF) |
| 3-30 | gigahertz (GHz) | super high frequency (SHF) |
| 30-300 | GHz | extremely high frequency (EHF) |

Table 2-1. Frequency range and band designator.

POLARIZATION

The direction of the E field of a radio wave, relative to the ground, determines the polarization of the wave. Polarization can either be horizontal, vertical, or a mutation which adopts portions of vertical and horizontal. The latter results in a circular or a hybrid form of a wave. If a whip or other vertical type transmitting antenna is used to propagate radio waves, the transmitted wave is considered to be vertically polarized. If the transmitting antenna is horizontal, relative to the earth's surface, the transmitted wave is horizontally polarized.

To illustrate vertical wave polarization, imagine a rope lying reasonably straight on the ground. One end is attached to a tree or other support (Figure 2-2). If the loose end of the rope is raised, tightened, and given a violent up and down motion, a series of undulating waves will travel along the rope. The movement of the waves will be vertical to the earth and clearly visible.

If the same rope had a similar movement applied in a horizontal manner, the waves would be in a horizontal plane. These waves would be called horizontally polarized (Figure 2-3).

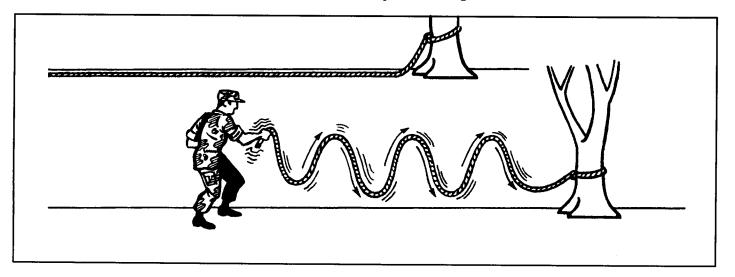


Figure 2-2. Vertical wave polarization.

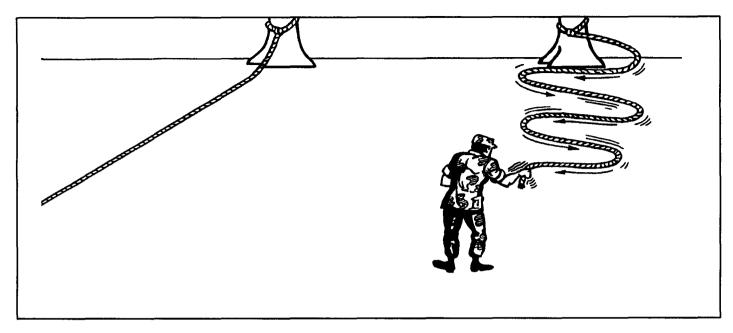


Figure 2-3. Horizontal wave polarization.

PROPAGATION FACTORS

Radio waves are electromagnetic waves which travel through space at the same speed as light. They travel approximately 186,000 miles per second or 300,000,000 meters per second. A conversion formula for wavelength and frequency is shown below. If the measurement in Hertz is known and a conversion to wavelength is desired, apply—

Wavelength (meters) = 300,000,000 Frequency (Hz)

If wavelength (in meters) is known and a conversion to frequency (Hz) is desired, apply—

Frequency (Hz) = $\frac{300,000,000}{\text{Wavelength (meters)}}$

Radio wave propagation is defined as extending or transmitting electromagnetic energy through space. Wavelength, frequency, and polarization are all essential elements of the actual wave and are factors which affect the radio wave propagation. The simplest form of propagation is through the space wave. The wave is radiated from the transmitter and continues through

space in a line of sight (LOS) fashion until it reaches the receiver. Over a flat surface there are few problems in interception or direction finding. However, we do not live on a flat surface. The curved surface of the earth, while appearing to be flat over a short distance, limits the effective LOS range.

Radio waves tend to travel in straight lines unless they are acted on by some force. They can be reflected off the surface of any sharply defined object such as the earth's surface. The radio waves can also meet other obstructions or objects that will scatter or reflect the signal. They can be reflected, refracted, or diffracted. Factors which affect radio wave propagation include—

- Wavelength.
- Polarization.
- Space (or the medium through which waves travel).
- Physical obstructions.

All of the above factors contribute to or create additional considerations. Personnel engaged in or using direction finding results must understand these factors.

Reflection

When observing oneself in a mirror, the light beams or waves reflected directly off the mirror's silver finish give the identical or mirror image, barring an optical distortion. Radio waves are reflected similar to light waves traveling at the same speed. Although light waves can be seen, radio waves must be detected by electronic equipment. Figure 2-4 illustrates how radio waves are reflected off the ionosphere. The reflective components of light beams are further illustrated in Figure 2-5.

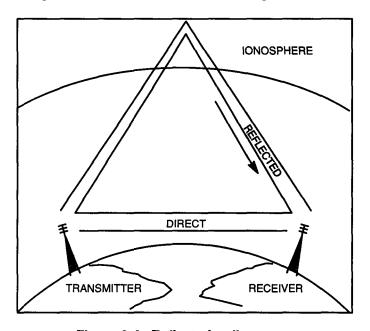


Figure 2-4. Reflected radio waves.

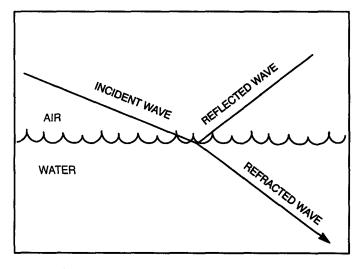


Figure 2-5. Reflection of a light beam.

Refraction

Refraction can best be illustrated by a pencil held obliquely so that a portion of it is beneath the surface of some water (Figure 2-6). From most viewpoints, the pencil will have the appearance of being bent at the point where it enters the water. This effect is because light waves travel more slowly in water than in air. This causes a change in direction of travel of the refracted light. Also, radio waves travel at a different speed over water than land. Therefore, when passing from land to water or vice versa, the radio wave is refracted or bent. Note, refraction occurs only when the wave or light beam approaches the new medium at an oblique angle. If the whole wave front arrives at the new medium at the same moment (perpendicularly), it is slowed uniformly and no bending occurs.

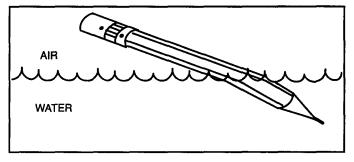


Figure 2-6. Refraction of a pencil.

Diffraction

Diffraction of a radio wave is the phenomena of bending the wave around a solid object. The lower the frequency or the longer the wavelength, the greater the bending of the wave. Therefore, radio waves are more readily diffracted than light waves. Sound waves are more readily diffracted than radio waves. Figure 2-7 illustrates why radio waves of the proper frequency can be received on the far side of a hill or other natural obstruction. It also illustrates why sound waves can be heard readily around the corner of a large building. Diffraction is an important consideration in the propagation of radio waves over long distances. The largest object to contend with is the curvature of the earth. It prevents the direct passage of the waves from the transmitter to the DF receiver.

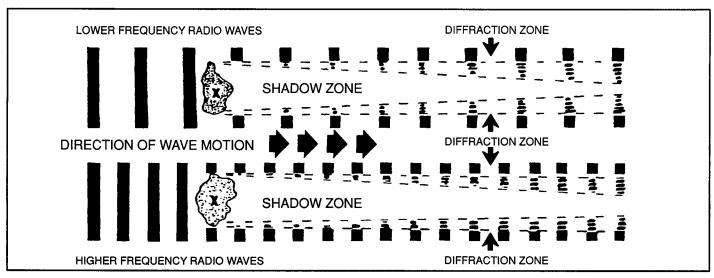


Figure 2-7. Diffraction of radio waves around a solid object.

ATMOSPHERE

The earth's atmosphere plays a crucial role in long distance radio communications. Radio waves may be reflected in the atmosphere and returned to earth. This technique is discussed later in this chapter. As shown in

Table 2-2, the atmosphere consists of multiple layers, of which only a few have any discernible effect on radio waves. The ionosphere is the primary layer that is used to return a radio wave back to earth.

Table 2-2. Characteristics of the atmosphere.

| ATMOSPHERIC REGION | LOCATION (Km) | FEATURES | EFFECT ON COMMUNICATIONS (Radio Frequency) |
|-----------------------|---|---|---|
| lonosphere | Extending 50-600 km from the earth's surface. | Electrically charged set of layers, with large amounts of free electrons. | Excellent reflection/refraction of MF and HF signals. Some VHF may be propagated as well. Primary medium for sky wave communications. |
| Stratosphere | Extending 15-50 km from the earth's surface. | The only isothermal region of the atmosphere. | No effect. |
| Troposphere | From earth's surface to 10-15 km. | Lowest region of the atmosphere. Sustains life. Temperature decreases with increasing altitude. | Negligible effect. Allows direct, surface, and ground wave communications of all frequencies. |

Ionosphere

The ionosphere is a region of ionized (electrically charged) gasses located approximately 50-600 kilometers (km) above the earth's surface. As illustrated in Table 2-3, there are essentially four layers (D, E, F1, and F2) of the ionosphere which affect communications and DF. These layers vary in ionization and height above the earth's surface, depending on the amount of exposure to the sun.

The ionosphere is formed when extreme ultraviolet light from the sun strips the electrons from neutral atoms in the ionosphere. Thus, the electrons become *free* (unbound), and the remaining atom becomes positively ionized. The free electrons reflect/refract radio waves of a certain frequency. Due to this process, the E and F layers become positively ionized.

However, the free electrons may attach to neutral atoms. When such attachments occur, the atoms become nega-

tively ionized. This process is common in the D layer, making the region of the ionosphere negatively ionized. Factors which influence the ionosphere and its effect on radio waves include—

- The time of day.
- The seasons of the year.
- Solar flares.
- Magnetic storms.
- Certain man-made disturbances such as nuclear detonations.

An important relationship between radio waves and the ionosphere is that the higher the frequency, the less its tendency to bend. Depending upon ionospheric conditions and the angle of the signal's arrival at the ionosphere, the bending may be slight. The radio waves may not be sent back to earth (Figure 2-8).

Table 2-3. Characteristics of the ionosphere.

| IONOSPHERIC LAYERS | LOCATION (Km) | FEATURES | EFFECT ON COMMUNICATIONS (Radio Frequency) |
|-----------------------|--|---|---|
| D | 50-100 km | Layer closest to earth. Negatively ionized layer, with relatively little free electrons. Exists during the day. | Primarily acts to absorb radio waves. Small amounts of refraction are possible, but unpredictable. |
| E | 100-200 km | Positively ionized with varying amounts of free electrons. State changes with temperature, angle of the sun, magnetic fields, and time of day. Exists during the day. | Erratic behavior. Sometimes reflects/ refracts radio waves in MF, HF, and lower VHF bands. |
| F | 145-400 km (F1–145-200 km) (F2–240-400 km) | Very positively ionized with large amounts of free electrons. During the day, this region separates into the F1 and F2 layers. The F region decreases in ionization and increases in altitude at night. | Primary means of reflecting/refracting MF and HF signals in sky wave propagation. At night, behavior becomes slightly erratic, but communications distances are much greater. |

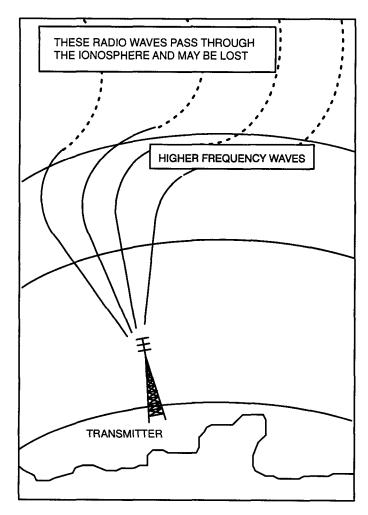


Figure 2-8. High frequency wave penetration.

During daylight hours, the ionosphere is subject to full ultraviolet output from the sun. Therefore, the D, E, F1, and F2 layers reach their full potential. At night, the composition of the layers of the ionosphere changes as the F layers combine. Therefore, higher radio frequencies are more likely to penetrate the ionosphere and be lost. As a general rule, lower communication frequencies are used during the night.

Conversely, during the day when ionization of the atmosphere is more intense, higher communications frequencies can be used without undue loss of the signal. This is because penetration of the ionized layer is at a minimum. Changes in the relative proximity of the sun to the earth will also cause gradual changes in the ionosphere. The longer exposure of the ionosphere to the sun in the summer causes a greater degree of ionization during the night and day. Therefore, higher

frequencies may be used for summer operations. Figure 2-9 illustrates the approximate heights of the various layers of the ionosphere.

Remember, however, that the actual number of layers, their heights above the earth, and the relative intensity of ionization present will vary. They vary from hour to hour, from day to day, from month to month, and from year to year.

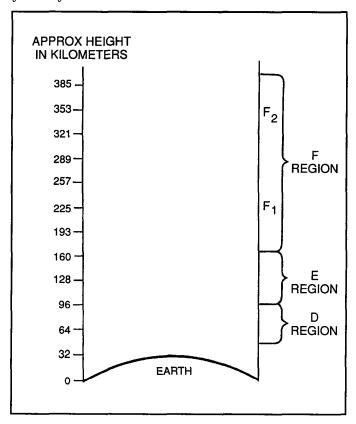


Figure 2-9. Approximate heights of ionospheric layers.

Stratosphere

The stratosphere is that portion of the earth's atmosphere between the ionosphere and the troposphere. Since the temperature in this region is considered to be almost constant, it is also known as the isothermal region. The stratosphere has little, if any, effect on radio waves which are transmitted through it. It is mentioned only to differentiate the three major regions of the earth's atmosphere.

Troposphere

The troposphere greatly influences electromagnetic emissions. It is that portion of the earth's atmosphere extending from the surface of the earth to heights of approximately 10 to 15 kilometers. This region contains the mixture of gasses we depend on for life. Additionally, most weather activity occurs in the troposphere.

WAVE PATHS

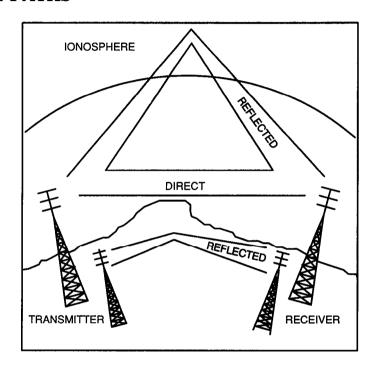
There are three distinct paths that a radio wave may take to reach the receiving antenna. They are—

- Direct.
- Reflected.
- Refracted.

The direct and reflected paths are shown in Figure 2-10. They are purposely exaggerated to enable the reader to clearly grasp the differences.

The direct path goes directly from the transmitting to the receiving antenna. The reflected path bounces off the ionosphere or the surface of the earth at the same angle at which it arrives and continues to the receiving antenna (angle of incidence = angle of arrival). The refracted path is the path caused by the bending of the waves in the same manner light waves are bent when seen through water.

If the waves are refracted by the earth, the distance they travel is severely limited due to large losses of energy in the form of heat dissipated into the earth's crust.



WAVE TYPES

Radio waves may be classified as either ground waves or sky waves (Figure 2-11).

Ground waves are continually in contact with the earth's surface. They do not make use of reflection from the ionosphere. They have a tendency to be refracted and, in some cases, reflected into the lower atmosphere. At frequencies above 1500 kilohertz, a ground wave is affected very little by the time of day or season. The ground wave loses much of its strength and dissipates energy as it travels over the earth's surface. However, less strength is lost when it travels over water.

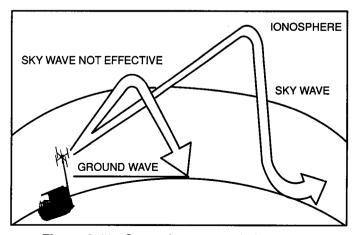


Figure 2-11. Ground waves and sky waves.

Sky waves are transmitted upward with respect to the earth's surface. Sky waves would not be useful for communications were it not for the ionosphere. Radio waves approaching the ionosphere at an angle are refracted back to earth. They may be detected and used

for communications purposes or for DF exploitation. Figure 2-12 depicts the waves that penetrate the ionosphere and are lost for all practical purposes. It also illustrates those waves that return to earth for communication use.

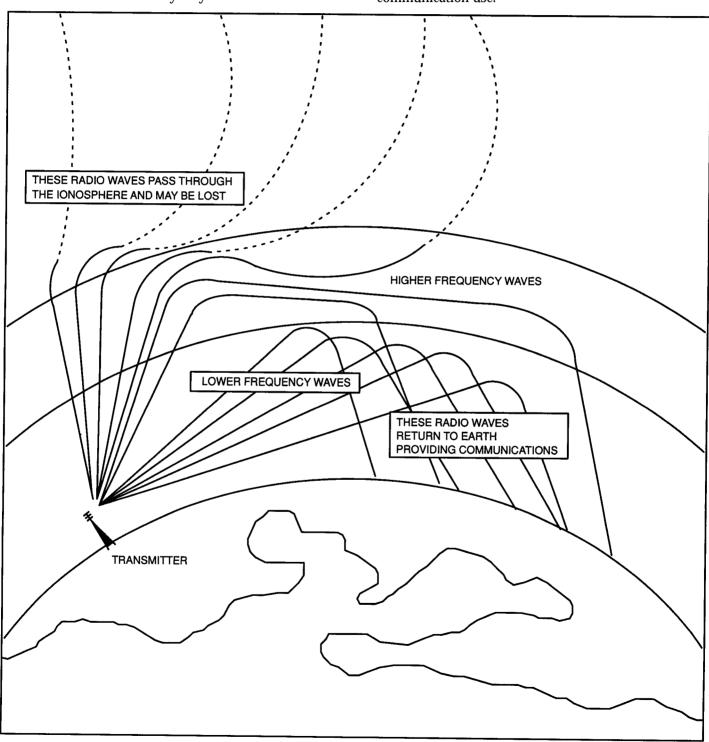


Figure 2-12. Sky waves.

SKIP ZONE AND DISTANCE

The skip zone is the area where the ground wave can no longer be detected (Figure 2- 13) and the sky wave has not yet returned to earth after being reflected or refracted off the ionosphere or troposphere. The skip distance is that area where no sky wave reception will be possible. This is because the wave has not returned to earth after its first or subsequent bounce off the reflecting layer.

Depending upon the frequency and the transmitter power, multihop transmissions are routinely used for communications. Figure 2-14 illustrates multihop transmissions. There will be, however, skip zones between the points of the wave's return at each hop. Note, however, skip zones are not static or stable.

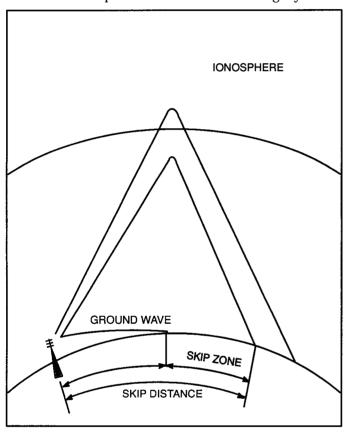


Figure 2-13. Skip zone and distance.

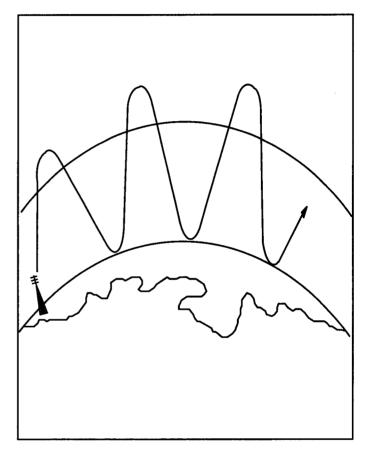


Figure 2-14. Multihop transmissions.

CHAPTER 3

TECHNOLOGY

The Army has several DF systems that target varying types of threat signals, frequencies, and ranges. The DF systems are also characterized by their mobility and their assigned military echelon. These systems are outlined in Table 3-1.

This chapter relates some of the historical and technological developments in acquiring a signal

azimuth. It explains some of the antennas, systems, and bearing indicators used to obtain DF information. All direction finding systems serve one primary purpose-to measure the angle of arrival of an EM wave in reference to a known reference (true, magnetic, or grid north).

Table 3-1. Army direction finding systems.

| EQUIPMENT | ECHELON | MOBILITY | SIGNALS | MOS (Op/Maint) | FREQ (DF) |
|----------------------------|------------------------|------------------------------|-----------------|----------------------|-----------------|
| AN/PRD-10 MRDFS | Div, ACR MI Co (SF) | Ground Vehicle Manpack | CW, AM, FM, SSB | 98G/33T | VHF |
| AN/PRD-11 MANPACK | Div, ACR MI Co (SF) | Ground Vehicle Manpack | CW, AM, FM, SSB | 98G/33T | VHF, UHF |
| AN/TRQ-32 TEAMMATE | Corps, Div ACR | Ground Vehicle | CW, AM, FM, SSB | 98G, 98H, 33T | VHF |
| AN/TRQ-37 TACFIX | Div | Ground Vehicle | CW, AM, FM, SSB | 98G, 98H, 33T | VHF |
| AN/TSQ-138 TRAILBLAZER | Div | Ground Vehicle | CW, AM, FM, SSB | 98G/33T | VHF |
| AN/TRD-15/23 | EAC | Ground Vehicle Semi-Fixed | CW, AM, FM, SSB | 98D/33T | HF |
| AN/TSQ-152 TRACKWOLF | EAC | Ground Vehicle Semi-Fixed | CW, AM, FM, SSB | 98D, 98H, 98G/33T | HF |
| AN/FLR1-9 | EAC | Fixed | CW, AM, FM, SSB | 98D/33P | HF |
| DF-6 | EAC | Fixed | CW, AM, FM, SSB | 98D/33P | HF |
| AN/ALQ-151 QUICKFIX | Div, ACR | Airborne | CW, AM, FM, SSB | 98G/33R | HF, VHF |
| AN/USD-9 GUARDRAIL V | Corps | Airborne | CW, AM, FM, SSB | 98D, 98C, 98G/33R | HF, VHF, UHF |
| AN/ALQ-133 QUICKLOOK II | Classified | Airborne | CW, Pulse | 98J, 33T | UHF |
| AN/TSQ-164 DRAGONFIX | Corps | Ground Vehicle | CW, AM, FM, SSB | 98G, 98H, 33T | HF |

HISTORY OF MAJOR DIRECTION FINDING SYSTEMS

Loop Antenna

Early direction finding technology required a movable directional loop antenna and a receiver. The arrival angle is measured by moving the antenna until a maximum or minimum signal strength is achieved. The simple loop antenna (Figure 3-1), or some derivative of it, can still be found today. One of the disadvantages of using this method is that the signal being measured is reduced, while noise from other directions is not. To overcome this problem, wave amplitude comparison (using two directional antennas with different orientations) was introduced.

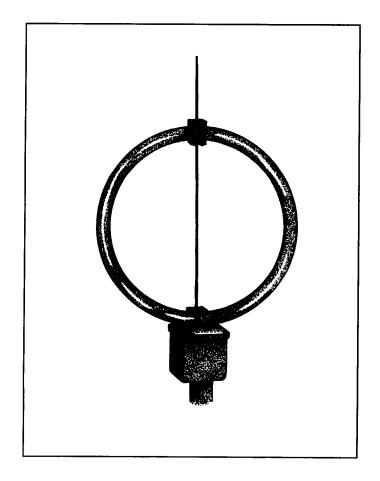


Figure 3-1. Loop antenna.

Rotating Loop

It was not always feasible or desirable to physically move the antenna. As a result, some RDF technology used a fixed antenna that measured signal strength to provide an azimuth. One of the earliest of these systems used fixed crossed loops to feed a small orthogonal loop arrangement with a rotating loop inside of it. This was called a goniometer. Today, the term goniometer may refer to any type of mechanical or electrical cyclic sampling equipment.

Cathode Ray Tube

The first cathode ray tube (CRT) direction finder used cross loops (Figure 3-2). Instead of using a goniometer, each loop was fed to a channel of a dual-channel receiver. The outputs from the receiver were applied to pairs of deflection plates within a special CRT.

A clear signal produced a straight line, the angle of which gives the azimuth of the signal.

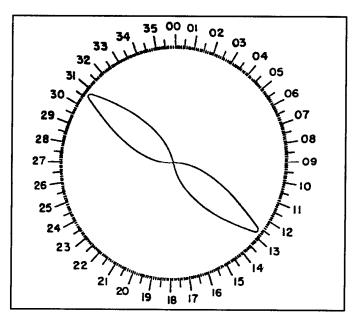


Figure 3-2. Cathode ray tube.

Adcock Antenna

Until the end of World War II (WWII), the most common type of DF system was the crossed loop or Adcock antenna (Figure 3-3). This antenna system is still used in modified form for short-distance direction finding systems. The Adcock antenna used top horizontal members that were well shielded, to reduce polarization errors. These systems were small in relation to the wavelength of the received signals. They were therefore classified as narrow aperture direction finding (NADF) systems.

Wullenweber System

During WWII, the Wullenweber system heralded the era of wide aperture direction finding (WADF) systems (Figure 3-4). The Wullenweber has a circularly disposed antenna array (CDAA) up to 1,000 meters in diameter with a large number of elements. About a third of the elements are combined to form sum/difference beams. The beams are effectively rotated in azimuth by a rotating switch (goniometer) which connects and combines elements around the ring.

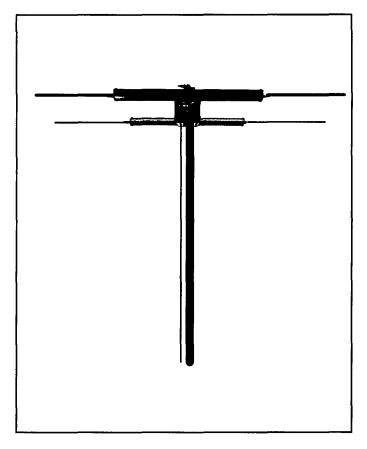


Figure 3-3. Adcock antenna.

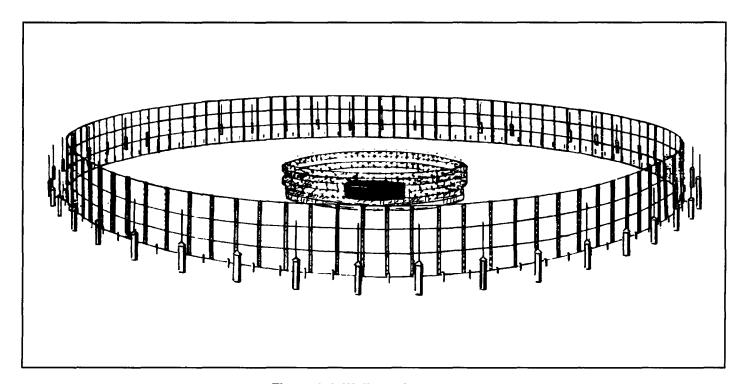


Figure 3-4. Wullenweber system.

Quasi-Doppler System

A further variation of the Wullenweber system is called the Quasi-Doppler or Pseudo-Doppler system (Figure 3-5). This variation has also been called a commutated-antenna direction finder (CADF). Most of the older groundbased EAC tactical direction finding systems are of this type. In theory, the Doppler systems impose a phase modulation on the received signal by moving the antenna in a circle. The phase of the modulated signal is a function of its direction. In actual practice, a fixed CDAA is used. The receiver rapidly samples each antenna around the ring by using a goniometer switch.

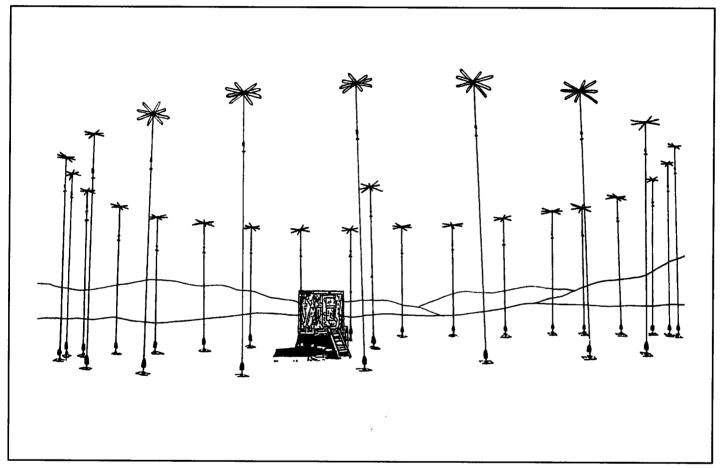


Figure 3-5. Quasi-Doppler system.

Interferometric System

Interferometric systems area completely different class of direction finding systems (as illustrated in Figure 3-6). The azimuth of an incoming wave is not deduced by rotating beams. It is taken from the phase measurements of signals, made on a number of spaced antennas. Unlike the beam-forming type of WADFs, interferometers accept all signals on the array. Two different approaches are used to process the results. Depending on the type of system, one or both of the following may be used:

- Wavefront analysis (WFA).
- Wavefront testing (WFT).

Wavefront analysis accepts all signals but attempts to recover the major ones. It attempts this by analyzing the complex voltages measured on the elements of the antenna array under wave interference conditions.

Wavefront testing accepts only signals arriving from one direction or quasi uni-modal propagation (QUMP). QUMP is achieved by detecting a linear phase shift across the array with near equal amplitudes on all the elements. (This process is also called coincidence interferometry.) For further information on linear phase shift and measuring wave amplitude, see TM 11-666.

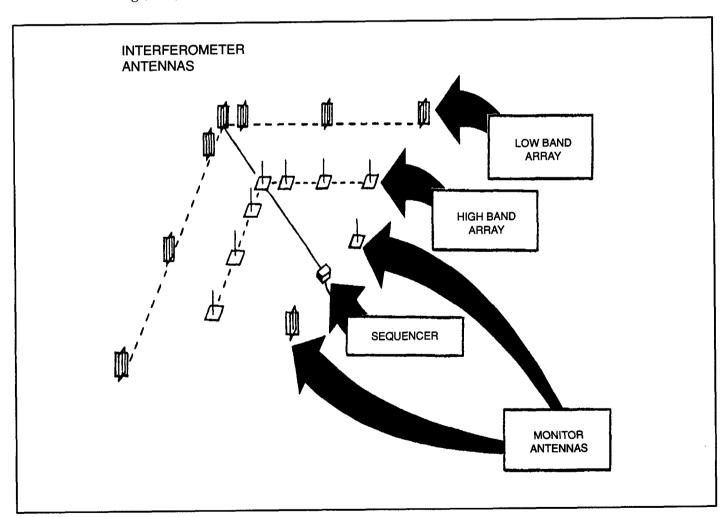


Figure 3-6. Interferometric system.

Time-Difference System

There are time-difference direction finders (TDDF) which measure the difference between the times of arrival of the radio wave at a number of receiving sites. A hyperbolic position line is obtained from the time difference between each pair of sites.

Single Station Locator System

As demonstrated earlier, there are many types of direction finding systems. In some, only the horizontal component (or azimuth) of the arrival angle can be measured. In others, the azimuth and the vertical component (elevation angle) can be obtained. When only an azimuth is resolved, two or more independent DF stations are needed to determine the position of the

transmitting antenna. Systems that measure both azimuth and elevation angles are called single station locator systems because, in the case of signals propagated in the ionosphere, two components from just one DF station are sufficient to define the location of the transmitting antenna (assuming a knowledge of the ionosphere along the wave path). The SSL was developed because of the problems of audibility with the traditional DF network. Sometimes the signal could only be heard at one DF site.

The SSL system direction finder is a phase measuring interferometer. Location data include an azimuth measurement on the target signal and a range estimate based on the measured parameters at the DF site. The combination of azimuth and great circle range to the target produces the location output from the system's computer.

DIRECTION FINDING THEORY

Quasi-Doppler Theory

The Doppler DF system is based on Christian Johann Doppler's principle for wave motion, commonly called the *Doppler effect*. The Doppler effect is the perceived change in the frequency of waves from a given source by the observer, when the source and observer are in rapid motion with respect to each other. The frequency of the wave increases or decreases according to the speed at which the distance is increasing or decreasing between the observer and source. An example of the Doppler effect is a train approaching an observer and blowing its whistle. As the train approaches at a high rate of speed, the frequency of the sound waves emitted from the whistle increase. The train passes by and leaves the observer, and the frequency of the whistle decreases.

In an idealized Doppler DF system, the motion of the receiver could be obtained by moving one antenna in a circular path as shown in Figure 3-7. With this system, the frequency of the received wave would be lower than

the transmitted frequency during the time the antenna moves with the wavefront. It would be higher than the transmitted frequency when it moves against the wavefront. No change occurs when the antenna is moving perpendicular to the direction of arrival of the EM wave. This activity produces a sinusoidal waveform across the array, such as illustrated in Figure 3-8.

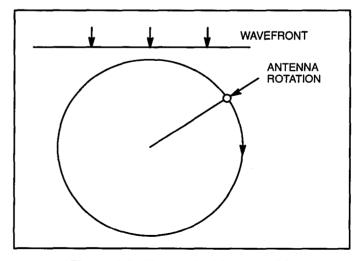


Figure 3-7. Theoretical Doppler DF.

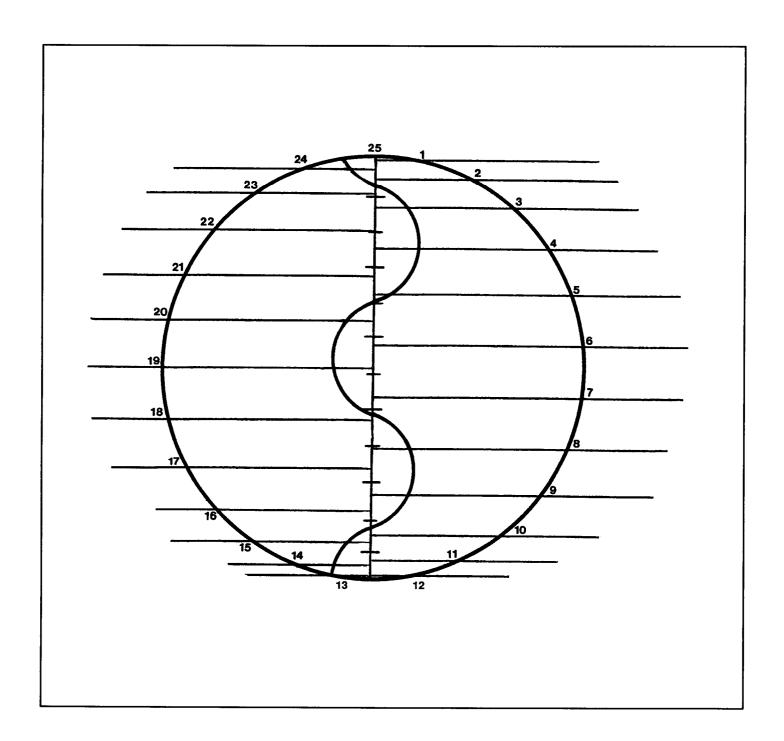


Figure 3-8. Sinusoidal waveform across the array.

The direction of arrival of the signal can be determined if the phase of the frequency modulation signal produced by the antenna motion is compared to a reference phase. The antenna peripheral speed is required to produce an adequate degree of frequency modulation. This speed is impractical to attain in a single rotating antenna system.

To create the required peripheral speed, a simulated Doppler motion is made by placing a number of fixed antennas in a circular array and scanning the signals from the antennas. This is done by sequential sampling using a rotary coupler and drive unit motor (Figure 3-9, page 3-8).

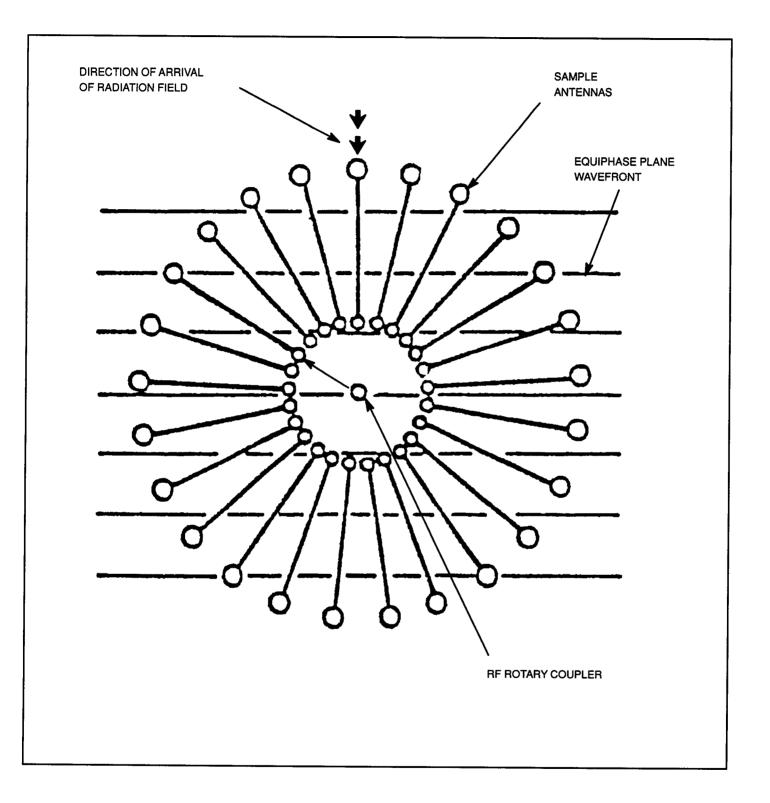


Figure 3-9. Quasi-Doppler DF.

A signal from a distant transmitter induces voltages of equal amplitude in all antennas of the array. The phase difference between the signals in adjacent antennas is a

function of the frequency and direction of arrival as shown in Figure 3-10.

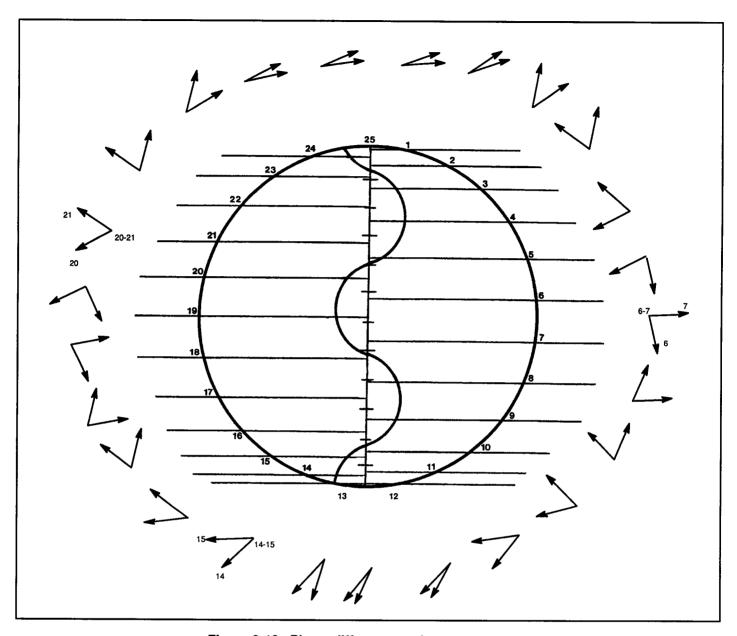


Figure 3-10. Phase difference at the antenna array.

The maximum phase step between adjacent antennas is found between those which fall on a line most nearly parallel with the direction of the wave travel. The minimum phase step occurs between antennas falling on a line most nearly perpendicular to the direction of wave travel.

The antennas of the array are scanned in sequence by a rotating coupling coil unit. The vectors revolve quickly in relation to the motion of the rotor unit. However, at any single moment, the relative phase relationships between antennas do not change with the time of

viewing or motion of the coupler. The relationship only changes with the measured frequency.

Signals from adjacent antennas are combined during the scan to produce a frequency modulated (FM) signal. The frequency deviation at every instant is proportional to the size of the phase step between adjacent antennas. The phase of the envelope of the FM depends only on the direction of arrival of the signal. A bearing indicator compares the phase of the FM envelope with a reference phase and presents the bearing indication on a CRT.

Single Station Locator System Theory

Determining a transmitting antenna's location with the SSL system requires an azimuth measurement on the target signal and a range estimate based on measured ionospheric parameters. These requirements automatically infer certain limitations on the system.

Because the SSL system depends on ionospheric propagations, it is designed for use against the high frequency (HF) spectrum sky wave transmissions. As shown in Figure 3-11, the combination of an azimuth and great circle range to the target produces a location from the system that is expressed in geographic coordinates. An HF radio wave transmitted from a target transmitter is reflected from one or more reflecting

regions in the ionosphere and arrives at the SSL site with a given bearing and angle of elevation. All SSL systems today use interferometric antenna systems to measure these azimuth and elevation angles.

The SSL system includes an ionospheric sounder which measures the height of the ionospheric reflecting region. There are two types of sounders used in SSL systems. The oldest type is the vertical incidence sounder (VIS) as shown in Figure 3-12. This sounder measures ionospheric reflection heights straight up from the sounder site (usually collocated with the SSL site). A more recent and accurate sounder is the oblique incidence sounder (0IS) as shown in Figure 3-13. The sounder, usually located along the anticipated target ray path, transmits at an oblique angle to the ionosphere and is received at another location (usually the SSL site).

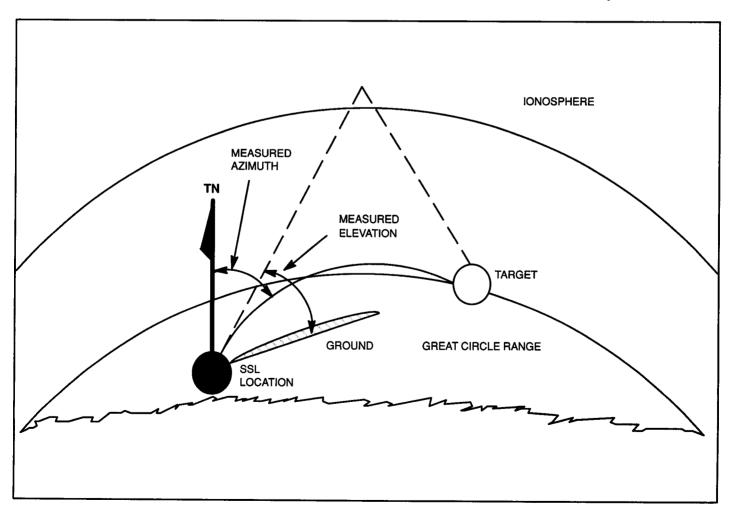


Figure 3-11. Single station locator DF.

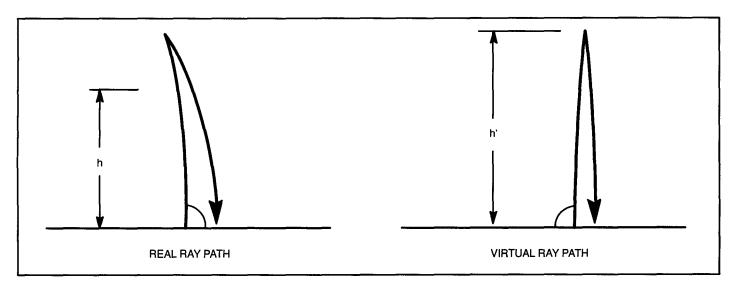


Figure 3-12. Vertical incidence sounder.

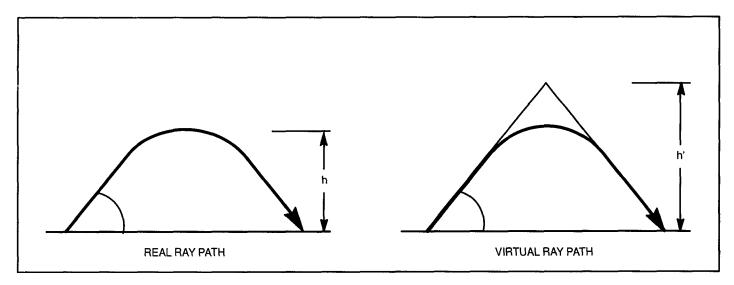


Figure 3-13. Oblique incidence sounder.

After the height of the ionosphere is measured, the SSL then assumes that the reflection height measured by the sounder applies at the midpoint of the radio wave path. Figure 3-14, page 3-12, shows the triangle from the SSL site through the ionospheric midpoint and down to the target transmitter antenna may be solved. This calculation generates a range estimate which, when combined with the observed bearing, is used to calculate the coordinates of the target location.

Each SSL system has a unique way of calculating range. The most commonly found range calculation uses the measured elevation and virtual height with the law of cosines to determine the angle at the center of the earth from the midpoint (half range) to the SSL system. This angle, when multiplied by twice the earth's radius, gives the great circle range from the SSL site to the target. Other systems attempt to also provide traveling ionospheric disturbances, magnetic dip angle, and electron density data in the calculations for a more accurate product.

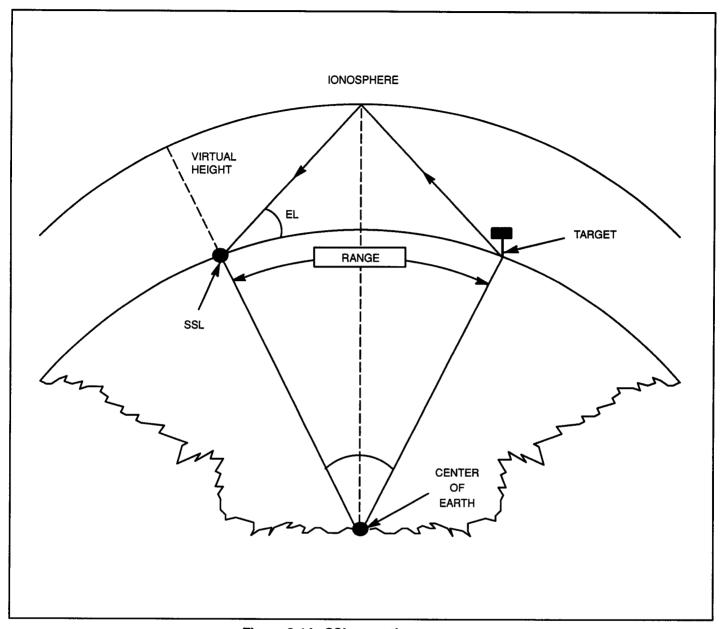


Figure 3-14. SSL operations concept.

Most SSL systems offer the following fundamental performance steps:

- The SSL computer is interfaced to the phase-measuring interferometer antenna array and to the ionospheric sounder.
- System data acquisition is controlled by a single operator.

Operator functions include—

- Identifying the target signal.
- Optimizing receiver tuning.

• Starting and terminating direction finding data collection.

Automatic functions of the systems include—

- Computing the target azimuth and elevation angles of arrival.
- Providing real-time measurement of ionospheric heights.
- Computing location coordinates.

CHAPTER 4

PERFORMANCE FACTORS

Strategic direction finding is normally conducted against transmitters located a great distance from the DF site. The radio waves are reflected or refracted by the atmosphere prior to interception. This is commonly referred to as sky wave direction finding (SWDF). Strategic DF sites at echelons above corps are normally a minimum of 150 kilometers from the forward line of own troops (FLOT).

Tactical direction finding is normally conducted against enemy transmitters located close to the DF site. The direct wave component of the transmitted wave is normally used to locate the transmitting antenna. This is referred to as direct wave direction finding (DWDF). Tactical DF equipment is normally located within 5 to 15 kilometers of the FLOT.

Airborne radio direction finding (ARDF) is the term used to identify the DF effort conducted from an airborne platform. ARDF may be used in either a strategic or tactical situation.

STRATEGIC FACTORS

Strategic direction finding sites are quite often designed to provide DF coverage over vast geographic areas such as an entire or large portion of a continent. Nets of this nature will frequently have sites established along a baseline thousands of kilometers in length. Bearings are acquired on sky waves arriving at the DF antennas. The major influencing factors concerning SWDF operations

include the—

- Distance from the transmitting antenna.
- Sky wave propagation.
- Transmitter power.

To illustrate the distance factor, imagine a strategic direction finding site located in the skip zone (Figure 4-1).

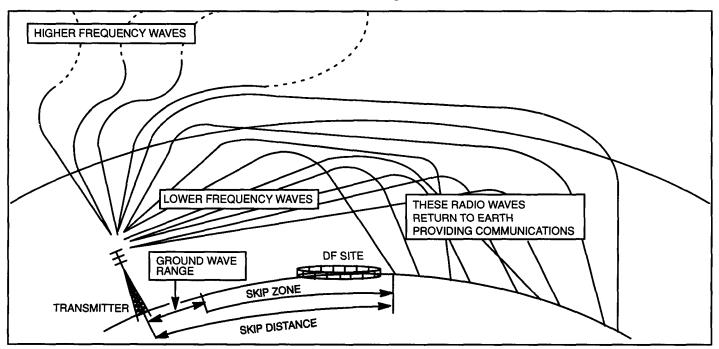


Figure 4-1. DF site located in skip zone.

The skip zone is that area where the ground wave can no longer be detected and the sky wave has not yet returned to the earth after being reflected or refracted off the ionosphere or troposphere. A SWDF site in the skip zone would not be able to receive the transmitted signal. Therefore, it could not obtain a bearing. (Strategic DF errors caused by radio wave propagation are discussed in Chapter 7.)

Sky waves and multihop transmissions (Figure 4-2) are dependent upon the frequency used and the power of the transmitter. The transmission range is affected when a low-powered transmitter is used. A signal from a low-powered transmitter that travels a great distance to the strategic site will normally be weak and fading. This results in no bearing being obtained on the signal, or if a bearing can be obtained the reliability will be questionable.

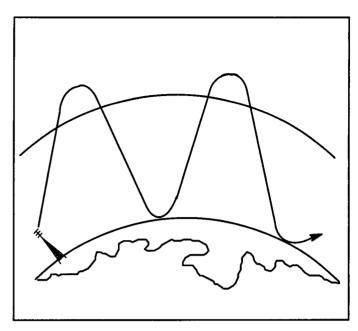


Figure 4-2. Sky waves and multihop transmission.

TACTICAL FACTORS

Consider a tactical situation where the predominant enemy frequencies used are 30 megahertz (MHz) and above. Normally, the characteristics are as follows:

- Communications are short range and line of sight.
- Frequency modulated voice is the primary type of transmission.
- Transmitters are usually highly mobile, either man-packed or vehicle mounted. They commonly use whip antennas which are omnidirectional and vertically polarized.

An important factor in tactical radio direction finding is wave propagation. The following paragraphs identify and discuss wave propagation factors.

Ground Wave

The waves radiated from a transmitting antenna spread out into the atmosphere and along the earth, as well as into the earth. Because of the conducting properties of the earth, some of the energy is reflected from the earth's surface. The part of the wave not reflected enters the earth where the energy rapidly dissipates as heat. Other portions of the waves spread out along the earth and into the atmosphere. They travel to the intended receiver as

well as to the DF set. The resulting ground wave is composed of one or more of the following wave components:

- Direct wave.
- Ground-reflected wave.
- Surface wave.

Direct Wave

Direct waves travel directly from the transmitting antenna to the receiving antenna. The direct wave is not appreciable y affected by the earth's surface, but it is subject to refraction in the atmosphere between the transmitting and receiving antennas. The direct wave is the principle means of transmission in tactical very high frequency (VHF) communications, so it is important in tactical direction finding operations.

Ground-Reflected Wave

A ground-reflected wave reaches the receiving antenna after being reflected off the ground. If both the transmitting and receiving antennas are located on the ground, the difference in path lengths between a direct wave and a ground-reflected wave is small. However, these waves may arrive at a tactical DF set out of phase.

This reduces the received signal strength, particularly at frequencies below 30 MHz. Tactical communications conducted below 30 MHz are primarily with the surface wave component.

Surface Wave

A surface wave travels directly along the surface of the earth. Although it does extend above the ground, its strength is diminished with increasing height. A surface wave is affected primarily by the conductivity and dielectric constant of the ground over which it travels. It is the primary component acted upon by groundbased tactical DWDF systems taking bearings on frequencies below 30 MHz. Three important influencing factors of a surface wave are—

- Frequency.
- Terrain.
- Polarization.

Frequency. Frequency, along with transmitter power, affects the range of the signal. While ground waves are produced at all frequency ranges, sky waves are generally possible only at frequencies below 20 to 30 MHz. Any DF effort targeted above this range will be working with ground waves. Below this range, tactical equipment can actually work with sky waves and ground waves. Generally, surface wave performance is greater

at lower frequencies. These ground waves are unintentional by-products of transmissions whose main energy is directed toward the ionosphere rather than along the surface of the earth (Figure 4-3).

Terrain. Terrain is most influential on high frequency radio communications. The dielectric constant and the conductivity of the terrain over which the HF surface wave component travels can affect its range considerably. However, as previously stated, as the frequency of the transmitted signal increases, the surface wave decreases. Therefore, the electrical characteristics of the terrain have less effect on a signal as it increases in frequency.

Polarization. When a surface wave is horizontally polarized, the earth has a short-circuiting effect which causes the wave to dissipate rapidly into the ground. If a transmitted wave has some degree of both vertical and horizontal polarization, the horizontal portion will be quickly absorbed. Only the vertically polarized part of the wave will travel any appreciable distance. Because of this, it can be assumed that surface waves received can be considered to be vertically polarized. This is an important factor since most tactical DF systems employed against surface waves use monopole antennas to receive vertically polarized waves.

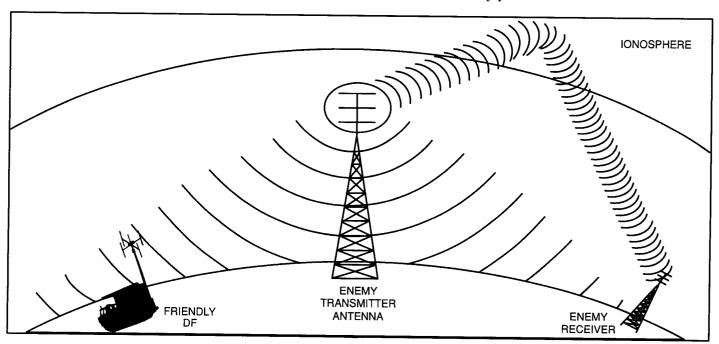


Figure 4-3. Ground wave DF.

Ground Wave Distance

The distance (from the transmitter to a tactical DF set) that a ground wave can be received is subject to extreme variations. It is affected by such factors as transmitter power, antenna type, terrain, man-made objects, and operating frequency. Advance estimates of expected

ground wave range in a given environment can be made if some knowledge of the enemy's communications equipment and operating techniques are available. However, some actual operating experience in each situation is usually required before reliable range estimates can be made.

DIRECTION FINDING BASELINES

A groundbased DF baseline is that imaginary line or axis along which the DF equipment of a DF network (three or more DF sites) are deployed. The establishment of either a groundbased strategic or tactical DF baseline is a

matter of placing the DF equipment so that good bearing angles for triangulation within the target area are possible. Triangulation is the intersection of bearings at the target area (Figure 4-4).

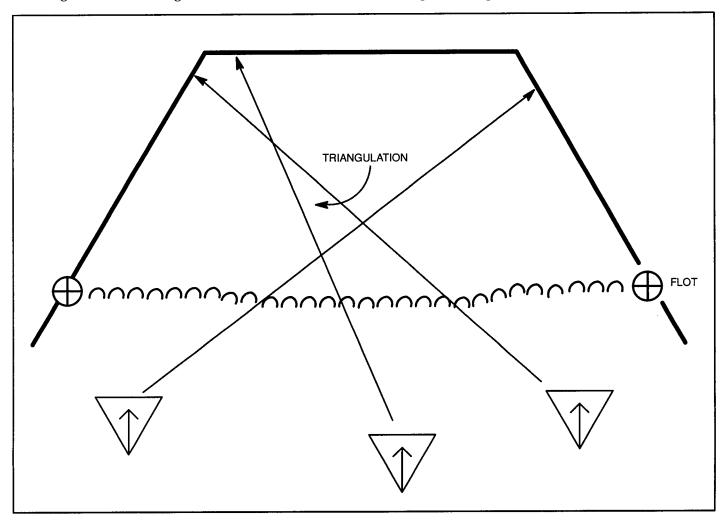


Figure 4-4. Triangulation.

Ideally, each of the DF sites should have an unobstructed wave path between the DF antenna and any point within the target area. In most cases, however, this is not possible. Tactical DF sites should be arranged so that portions of the target area that are *masked* or hidden from one or more DF sites can still be covered by at least three other sites. This is similar to setting up interlocking fields of fire for weapons. The exception, in the case of the DF equipment, is that each area must be

covered by a minimum of three *lines of fire* instead of one or two (Figure 4-5).

A masked transmitter occurs whenever the enemy takes advantage of terrain features to hide their communications from our groundbased DF operations. Masking is most effective in line of sight communications. A situation in which a site is masked is illustrated in Figure 4-6, page 4-6.

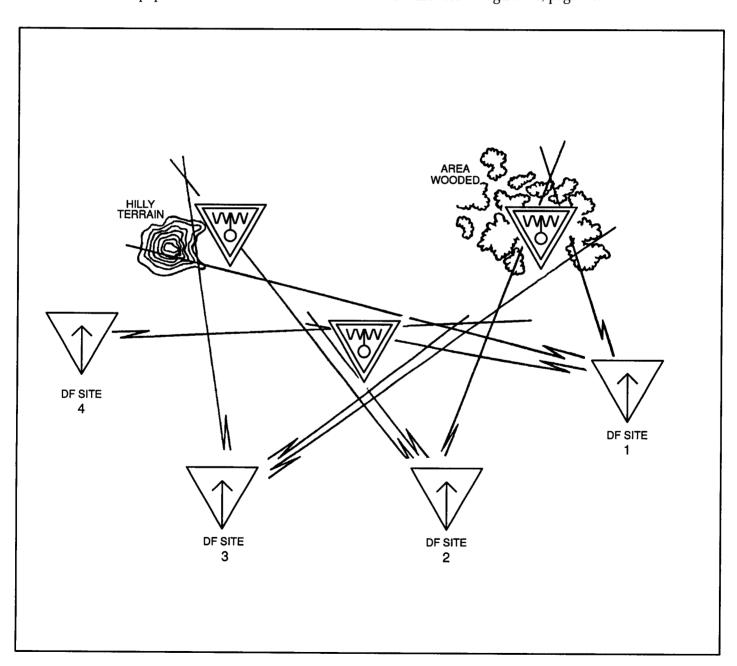


Figure 4-5. Target area coverage.

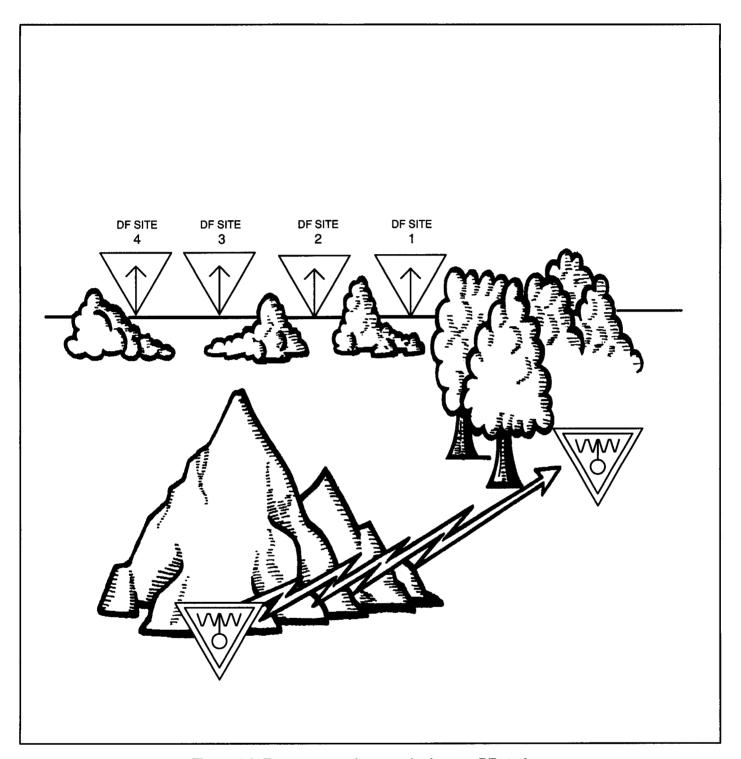


Figure 4-6. Enemy transmitter masked to our DF stations.

As you can see, when the transmitting antenna is hidden behind a hill, it is electronically hidden from the direction finding sites. However, the enemy is still able to communicate effectively with it outstation. Additionally, establishing a suitable DF baseline is affected by tactical, stragic, and technical considerations. Essentially, there are two types of baseline configurations used to establish a groundbased direction finding network—concave and convex.

Concave Baseline

It is best to locate the DF sites on a concave baseline if it is expected that the target locations will be in a compact, narrow but deep frontal area. This situation is illustrated in Figure 4-7.

Using this baseline, triangulation from the DF site bearings is satisfactory at longer ranges. Triangulation is excellent at short ranges.

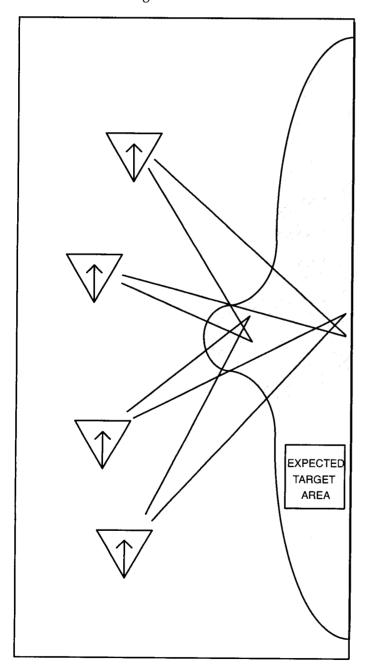


Figure 4-7. Concave baseline.

Convex Baseline

If the target locations are anticipated to be located over a wide flanking, short, in-depth area (Figure 4-8), a convex baseline is suitable.

Using a convex baseline provides a reasonable azimuth angle over a wide front. It is probable that the convex baseline will satisfy the average tactical or strategic situation.

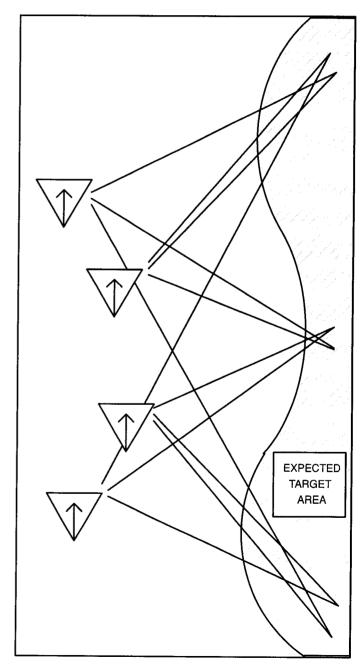


Figure 4-8. Convex baseline.

Baseline Distance

The baseline distance is a straight-line distance that separates the two outermost DF sites (Figure 4-9).

As a rule of thumb, the depth at which a DF network can effectively locate enemy transmitter antennas is equal to the total distance of the baseline joining the two outermost DF sites. This distance is then measured from the center of the imaginary baseline to the target area. For example, if the DF baseline is 80 kilometers in length, the net fix location capability is 80 kilometers in depth (Figure 4-10).

KILOMETERS **EXPECTED** TARGET **AREA**

Figure 4-9. Baseline distance.

Establishing a tactical DWDF baseline is dependent on the mission, enemy, terrain, troops and time available (METT-T). The tactical commander determines the areas available for the siting of the DF equipment within the area of operations. However, the target area to be covered dictates the baseline configuration employed in most situations. It should also be noted that an effective DF baseline is dependent upon equipment capabilities. In some situations, conditions maybe prohibitively unfavorable for tactical DWDF operations. This is because of impossible terrain conditions, unusual propagation factors, or baseline restraints.

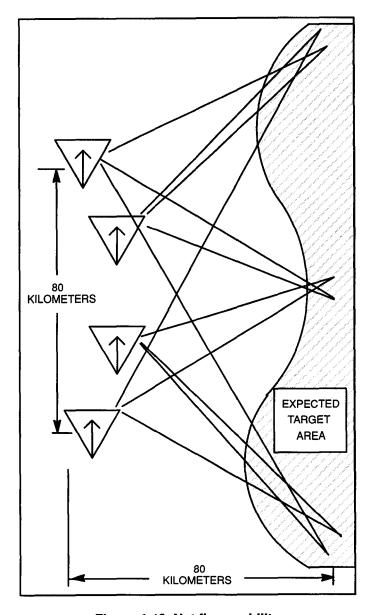


Figure 4-10. Net fix capability.

AIRBORNE RADIO DIRECTION FINDING

In the ARDF effort, aircraft are used as DF sites. These aircraft are used to supplement groundbased DF systems by providing an aerial platform to extend the radio horizon. There are several factors, however, which affect ARDF operations. The most important factors are the weather and the availability of airspace. Obviously, storms and adverse weather conditions will keep ARDF aircraft on the ground. Because ARDF aircraft operate at relatively low altitudes and slow speeds, they are vulnerable to surface-to-air missiles and hostile aircraft. Therefore, to accomplish the mission, ARDF aircraft must have the freedom of airspace.

Groundbase direction finding baseline principles are also applicable to ARDF. However, ARDF operations do not have the possible restraints that could hinder establishing a groundbased DF baseline; for example, terrain restrictions or the availability of land. Considering that the airspace will be controlled by friendly forces, ARDF aircraft only have to maneuver for a baseline behind the FLOT. In single ARDF aircraft operations, a baseline is that flight pattern where a minimum of three LOBs or line of position (LOP) are taken on a target, resulting in the location of the target transmitter antenna (Figure 4-11).

Operations involving more than one aircraft (Figure 4-12, page 4-10) require that each aircraft fly a track which provides as wide a baseline as possible. As with groundbase systems, a minimum of three LOBs are required to accurately locate the target.

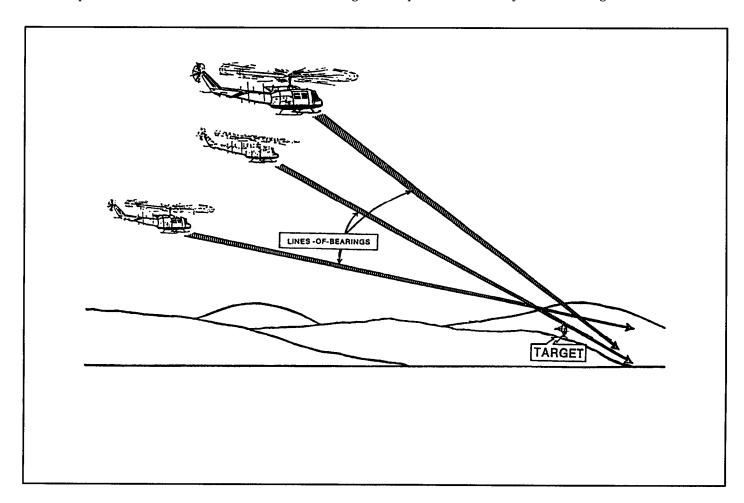


Figure 4-11. Single aircraft deployment.

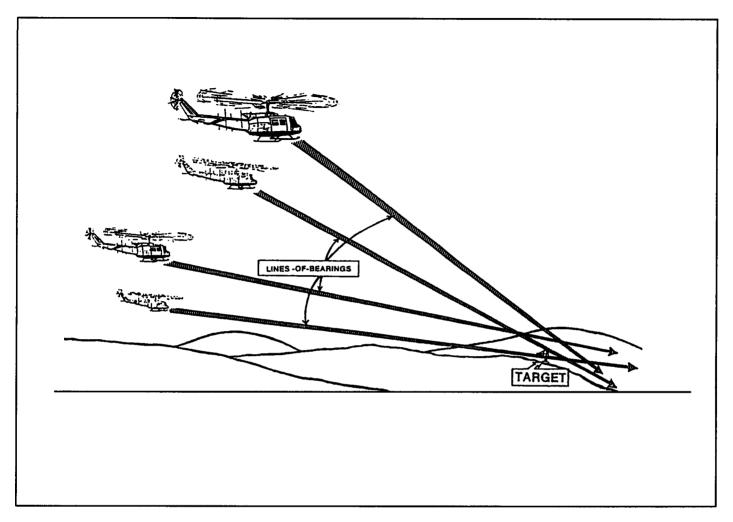


Figure 4-12. Multiple aircraft deployment.

CHAPTER 5

SITE DEPLOYMENT

It is not the intent of this section to address all aspects of a strategic or tactical direction finding site. Rather, the purpose is to establish general guidelines for use in strategic and tactical DF site deployment. NOTE: EAC groundbased DF can be employed in semifixed or mobile configurations, as either strategic or tactical assets.

STRATEGIC

Normally, EAC and strategic direction finding sites are distantly located from their net control station (NCS). A noncommissioned officer, referred to as the DF site supervisor, is in charge of an EAC or strategic DF site. In many cases, these direction finding sites are not located near any military support activity. Therefore, as the direct representative of the commander, the duties and responsibilities of the site supervisor are diversified and numerous. The site supervisor is directly responsible to the commander for—

- Mission. This includes the day-to-day site operation (equipment operation and maintenance) and accomplishing the mission as directed by the NCS.
- **Security**. This includes physical security of the DF site (equipment and personnel) and classified information security (communications security (COMSEC)).
- Personnel. This includes the health, welfare, recommendation for promotion, discipline, and counseling of DF site personnel.

TACTICAL

A team chief is normally in charge of tactical communications and noncommunications DF site operations. A team chief is directly responsible to the platoon leader for—

 Mission. This includes the day-to-day operation (equipment operation and maintenance) and accomplishing the mission as directed by the MI battalion tactical operations center (TOC) (division) or the MI brigade TOC (corps).

- **Security.** This includes survivability of the equipment and personnel in a hostile environment.
- **Personnel.** This includes the health, welfare, recommendation for promotion, discipline, and counseling of DF site personnel.

SITE LOCATION

Regardless of whether a DF site is strategic or tactical, once it has been installed its location must be accurately determined and reported. If a site's location is erroneously calculated, reported, and placed on a plotting map or entered into a computer, it will result in

an inaccurate determination of target locations. There are three methods of determining a site location—

- Resection.
- Geodetics.
- Satellite derived, global positioning system (GPS).

Resection

Determining the location of a DF site by sighting two or three known features, from the DF site, is called resection. First, orient the universal transverse mercator (UTM) 1:50,000 map using the compass. Locate the two or three known positions on the ground and mark them on the map. Using the compass, measure the magnetic azimuth from the DF site to one known position. Convert this azimuth to a grid azimuth. Change the grid azimuth to a back azimuth (refer to FM 21-26) and draw a line on the map from the known position back toward the DF site. Repeat for each known position. The intersection of the lines is the location of the DF site (Figure 5-l). Using three lines, a triangle may be

formed. If this triangle is large, check the procedures. *Do not* assume the DF site is located in the center of a large triangle.

Geodetics

Geodetics is the determination of a site's position through the use of mathematics and the positioning of celestial bodies. Due to the complexity and time involved in the computation, this method normally is used for permanent strategic DF sites. This field manual does not provide the computation procedures.

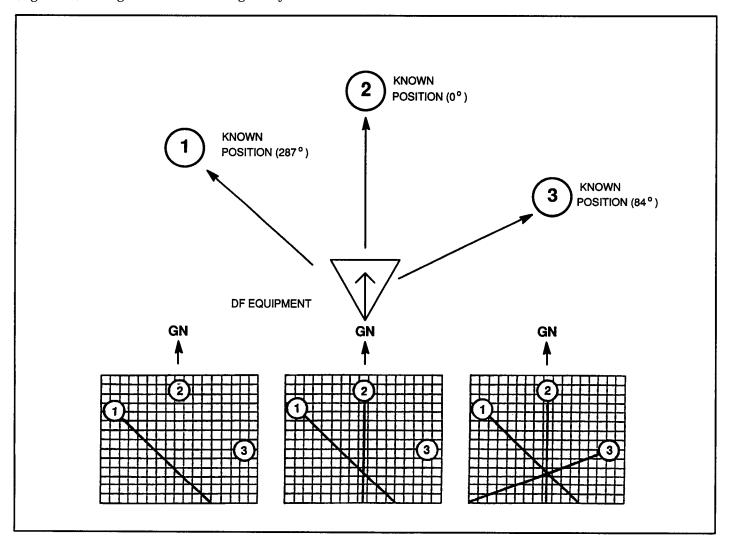


Figure 5-1. Resection.

SITE ORIENTATION TECHNIQUES

Whenever DF equipment is installed in a new location, it is necessary to orient the site's antenna(s) to either true, magnetic, or grid north. What orientation method used depends on the equipment employed and the established reporting criteria for LOBs.

True, Magnetic, and Grid North

True north is the actual direction of the earth's north pole. Magnetic north is the direction of the north magnetic pole. It is indicated by the N (north seeking) end of the compass needle. Grid north is the direction of the vertical grid lines usually found on military maps. The difference in direction between true north and magnetic north, or between true north and grid north, is known as declination (Figure 5-2).

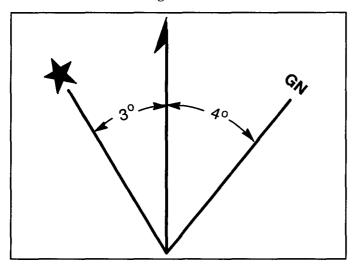


Figure 5-2. Declination diagram.

True North Declination

True north declination is the fixed difference in direction between true north and grid north. True north declination varies in different localities. Actually, it varies at different points on any one map, but on a tactical map the variation is so slight that the average declination can be used without introducing an appreciable error.

Magnetic Declination

Magnetic declination is the angle between true north and magnetic north. In localities where a compass needle points east of true north, magnetic declination is east. Where a compass needle points west of true north, the magnetic declination is west. Where true north and magnetic north are the same, magnetic declination is zero. The magnetic declination in any given locality is subject to gradual change, the amount of which can be calculated from the declination diagram. Annual change is frequently expressed as E or W (east or west) to avoid ambiguity in the change of direction.

SITE CRITERIA

The following site criteria should be used as a guide in selecting either a strategic or tactical DF site location. These are optimum considerations that cannot always be achieved, especially under tactical conditions. For example, a volatile tactical situation, the availability of land in strategic and tactical situations, and many other factors may require some site criteria compromise. Site criteria is as follows:

- The area should be substantially flat for approximately 90 meters from the DF antenna(s). It should also have no more than a gentle slope for at least 180 meters.
- The area should be the highest level area in the vicinity. A site in a valley is usually unsatisfactory.

- wavelengths of the lowest frequency to be used for
- If the DF site must be placed on or near a shoreline, it of interest (Figure 5-3).
- The earth at or around the site should have uniformly high conductivity and moisture content. Areas
 - meet this requirement. Rocky or sandy soil is a poor location for a direction finding site. However, areas having low conductivity are preferable to areas having high conductivity spotted with rock formations, sand, or a varying moisture content.
- Regions where there are abrupt gaps or changes in elevation of the earth should be avoided. Sharp changes in terrain elevation usually indicate the presence of rock or mineral outcropping or underground streams.
- The site should be removed from buildings, wire fences, power or telephone lines, radio antennas, railroad tracks, buried metal conductors (cables and pipelines), sharp ground contour changes (mountains, cliffs, and ravines), chimney stacks, water towers, rivers, lakes, and streams.
- Distances to be maintained between the direction finding site and these obstructions, to minimize their effect on accuracy, are listed in Table 5-1.

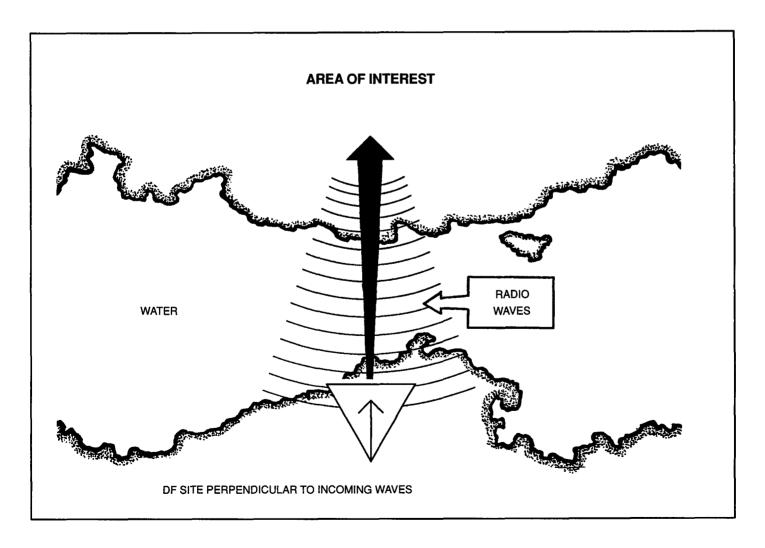


Figure 5-3. DF site located on the coast.

| OBSTACLES | DISTANCE TO BE MAINTAINED |
|---|---------------------------|
| Scattered trees and single small buildings. | 185 meters |
| Wire fences. | 275 meters |
| High cliffs and deep ravines. | 1.6 kilometers or farther |
| Buried metallic conductors. | 275 meters |
| Chimney stacks and water towers. | 450 meters |
| Railroad tracks and overhead conductors (utility lines and antennas). | 450 meters |
| Mountains. | 10-50 kilometers |
| Rivers, streams, and lakes. | 550 meters |

Table 5-1. Preferred distance to be maintained from obstacles.

Strategic Guidelines

The specific guidelines apply for strategic direction finding systems. Some strategic DF sites may not be able to adhere to the following criteria due to environmental, climatic, geographic, or political conditions. In these cases, the NCS of that site is responsible for considering and approving any exception—

- The DF shelter should be located in the quadrant of least interest (where incoming enemy signals are not expected). It should be as far from the antennas as the real estate will permit (Figure 5-4, page 5-6).
- The DF antennas should be positioned in the area of primary interest (where incoming enemy signals are expected). The antennas will be as far from other site equipment such as vehicles, generators, and petroleum, oils and lubricants (POL) as the real estate permits.
- No structure or other equipment should be located closer than 300 feet from the nearest DF antenna or in line of the area of prime interest. All incoming power cables should be buried to a depth of at least 1 foot, beginning a minimum of 500 feet from the site area. Power cables inside the DF antenna array or within 50 feet of the antennas should be buried to a

- depth of at least 3 feet. The direction of buried electrical cables should be indicated by nonmetallic cable signs posted every 200 to 500 feet.
- Strategic DF sites should be declared a restricted area by the commander and posted with nonmetallic signs. Signs should not exceed a height of 3 feet. They should be printed in black letters on a white background. Where required, the signs should be multilingual. Signs should be spaced approximately every 100 feet along the perimeter of the DF antennas. The signs should also be positioned so that they face all quadrants of the DF site.
- Perimeter lights should be placed within 5 feet of each comer of the equipment facing outward. The lights should not exceed 5 feet in height. Electrical wiring for the lights should be kept to a minimum length and buried to a depth of 3 feet.
- Associated equipment such as vehicles, generators, supply shelters, and POL should be arranged so as to lie along a center line opposite the area of primary interest. Vehicles should be parked as far away as possible, with a minimum of 500 feet. They should always be parked in the area behind the quadrant of least interest.

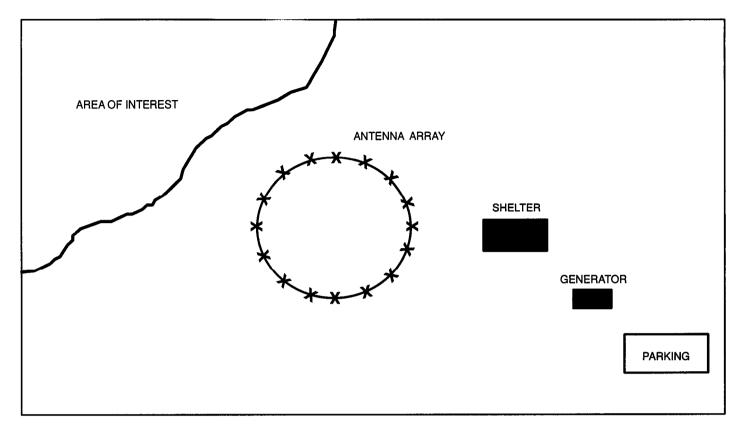


Figure 5-4. DF shelter located outside of antennas in the area of least interest.

Tactical Guidelines

It would be impossible to address every tactical situation in which the platoon leader and team chief might find themselves. Therefore, the following paragraphs will provide general guidelines on tactical site selection and battlefield survival.

A primary consideration in selecting a tactical intercept or DF site location is the ability to receive the target emitter signals from the area of interest. A major consideration for deployment of tactical DF systems is obtaining radio LOS for targets. Radio line of sight is the straight-line path between a transmitting and receiving antenna that is not blocked by the curvature of the earth (Figure 5-5).

Good VHF communications depend on LOS radio wave propagation. Likewise, tactical groundbased DF systems must be deployed within LOS range of the area of interest for intercept and direction finding. Additionally, DF sites must be able to communicate with their NCS.

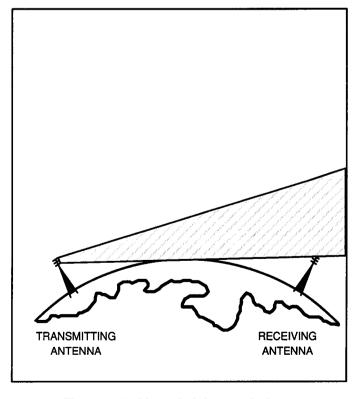


Figure 5-5. Line of sight restrictions.

All tactical intercept or direction finding systems have common requirements that must be met if the equipment is to provide combat information and intelligence to the supported commander. These requirements are—

- Ability to intercept the enemy signal.
- Effective DF baseline.
- Freedom from enemy detection.
- Close proximity to supported elements.

Ability to Intercept the Enemy Signal

Wide variations in the signal strength may exist within relatively small areas. Hills and mountains between the enemy transmitting antennas and the intercept/direction finding equipment limit the quality of intercept and could cause inadvertent DF errors. (Further information

is provided in Chapter 7.) The direction of arrival of the enemy's signal can also be affected by barbed wire, armored vehicles, or other metallic objects that could possibly negate the site's original technical advantages. Enemy VHF signals normally are not affected by the ground on which they travel. However, signals are reflected and reradiated by objects in their wave path. Obstructions in the near vicinity of the site are particularly objectionable. The closer the obstruction is to the DF site, the greater its adverse effect on the site.

Effective DF Baseline

An effective DF baseline must be established. As previously discussed, a direction finding baseline is normally convex or concave to the target area (Figure 5-6).

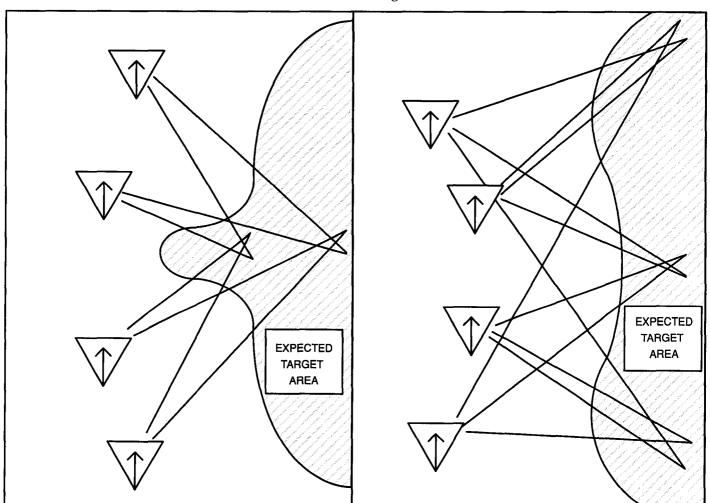


Figure 5-6. Concave and convex baselines.

As illustrated in Figure 5-7, when the tactical DF baseline is approximately 20 kilometers in length, the effective target area depth is approximately 20 kilometers. There are instances when the need for establishing an adequate baseline to locate enemy transmitter antennas requires placing one or more direction finding systems in an undesirable location. If an effective baseline cannot be established, direction finding results may be unsatisfactory.

Freedom From Enemy Detection

Intercept/direction finding personnel should have the freedom to perform their mission during combat to provide current intelligence and combat information. Military intelligence personnel are armed with individual

weapons, but this is not sufficient to engage an enemy combat unit. Therefore, the intercept/direction finding system and the survival of personnel depend on their ability to operate undetected by the enemy. Combat should be avoided if at all possible. Intercept/direction finding equipment destroyed during combat may not be replaced for the duration of the conflict. Platoon leaders and team chiefs should look for good potential concealment when locating a site. They must become experts at camouflage. Locations selected for intercept/direction finding operations should provide the best cover and concealment possible consistent with good reception. However, some amount of signal impairment must be tolerated if the intercept/direction finding system and personnel are to survive in a tactical environment.

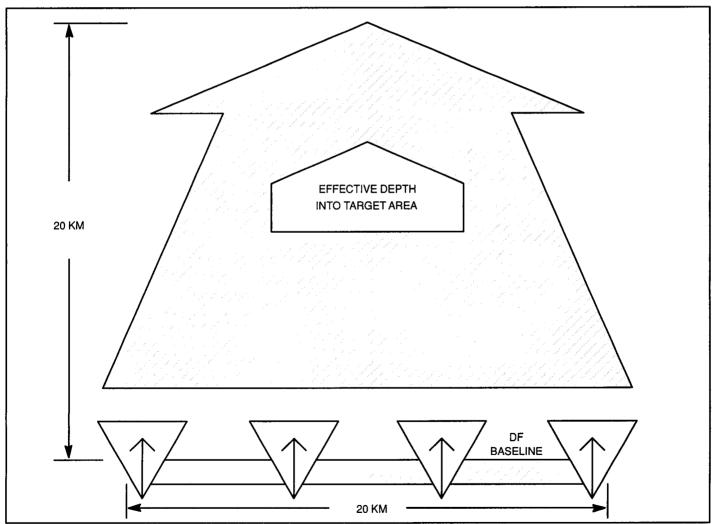


Figure 5-7. Baseline effectiveness.

Close Proximity to Supported Elements

The intelligence and electronic warfare support element (IEWSE) is the MI battalion's liaison to the maneuver brigade. The maneuver brigade commander and staff work closely with the IEWSE to develop an intelligence plan which will effectively integrate electronic warfare (EW) support into the operational scheme. The IEWSE coordinates and resolves terrain siting conflicts of all the MI battalion assets within a supported brigade's sector.

The IEWSE closely coordinates with the S3s of the maneuver brigade and the MI battalion. The IEWSE ensures that essential information on the progress of the maneuver brigade operations is passed to the MI

battalion TOC so timely mission adjustments can be effectively integrated into the maneuver effort.

The company team commander is responsible for coordinating support with neighboring units for the MI battalion assets within an assigned maneuver brigade area. The company team commander, the IEWSE, and the MI battalion S3 work closely together on mission requirements and combat service support for the deployed platoons, so that the deployed platoon leaders can concentrate on mission accomplishment. If a platoon is deployed into a sector and is not part of a company team, the platoon leader must fulfill the role of the company team commander.

SITE SELECTION

Geographic locations of a tactical intercept/direction finding site depend on several factors. The frequency range and propagation characteristics of the enemy transmitters are important. For example, intercept/direction finding operations directed against VHF targets are usually located in a forward area. As previously stated, the intercept/direction finding equipment must be within LOS of the enemy's transmitting antennas. Operations directed against enemy transmitters operating in the HF spectrum can be located well to the rear of the FLOT.

The MI battalion S3, with the technical control and analysis element (TCAE), normally selects the general locations for MI battalion assets. The IEWSE coordinates and resolves the locations with the maneuver brigade staff. The platoon leader coordinates with local units as directed by the S3 and performs site reconnaissance for specific intercept/direction finding site locations. Generally, one primary and several alternate sites are selected. The first consideration in reconnaissance of a site is the terrain. The site must be accessible and relatively flat. The intercept/direction finding equipment must be able to be taken into and out of an area. This must be done in any type of weather and by more than one route when the command to "move out" is given. The site location should provide for rapid, disciplined movement. The movement would

be in conjunction with the result of rapid advances by friendly forces or retrograde movement to avoid capture and compromise or destruction by the enemy.

Advanced planning can simplify site reconnaissance and the selection of primary and alternate sites. A detailed map study of the entire area of operations is part of the planning process. An excellent aid is a modified area map with the contour lines color-coded by elevation. Color coding can be accomplished with felt-tip pens, grease pencils, or crayons. This information is extremely helpful when selecting a VHF site that operates by LOS. Color-coded changes in elevation and high ground areas adjacent to the selected site(s) are readily apparent.

The platoon leader or team chief should also conduct limited bearability tests during the reconnaissance. A bearability test determines how well the intercept/direction finding equipment can receive enemy signals of interest. When conducting the bearability test, the platoon leader must consider the friendly signal density. Heavy friendly signal activity may prevent successful intercept at an otherwise desirable site. There may also be times when a platoon leader or team chief will not have time to conduct a thorough or detailed reconnaissance trip. The combat unit may be involved in very rapid movements and the collection and jamming (C&J) platoon may be forced to move just as rapidly.

When this happens, it is crucial for the platoon leader or team chief to retain as much order and purpose to their movements as possible. The basics of site selection and defense preparation remain constant. They must be considered regardless of the posture of the supported command. If the platoon leader or team chief cannot obtain a proper site location in the given area, the MI battalion can assist and resolve the problem with the maneuver brigade staff through the IEWSE. The company team commander provides additional assistance as directed by the S3.

Once a site location has been identified, the platoon leader or team chief must determine the location of adjacent units. Defensive measures must be coordinated with them. Fields of fire and protective positions must be identified, known, and understood by the platoon leader, team chief, and intercept/direction finding operators. The platoon leader or the team chief should draw up a site defense plan. The plan is placed into effect as soon as the team arrives on site. Additionally, the platoon leader or team chief should take the time to stake the area, indicating exactly where the equipment should be positioned. The platoon leader or team chief normally makes a rough site map and strip map for the equipment driver to follow.

BATTLEFIELD SURVIVAL

Because some intercept/DF systems may be located close to the FLOT and because of their unique antennas, their positions may be observed by enemy forward observers. Considering that attack on these systems by indirect fires is a probability, EW platoon leaders, team chiefs, and intercept/direction finding personnel should be knowledgeable of the enemy doctrine. This knowledge will enhance the survival of the intercept/direction finding systems and personnel.

Threat

The doctrine for the current threat to United States (US) forces calls for the employment of massive amounts of indirect fire. The majority of this fire will be preplanned and delivered as a coordinated part of the overall combat operation.

Artillery fires will be directed by observers operating from advance observation posts. The observers will be located in the forward lines of motorized rifle or tank units or main observation posts. The main observation post for a motorized rifle or tank battalion normally is within 500 to 1,000 meters of the FLOT. Forward observers are equipped with binoculars, range measuring equipment, and communications equipment. They can communicate directly with the artillery firing units. They can also detect targets out to 5 kilometers with their observation devices.

Not only can massed artillery fires against intercept/direction finding systems be called and delivered quickly and effectively, but attack helicopters could be used against intelligence gathering systems. Because of the helicopter's lethality and the skill of pilots in using terrain flight tactics, it is possible that enemy commanders will task these assets to attack US intercept/direction finding systems. US tactical intercept/DF systems must be properly camouflaged and positioned to survive against the enemy.

Camouflage

Camouflage can contribute to the survival of intercept/direction finding systems by reducing the enemy's ability to see the equipment. See is used here because the technology of sensors has advanced parallel with that of weapons. Seeing is no longer strictly a capability of the human eye. Enemy forces use sensors which can detect targets in the ultraviolet wavelength (shorter than visible). They can also detect targets in the broader near and far infrared and radar bands (wavelengths longer than visible). Intercept/DF systems have unique antenna systems, so camouflage techniques must be used to reduce the probability of detection by enemy observers. Sensors attempt to locate and identify equipment by means of radar image, visual image, or temperature change.

The US Army has implemented two basic camouflage concepts that provide protection from detection, either visually or electronically—

- Shape-disruptive painting.
- Lightweight camouflage screen system (LCSS).

Shape-disruptive painting is commonly called pattern painting or camouflage painting. This type of painting provides protection from image intensifying sensors such as the sniper scope and from cameras employing detection film.

LCSSs are usually referred to as garnished screens. They are manufactured as either radar scattering or radar transparent. The garnish of the radar-scattering screen contains minute fibers of stainless steel which inhibit the passage, reflection, and return of a radar signal. These screens are most effective against older, less sophisticated radar equipment. The radar transparent

version is made without these fibers and can be used without altering the effectiveness of the intercept/direction finding system. Obviously, the antennas of these systems cannot be camouflaged without degrading intercept or direction finding accuracy.

Positioning

Certain siting procedures can be followed which reduce the visibility of intercept/DF equipment even though the antennas of these systems cannot be camouflaged. Natural terrain features can be used to keep the antenna from standing out in a silhouette. The systems can be located in front of a hill or tree line, with the antenna below the top of the hill or trees. This reduces the visibility of the station and the antenna by obscuring their outline (Figure 5-8).

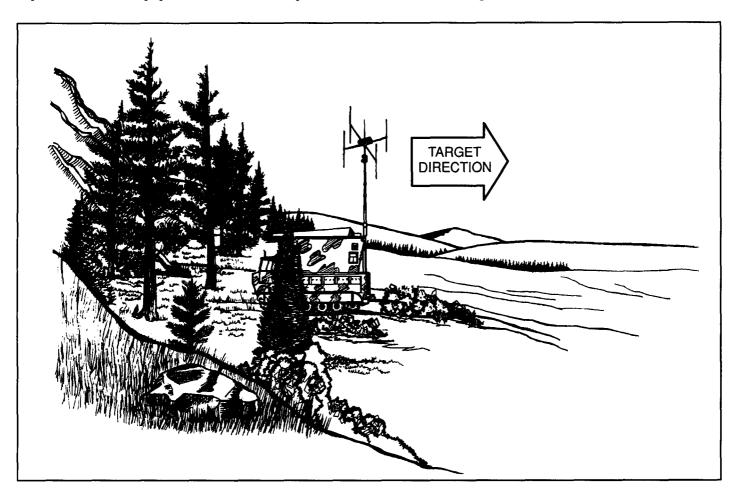


Figure 5-8. Reduced antenna visibility.

To a forward observer, the intercept/direction finding system profile would appear to be a continuation of the profile of the objects around it. Additionally, trees near the antenna can offer certain advantages as well as disadvantages. Foliage can be used to mask the antenna system from unwanted signals. That is, if the equipment is positioned so that the foliage behind and to each side of it extends higher than the antenna. However, foliage located between the antenna and the enemy transmitter antenna has an adverse effect on signal reception. Trees with heavy foliage absorb radio waves; leafy trees more than evergreens. Therefore, intercept/direction finding antennas should extend above the surface of the vegetation level when looking at the enemy transmitter antenna (Figure 5-9).

Redeployment

In a tactical situation, the intercept/direction finding systems must be redeployed frequently if they are to accomplish their mission and survive a hostile environment. This is due to the—

- LOS requirements for VHF intercept and DF. A significant change of the FLOT or the area of interest also requires redeployment.
- Area of interest of the supported division being larger than the area which can be covered by the intercept/direction finding systems. This requires frequent redeployment to adequately cover the desired area.

• Tactical intercept/direction finding systems requirement to stay within LOS of the target areas. This makes them susceptible to visual targeting and the possible detection of their communications equipment. Frequent redeployment reduces the chance of the enemy being able to effectively target and fire on them.

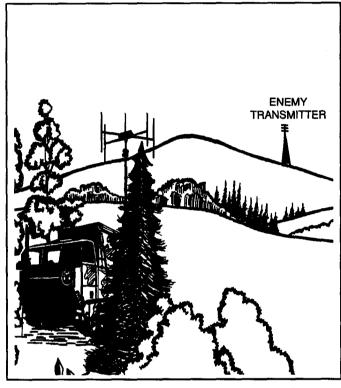


Figure 5-9. *Looking* at the enemy transmitter antenna.

AIRBORNE DIRECTION FINDING DEPLOYMENT

Fixed wing airborne direction finding systems are normally located at an airfield in the corps area. Heliborne systems operate from tactical sites with their parent aviation brigade units. Associated equipment is also located in close proximity to the airfield or tactical site.

ARDF aircraft requires flight patterns that may present the aircraft as targets to hostile forces. Depending upon the terrain, altitude, and distance from the FLOT, the aircraft could be acquired by hostile radar or by the enemy. If the aircraft comes within operational range of the weapon system, they can be attacked by surface-to-air missiles or by airborne interceptors. Due to the classification of this book, survivability tactics will not be discussed.

CHAPTER 6

TASKING AND REPORTING

While strategic and tactical DF share similar basic fundamentals, they differ in other areas. For example, different equipment is used. Strategic direction finding is normally performed from either a fixed or a semifixed posture. Tactical direction finding operates from a mobile posture. There are also disparities between the distances from strategic and tactical DF sites to their net control stations.

Strategic sites are typically located several hundred kilometers from their NCS. Real estate of most allied countries (who host our strategic direction finding nets) is at a premium. Negotiation for land is not an ongoing process. Barring a wartime situation, the likelihood of moving a strategic DF site from one location to another is extremely remote.

Tactical DF sites, normally located within 5 to 15 kilometers of the FLOT, are usually 10 to 15 kilometers from their NCS. Real estate for tactical groundbased DF systems must be coordinated with the supported combat commander. Due to the battlefield environment, frequent moves must be anticipated. Differences in equipment, distances from site to NCS, and deployment all affect tasking and reporting procedures.

COMMUNICATIONS

A prerequisite for direction finding tasking and reporting is rapid and secure communications. Strategic direction finding nets normally use secure telecommunications equipment for tasking and reporting, while tactical DF tasking and reporting are normally accomplished using secure VHF radios. National Security Agency (NSA) approved manual encryption systems are available and are used to secure communications.

STRATEGIC TASKING

Strategic tasking is the assignment of a target or targets to the mission of a strategic DF net control station. Placing a target on the DF mission also includes the priority of the target. The priority determines which target will be tasked to the net in the event two targets of different priorities are active simultaneously. Generally, the mission of a strategic NCS fluctuates with the number of targets on assignment. Targets normally will be added and deleted on a daily basis. Specific information concerning mission assignment can be found in USSID 103.

The purpose of tasking is to determine the location, or in some cases direction only, of a transmitter from the NCS. Tasking may originate from a higher headquarters or it may be local. In either case, requests for direction finding must come to the NCS for action. A strategic

DF NCS is normally collocated with an intercept station. Intercept operators request bearings or the location of suspected or known enemy transmitters. Direction finding operators usually do not search the frequency spectrum for targets of interest. Rather, DF requests are received from intercept operators. The basic terminology commonly used at strategic and some tactical direction finding net control stations is listed in the glossary.

The following functions are presented in a chronological sequence to illustrate how strategic DF net control stations task their DF sites for bearing returns on target emitters:

 The intercept operator requests a bearing or the location on an enemy transmitter.

- The DF controller records the tip-off along with amplifying target information. This includes call signs, frequency, and type of traffic being passed, if any. This permits rapid identification of the target signal.
- The DF controller passes the target information to the DF flash operator.
- The DF flash operator notifies the DF sites of the target and provides tracking so they may obtain a bearing.

This sequence is repeated many times each day. In some strategic nets hundreds of targets are flashed to the DF net daily. Tasking the DF sites to provide a bearing on a transmitter does not complete the direction finding process. To satisfy the intercept operator's request for a location, each bearing from each DF site must be reported to the NCS so that analysis may be performed for reporting.

STRATEGIC REPORTING

Strategic reporting originates at each DF site. The reportable product is a bearing. After the DF site operator determines a bearing on the flashed target, it is returned to the NCS through the report net. The DF operator may be unable to obtain a bearing on some targets. This could be due to natural or man-made co-channel interference, signal strength (weak, fading signal), or target terminating its transmission before the DF operator could obtain a bearing. This would result in the DF site operator submitting a negative bearing return. (Negative bearing returns are defined in USSID 103.)

Regardless of the results obtained at the NCS (whether valid or negative), all bearing returns are collected on each flashed target and the bearings are plotted. Plotting is performed either by hand or computer. Detailed plotting and analysis is covered in Chapter 8. Once the bearings on a target have been plotted and a location has been determined, the location is reported to the requester. This is done to help identify the target as well as to preclude redundant DF requests. Higher headquarters and local policies dictate detailed strategic direction finding reports and reporting procedures. Additional information can be found in USSID 103.

TACTICAL TASKING

As previously mentioned, tactical direction finding operations are influenced by several factors. The most important are the—

- Tactical environment.
- Mission.

It is anticipated that the next war will be unpredictable and fast moving. Groundbased tactical DF equipment may have to be moved several times daily to maintain pace with the supported commander's forces.

The priority intelligence requirements (PIR) and information requirements (IR) of the supported division or corps commander will drive tactical DF tasking. Initial hostilities may find our forces with a limited enemy communications data base available for intelligence gathering operations. Building an adequate data base normally takes several days. The MI battalion TOC at division and the MI brigade TOC at corps

provide intercept and DF guidance during this initial period. The possibility of identified targets being placed on assignment for tactical DF is remote during the initial stages of hostilities.

In most situations, general guidance on target designated frequencies is provided to the intercept and DF operators. The frequencies are those known to be used by specific enemy elements such as artillery, armor, and rocket forces. The frequencies to be monitored for enemy activity depend on the supported commander's PIR and IR. Therefore, initial tactical direction finding efforts are dependent on intercept. A LOB is taken on all intercepted targets. If possible, a location of that transmitter is determined. Once a significant data base has been developed, the MI battalion TOC or MI brigade TOC will then provide more selective DF tasking to its tactical DF assets.

TACTICAL REPORTING

All direction finding bearings in a strategic net are reported immediately to the NCS. In tactical direction finding, the DF team, the platoon operations center, and the TCAE (collocated with the MI battalion TOC) are partners in the DF process.

The voice collection teams in support of division operations normally report LOBs as directed by the MI battalion TOC. As desired by the supported commander, the MI battalion TOC may direct that all bearings be reported immediately to the supported brigade. Normally DF bearings taken by the voice collection teams are reported to the C&J platoon headquarters. Here the transcription and analysis team can perform quick plots if time permits and then, as directed, transmit the bearing results to the TCAE in the MI battalion TOC/supported brigade.

The noncommunications collection team reports all LOBs to the EW platoon headquarters which passes them to the MI battalion TOC. As directed by the supported commander, derived geographic locations are

then passed directly to the brigade or the fire support element.

Voice collection teams assigned to the operations platoon in support of corps report their bearings as directed by the brigade operation center. Normally the teams report their bearings to the transcription and analysis team of the operations platoon. Here, if time permits, they may be quickly plotted and then transmitted to the supported command or the MI brigade TOC. This, of course, will depend on the supported commander's desires. The ARDF systems and the noncommunications collection team in support of corps report their DF results directly to the MI brigade TOC.

At the MI battalion TOC or MI brigade TOC all bearings are consolidated, plotted, and, time permitting, integrated with other intelligence. Using groundbased DF and ARDF results, locations of enemy communications and noncommunications transmitters are determined. These locations are provided to the supported commander on a near real-time basis.

CHAPTER 7

ERRORS

To effectively plot direction finding bearings (or evaluate and report the most probable location of a target area) the person doing the plotting must know about direction finding errors. This information will influence their interpretation of the bearing intersection. Also, the supported commander should understand that due to the

influence of DF errors, enemy transmitter antennas cannot be pinpointed. However, a possible area can be identified where it is *highly probable* that the enemy transmitter antenna is located. This chapter describes common types of errors and their effect on direction finding.

SOURCE ERROR

Source error is a disruption of radio waves introduced at or near the enemy transmitter antenna. It can be caused by a specific type of directional antenna employed. It could also be caused by ground conditions at the antenna site which alter the normal radiation pattern of the antenna. If the DF equipment is farther than 15 kilometers from the transmitting antenna, the size of the source error is usually small. If the DF equipment is closer than 15 kilometers (as with the majority of our tactical DF systems), the source error will cause an inaccurate DF bearing.

PATH ERROR

Path error is caused by deviations of a radio wave from the great-circle path between the transmitting antenna and the DF system. This deviation is caused by the radio wave being absorbed, reflected, reradiated, refracted, or a combination of these factors. The more important sources of path error are—

- Scatter.
- Refraction.
- Reflection.
- Reradiation.

Scatter

In some instances, a small portion of the radio wave entering the ionosphere is scattered instead of being gradually bent and returned to earth. This scattered radio wave may be projected in any direction and is returned to the earth at random angles (Figure 7-1 and Figure 7-2, page 7-2).

The scatter phenomenon accounts for signals sporadically received in regions that are in a skip zone.

Error caused by scatter normally affects strategic direction finding sites but has little or no effect on tactical DF systems.

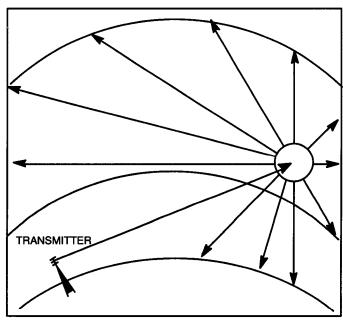


Figure 7-1. Short scatter.

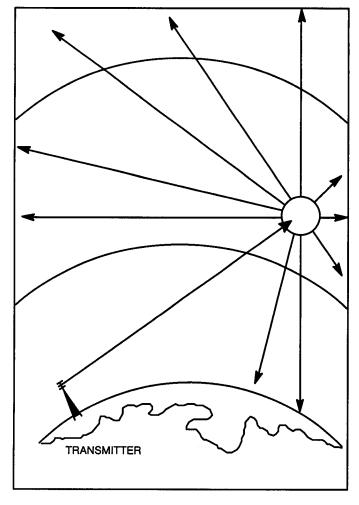


Figure 7-2. Long scatter.

Refraction

Radio waves (electromagnetic in character) are bent or refracted from their normal path when they pass from one medium to another. For example, the velocity of a radio wave over salt water is greater than its velocity over land or fresh water. As a result, when a radio wave crosses a coastline at an oblique angle, as illustrated in Figure 7-3, its direction is appreciably altered. Refraction error is particularly pronounced when either a DF site or the transmitting antenna is near the coast. This effect will also vary with the transmitted frequency.

Reflection

Reflection often causes incorrect DF bearings. A radio wave traveling over or close to cliffs, mountains, or tall buildings will in all probability be reflected (Figure 7-4).

The degree of reflection is immeasurable. It depends upon the obstacle and the frequency of the transmitted wave. Generally, DF errors are greatest from reflection when the reflecting mediums are located in the vicinity of either the transmitter or the DF equipment. Reflection error will affect both strategic and tactical direction finding systems.

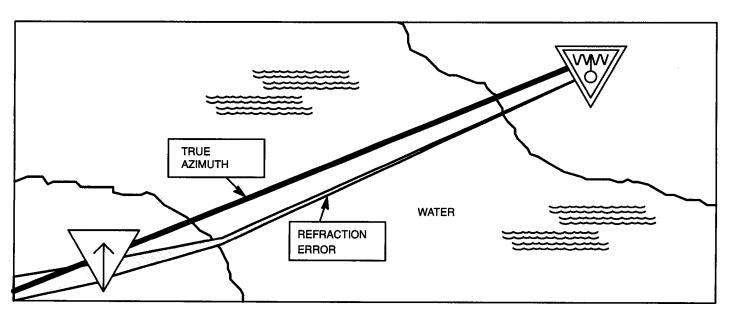


Figure 7-3. False azimuth indicated by refraction error.

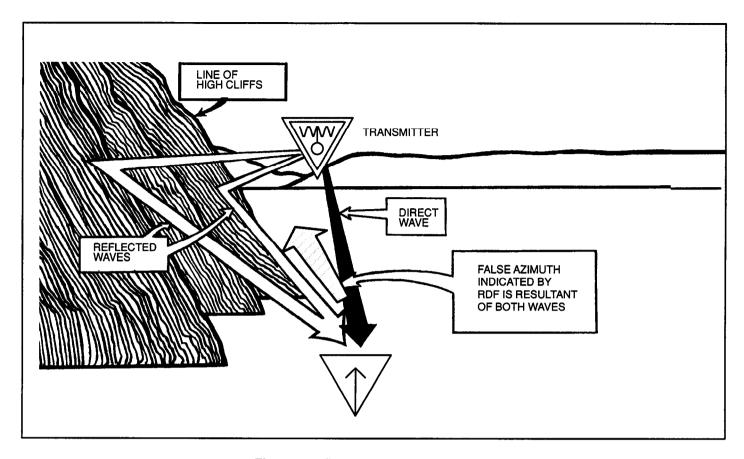


Figure 7-4. Reflection of a radio wave.

Reradiation

This effect occurs mainly because of the reradiation of the radio wave by metallic objects that are resonant at the frequency of the received wave. As a result of reradiation, the radio wave intercepted by the DF equipment may be abnormally polarized. An abnormally polarized signal makes the azimuth reading or bearing very difficult to determine. Reradiation error normally occurs in the vicinity of the direction finding site. Therefore, at strategic and tactical DF sites it is important to adhere. if at all possible. to the site criteria guidelines presented in Chapter 5. Barbed wire, trucks, tanks, other combat vehicles, and metal buildings can cause reradiation error.

POLARIZATION ERROR

Polarization error occurs when an undesired component of a radio wave induces voltage in a DF antenna. This undesired voltage blurs the bearing and makes an azimuth reading difficult to determine. For example, a vertical loop or an Adcock direction finding antenna (Figure 7-5, page 7-4) is designed to receive vertically polarized radio waves.

If the received wave is abnormally or randomly polarized (contains vertically and horizontally polarized

components), the voltage induced by the two components may combine. The azimuth reading on the signal will be difficult, if not impossible, to determine. The effect of polarization error depends upon the ability of the DF antenna (loop or Adcock) to discriminate between the desired component (vertically polarized wave) and the undesired component (horizontally polarized wave) of the received signal. Polarization error is common in most DF operations.

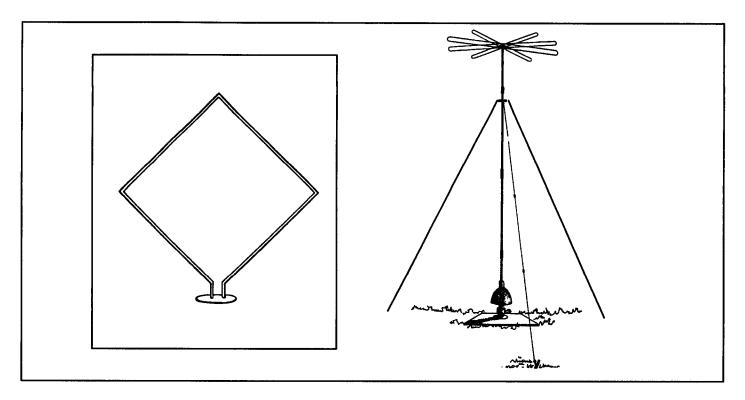


Figure 7-5. Vertical loop and Adcock antennas.

SITE ERROR

Site error occurs in the immediate vicinity of the direction finding site. Site error may be a result of one factor or a combination of several factors. Orientation of the DF system's antennas is extremely important in obtaining maximum DF accuracy. Whenever a direction finding site is setup in a new location, its antennas must be precisely oriented to a known reference point. This produces an accurate measurement of the arrival angle of the wave front. Without this accuracy, the plotting of the reported bearings is of no value. (See Chapter 6.)

Radio waves can be reflected from their original paths by various obstacles. The DF equipment will measure the actual angle of arrival at the DF antenna. Therefore, the DF antenna should be positioned where the wave path is least susceptible to outside influences. The DF equipment then will give the most accurate representation of the true direction of radio wave travel.

Obstructions in the near vicinity of strategic and tactical direction finding sites contribute to site error. The closer the obstruction is to the DF site, the greater its adverse

effect on the accuracy of the site's bearings. Errors caused by obstructions in the vicinity of the site can be eliminated by careful site selection.

Although in many cases the best available site location is far from ideal, definite measures for improving the site from a technical standpoint can be taken. For example, strategic DF sites (which are not substantially flat for at least 90 meters from the DF antennas) can be leveled off with a bulldozer or grader. If it is impossible to level the entire area for 360 degrees coverage, at least those areas within the azimuth arc of primary interest should be flattened. Natural objects such as trees and low vegetation should be cut down or uprooted. Vehicles and personnel not actually engaged in operations at the DF site should be kept away from the antenna system. Tactical DF site improvement is difficult because many compromises must be made for the sake of survivability. However, general site selection guidelines were provided in Chapter 5. They should be followed with discretion when selecting a tactical DF site.

INSTRUMENT ERROR

Instrument error is introduced by the DF equipment itself. Groundbased strategic and tactical DF equipment is designed to perform with a system bearing accuracy of plus or minus 2 degrees. It should be understood, however, that this accuracy is provided within an electronics laboratory where the equipment is unaffected by environmental or human effects. This accuracy provides a point of comparison and should never be used to predict the accuracy of target acquisition.

Normally, DF instrument error is dependent upon the general condition and adjustment of the equipment. A lack of a good maintenance program may also introduce instrument error. The DF operators can contribute to this problem if they perform poor first-echelon equipment maintenance. Various calibrations and adjustments must

be performed at regular intervals. These procedures are described in associated DF equipment technical manuals. They improve equipment performance and result in more accurate DF results.

Daily bearings on known transmitters (check bearings) should be taken at strategic DF sites. These transmitters are commonly called *check targets*. They are used to show if the accuracy or calibration of the DF equipment is acceptable. The check targets must represent the entire frequency spectrum and distances required in DF operation. Any appreciable deviation of the DF bearings (from the known bearing or the bearings normally obtained on a check target) should be investigated immediately.

OPERATOR ERROR

Operator errors are reduced to a minimum when operators have received sufficient training and experience. Newly assigned direction finding personnel must be trained by their supervisor. The DF training program is a supervisor responsibility. Although the service school responsible for training operators provides excellent instruction in many areas, there is no substitute for on-the-job training. Additionally, DF operators must be alert at all times when operating the

equipment. For example, DF operators are required to take bearings on many signals that are weak or fading. Through training, the operator learns to obtain an azimuth on the weak or fading signal when it appears strongest or most stable. Under adverse conditions, an efficient DF operator normally takes several readings and then determines the azimuth by averaging the readings to a mean bearing.

CHAPTER 8

PLOTTING AND ANALYSIS PROCEDURES AND TECHNIQUES

A DF plotter and analyst have an important job. They plot and evaluate the locations of transmitting antennas. This result is then used to determine enemy intentions or uncover enemy locations. At a strategic site, the DF analyst's product may reveal a mobilization for war or a sudden shift in defensive posture. The analyst acts as a catalyst by drawing on the raw data from the field and processing it into a viable product for battlefield commanders or national consumers.

This chapter provides reference to a multitude of procedures and techniques for plotting and analysis. Yet, as the word analysis implies, there is an element of human judgment involved in the process. Choosing the correct technique for the situation and applying the procedures correctly is imperative for mission accomplishment. Without sound plotting and analysis, the best DF equipment in the world would be useless.

DEVELOPING MAP PROJECTIONS

A map that is used for DF plotting and analysis is a graphic representation of a portion of the earth's surface. Although drawn to scale, no map is absolutely accurate since it represents the earth as a plane or flat surface. No portion of the earth's surface can be spread out into a flat plane without some *stretching* or *tearing*. This is illustrated by attempting to flatten either the cap of an orange peel or a portion of a hollow rubber ball. The outer portion must be stretched or torn before the central part will flatten. However, there are some surfaces which can be spread out in a flat surface without stretching or tearing. These are called developable surfaces. Surfaces which cannot be spread out in a flat surface, such as a sphere, are called nondevelopable surfaces.

Three well-known developable surfaces are the cone, plane, and cylinder. If a paper cone is cut from its base to the apex, the conical surface can be spread out in a flat surface without tearing or stretching (Figure 8-1). If such a cone is flattened, any line or curve drawn on it will have exactly the same length as before. In the same manner, if a cylindrical surface is cut from base to base, the whole surface can be rolled out into a plane or a

rectangle (Figure 8-2). In this case, there is no stretching or tearing of any part of its surface.

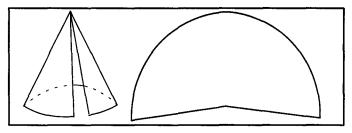


Figure 8-1. Conical surface.

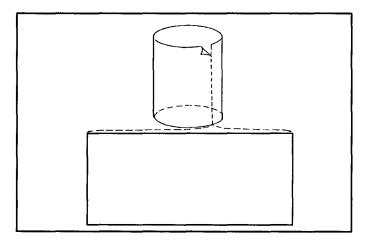


Figure 8-2. Cylindrical surface.

Since the spheroidal shape of the earth cannot be represented on a plane without distortion, a compromise must be made to obtain the most practical features for a specific use. Many different types of map projections have been devised. Each has special merits for its intended use, while compromising other features. The map projections used for direction finding plotting must be a type that a straight line, from a given point, will indicate the true azimuth. Two map projections commonly used for DF plotting and analysis are—

- Universal transverse mercator projection.
- Gnomonic projection.

Universal Transverse Mercator Projection

The universal transverse mercator projection is produced through the use of a cylinder. To project means literally to *throw forward*. A map projection is the network of coordinates picked off the globe and thrown upon a surface. A mercator projection is a mathematical projection very similar to what would be formed by projecting lines from the center of the earth to a cylinder. The cylinder fits around the earth and touches at the equator (Figure 8-3).

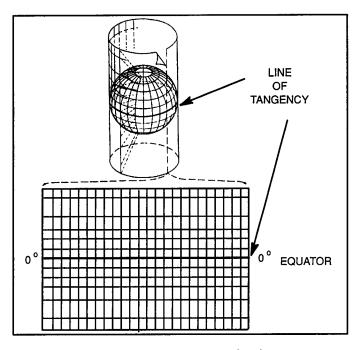


Figure 8-3. Mercator projection.

If the image of the earth could be projected against the cylinder and fixed there, the cylinder could be cut open and laid out flat. This would result in a sheet map that is comparatively accurate in the equatorial region. However, it is more and more distorted as the polar regions are approached. The line of tangency of the mercator projection is a horizontal line—in this example, the Equator. Turning the cylinder across its former horizontal line—that is, transversing it—results in the transverse mercator projection (Figure 8-4).

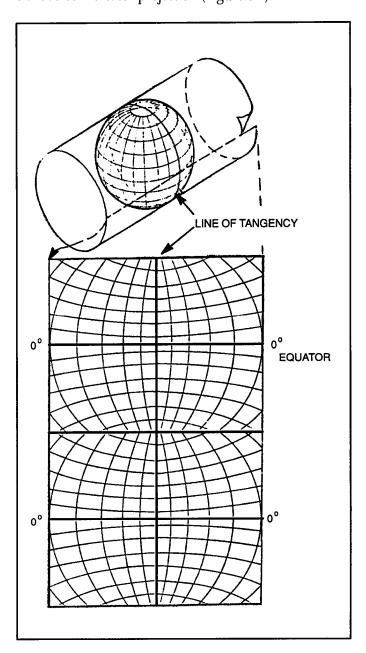


Figure 8-4. Transverse mercator projection.

The significant difference is that the transverse mercator projection uses a longitudinal or a vertical line as its line of tangency in place of a horizontal line (Equator) used in a mercator projection. By choosing several lines of longitude or meridians as lines of tangency, several transverse mercator projections can be constructed. When laid side by side, the entire land mass of the earth is mapped in north-south sections with a minimum of distortion.

The universal transverse mercator projection is the most common map projection used for tactical military purposes. It can be easily oriented for combat situations and readily used with a compass to find a true azimuth from any given point on the map. The UTM system makes it possible to plot from point to point using a straight line called a rhumb line. Advantages of using a universal transverse mercator projection for direction finding plotting are—

- Individual map sheets of the same scale may be joined to forma map of a larger area.
- Direction finding plotting and analysis within 200 miles on either side of the line of tangency can be accomplished with an ordinary protractor (true compass rose).
- There are no north-south plotting limitations.

Gnomonic Projection

A gnomonic projection of the earth is derived by projecting the surface of the globe, from its center, upon a planar surface. The gnomonic projection is the most commonly used map projection system for long-range strategic direction finding plotting and analysis. It is

particularly useful when plotting across great expanses of ocean. This projection method represents all great circles as straight lines. This is the projection's chief merit. This is important in DF plotting and analysis because the shortest route between two points, a straight line, is always a portion of the arc of a great circle. As a general rule, radio waves travel in great circle routes. The limitation of producing a gnomonic projection is that only a quarter of the globe, or 90 degrees, can be projected. Distortion beyond 90 degrees becomes severe and renders the projection useless for direction finding purposes.

Advantages of using a gnomonic projection for strategic direction finding plotting and analysis are as follows:

- Radio waves will appear as straight lines throughout the projection. There are no distance limitations imposed; only that of the area encompassed by the map.
- Strategic direction finding sites need not be located within the boundaries of the projection. As long as you know the latitude and longitude of the DF site, you can compute for the points where the site's bearing will enter and exit the projection.

Due to the amount of distortion in this type of projection, protractor plotting is limited to those areas located within 4 degrees of the point of tangency. Most strategic sites are established on a baseline located outside of the 4 degree area around the point of tangency. Bearings from these sites (as well as those sites located off the chart) require mathematical correction to compensate for map distortion. Mathematical correction methods are presented in Chapter 9.

PLOTTING

The following terms are commonly used in strategic and tactical plotting facilities:

- Line of bearing.
- Cut.
- Fix.

A line of bearing is the angular measurement of a radio wave in degrees from a given reference (true, magnetic, or grid north) (Figure 8-5).

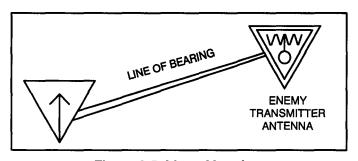


Figure 8-5. Line of bearing.

A cut is the point of intersection of two DF LOBs (Figure 8-6).

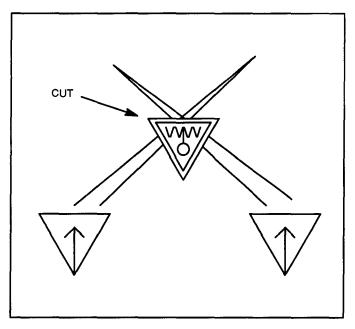


Figure 8-6. Cut.

A fix represents three or more DF plotted bearings that intersect (Figure 8-7).

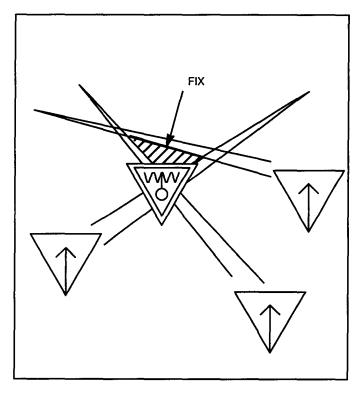


Figure 8-7. Fix.

Plotting a Line of Bearing

The simplest method of plotting a bearing is with a protractor and straightedge. Point A in Figure 8-8 represents the known location (by grid coordinates) of a DF station. This is entered as a tick mark (') on the map or overlay. In the example, the index of the protractor is placed to coincide with point A and is accurately aligned along the north-south grid lines by using dividers or parallel rulers. Either true or grid alignment may be used. Magnetic orientation is not used. While grid and true north reference lines are corrected throughout the map, magnetic declination is accurate only at the center of the map. As the scale of the UTM increases so does the inaccuracy of the magnetic orientation. Plotting at distances greater than 200 miles along an east-west axis will require a gnomonic projection. This is because the UTM becomes too distorted. (This includes combining several UTM maps.) The bearing taken by the DF station is measured in degrees from grid north and is indicated by another tick mark at the appropriate degree on the protractor. The protractor is removed and the straightedge aligned along two tick marks. The bearing is then plotted by drawing a line along the straightedge from the station location through the degree tick marks. Extend the line a sufficient length into the target area. The enemy's transmitting antenna is probably located along this line.

NOTE: The protractor may be aligned with a grid or true north, depending on DF equipment or reporting criteria.

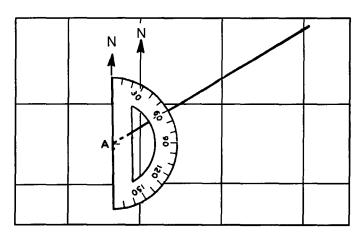


Figure 8-8. Plotting a bearing.

Plotting a Cut

Using the method outlined above, the bearing from a second DF station is plotted. The intersection of the two plotted bearings is identified as a DF cut (Figure 8-9).

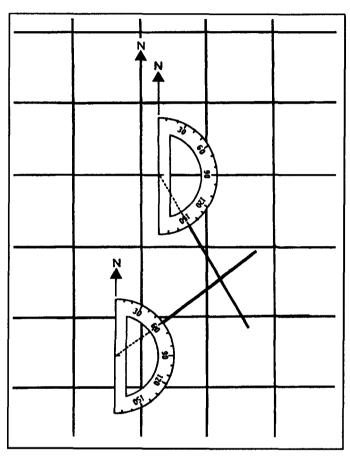


Figure 8-9. Plotting a cut.

Plotting a Fix

If three or more direction finding sites are arranged along a baseline, the protractor may still be used. As illustrated in Figure 8-10, DF sites A, B, and C are plotted and have reported bearings of 60, 90, and 130 degrees respectively.

Again, the protractor and straightedge may be used to successively plot the bearings of each DF site at its map location. The lines may be extended to form a small triangle. They may join at a point if the fix is perfect. Figure 8-11 illustrates a perfect fix. However, a perfect fix is extremely rare and suspect.

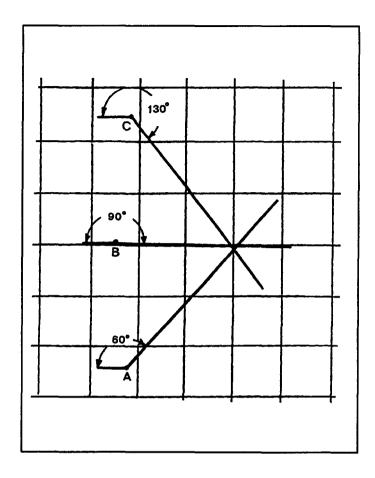


Figure 8-10. Plotting a DF fix.

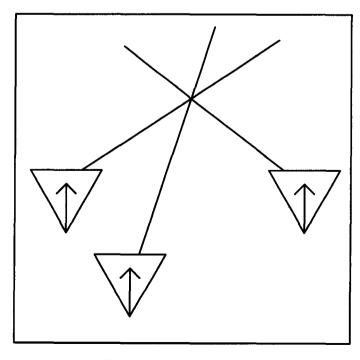


Figure 8-11. A perfect fix.

Map Size

The size and scale of the maps used in DF plotting and analysis depend on—

- Whether the direction finding effort is strategic or tactical.
- Range of the bearings to be plotted.
- Length of the baseline.

As previously mentioned, a gnomonic map projection is normally used for strategic plotting and analysis. The universal transverse mercator is used for tactical plotting and analysis. The range of the bearings or the distance from the DF sites to the target area obviously will affect the size of the plotting map. In a tactical situation, perhaps more than one map sheet may have to be joined with another to plot the DF sites' bearings. This is caused by the DF baseline being too long for a single map sheet. It could also be caused by the target area being too deep for a single map sheet. An ideal DF baseline should be the same length as the expected depth of the target area. Using a gnomonic map for strategic plotting, it is possible to have DF sites located off the map and still be able to plot their bearings. However, in

a tactical situation this is not possible. The map size has to allow for all sites to be located on the map projection.

Plotting and Analysis Centers

The plotting procedures described above, while completely valid in terms of accuracy, are somewhat slow and laborious. A DF plotter/analyst would find it difficult to plot all the DF bearing returns using a protractor and straightedge because of the following:

- Advancement of direction finding state of the art.
- Greater number of bearings reported by individual DF sites.

Accordingly, DF plotting and analysis centers with in-depth analysis capabilities have been established. In these centers, plotting boards are used. They have the DF sites LOBs represented by strings which may be pulled out and lined on calibrated map-edge scales. The plotter/analyst simply notes the DF site, the reported bearing, and the calibrated edge scale for the particular reporting site. When the string is pulled out and aligned along the reported bearing on the appropriate map-edge scale, the bearing is plotted. Additional DF sites are plotted in the same manner. The intersection of bearings determines the most probable target location.

FIX ANALYSIS

Plotting and fix analysis is the practice of determining the best place to put the target coordinates and from that point, an area in which the target may conceivably be located.

Thus far, ideal plotting and analysis conditions have been discussed. In the practical application of DF plotting and analysis, the returned bearings are carefully evaluated by the plotter/ analyst. They determine the most correct or most probable location or best point estimate (BPE) of the target of interest. A perfect fix, with three or more bearings intersecting at an exact grid location, is rare. When plotting and analyzing, the plotter/analyst has many factors which must be considered.

The process of plotting and fix analysis is substantially influenced by several human factors in the evaluation of the DF site's bearings. As the plotter/analyst's experience builds and reported fix locations are confirmed by enemy contacts or other reliable means, the plotter/analyst will concede increasing credibility to one DF site over another. In other words, each DF site develops a *track record*. A change of DF operators at a particular DF site can also influence the analytical process. In spite of the standard assignment of reliability indicators, manual plotting and fix analysis is still greatly influenced by these human factors.

The DF plotter/analyst must also be aware of DF equipment characteristics. For example, the design characteristics of some direction finding equipment are plus or minus 2 degrees. (Different DF equipment has different accuracy ratios.) This means that a bearing return is not a straight line. It is an ever-widening,

fanlike path. There is a high probability the transmitting antenna is located within this path. The center line of path A (Figure 8-12) has the highest probability that the target is located somewhere along this line. As the distance from the center line increases towards B, the target location probability decreases.

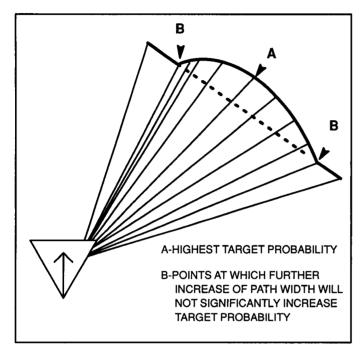


Figure 8-12. Bearing path.

Path width, or B, is determined during the design and testing of DF equipment. It is normally expressed as an angle, in degrees, based on mathematical calculations. Therefore, to determine the specific target area it is necessary for the bearings from two or more DF sites to intersect. A DF plotter must keep in mind that when the bearings intersect (Figure 8-13) the probable target area along each path is limited. It is limited to the width of the intersecting bearing paths at the point of intersection.

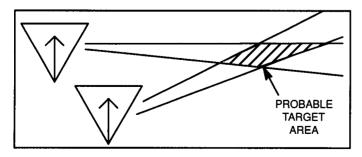


Figure 8-13. Intersecting bearing paths.

The direction finding fixes discussed in this chapter have all been *perfect* with all site bearings intersecting at an exact grid location. Of course, such a fix seldom occurs because of the inherent errors in DF operations. Significant contributions to direction finding inaccuracies are the—

- Continually changing electromagnetic environment of each DF site.
- Inherent equipment error.
- Operator error.
- Natural and man-made objects around the transmitting/receiving antennas.

Cut

It is possible to evaluate a cut. Obviously, such a plot is not normally used in DF reporting unless an extreme, high priority condition exists. However, the cut is frequently used at strategic DF sites for general distance or area observations and optimum antenna selection for intercept. A cut is not practical to obtain a fix point; therefore, an area must be determined in this analysis. Such a fix area is illustrated in Figure 8-14. If each individual bearing is represented by a fan-shaped figure centered about the bearing, it may be stated that there is a probability that the true bearing lies within this fan. This is called a fan bearing.

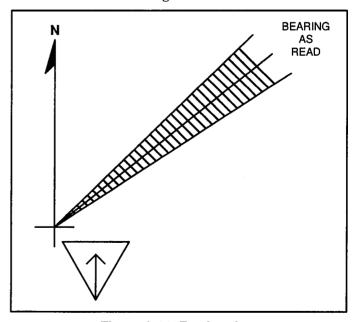


Figure 8-14. Fan bearing.

A two-station fan fix is shown in Figure 8-15. If each fan represents the limits within which there is a probability of 50 percent (1 to 1 chance) that the bearing lies there, then the cross-hatched portion represents the area in which there is a probability of 25 percent (1 to 3 chances) that the transmitter antenna lies there. Each site has its own standard deviation (SD). This is a measurement of the reliability of the sites' bearings based on the historical data base. (For more information on SD, see Chapter 9). By increasing the size of each bearing fan to the width of the DF site's SD, it may be estimated that the probability is 90 percent (9 to 1 chance) that each bearing lies within the fan, and that there is a probability of 81 percent (4 to 1 chance) that the transmitter antenna lies within the cross-hatched area. If the site SD is not available, expand the bearings to a total fan width of 10 degrees.

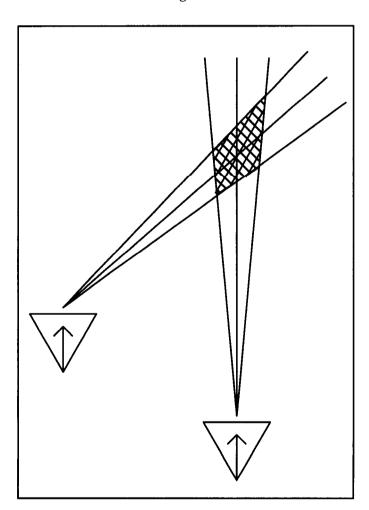


Figure 8-15. Two-station fan fix.

Extension of the two-station fan fix into fixes of three or more stations becomes very complicated and leads to ambiguous results. Even for a two-station fix, the area frequently becomes excessively large for any reasonable probability. However, by more refined mathematical considerations involving the theory of probability and the theory of least squares, it is possible to determine the size, shape, and location of a minimum area with a stated probability that the transmitter antenna lies within it. This applies to any number of DF sites involved.

Three-Station Fix

When plotting three bearings, one of three possible events occurs—

- No-fix situation, where a fix solution is not feasible.
- Perfect fix situation, where all three bearings intersect at a single point.
- Error triangle situation, where an area of probability is formed.

No Fix

As illustrated in Figure 8-16, a fix solution is not always feasible. This occurs more frequently with three-station plots than with plots of four or more stations. In many situations, the analyst will be cautious and will choose to report a no fix rather than risk reporting an erroneous location. For example, a triangle that encompasses a 3 by 3 grid-square area would not help to locate a mechanized infantry company. Due to the relatively low priority and speed of the unit, the plotter or analyst would consider the target information too inaccurate for use. However, if the same triangle was applied to a company transporting nuclear missiles, the target information (regardless of its accuracy) may be deemed of such importance that it justifies an inexact fix report. In such situations, use of each site's SD is helpful. Not all tactical sites will have these statistics available, but for those that do, such statistics will prove useful during analysis. Figure 8-17 illustrates how a large triangle can be reduced using SD. The bearing lines for the two sites are adjusted by applying twice the SD of each site. This produces a workable triangle for analysis.

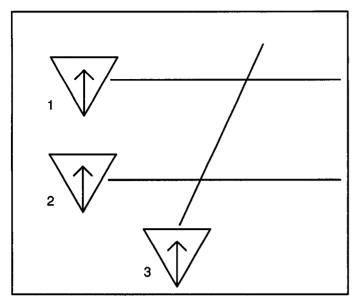


Figure 8-16. No fix.

Perfect Fix

Figure 8-18, page 8-10 illustrates a perfect fix situation. However, this plot could misdirect analysis. Such a fix does not guarantee that the point of intersection represents the exact location of the target transmitter antenna. Conceivably such a fix could be obtained if two or more bearings were in error.

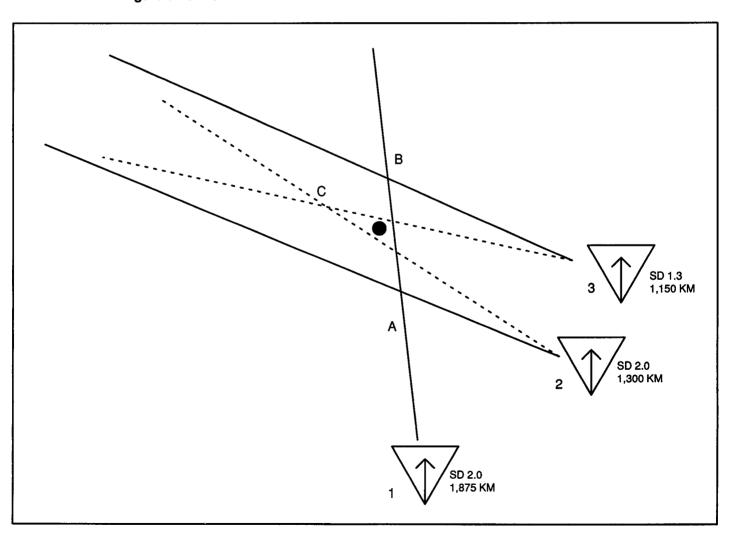


Figure 8-17. Using site SD to reduce triangle.

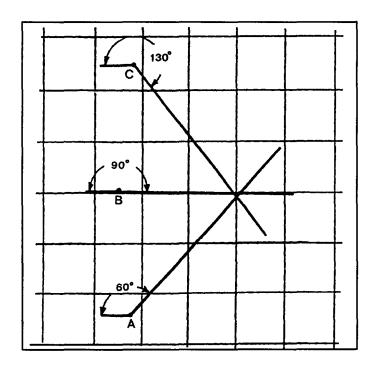


Figure 8-18. Perfect fix.

Error Triangle

This is the more usual type of three station bearing intersection found in DF analysis. It is sometimes called *triangulation* because the bearings intersect to form some type of triangle. There are many different methods employed to analyze a triangle to determine a fix point. These are—

- Bisection of the medians of a triangle.
- Bisection of the angles of a triangle.
- Steiner point.
- Visual inspection.
- Modified visual inspection.

NOTE: Strategic DF nets will most often use the visual inspection method. Prior to using this method, however, a reliable direction finding site data base must be established. The exceptions are those DF networks that use computers to do the plotting. As our dependence on automation grows, the computer assumes many of the duties once accomplished by a competent plotter. However equipment and power outages necessitate that every DF plotting facility train DF plotters how to manually plot using one of these methods.

Bisection of the Medians of a Triangle. To evaluate a fix using this method, the plotter simply draws a line from the midpoint of each median to the opposing angle. As illustrated in Figure 8-19, a line is plotted from the midpoint of line BC to angle A. Another line is plotted or drawn from the midpoint of line AC to angle B. The last line is drawn from the midpoint of line AB to angle C. The error triangle solution or probable target emitter location is the point where the three lines intersect or A'. This method should only be used on a case by case basis, where the immediacy of a report precludes the use of visual inspection or the construction of a steiner template.

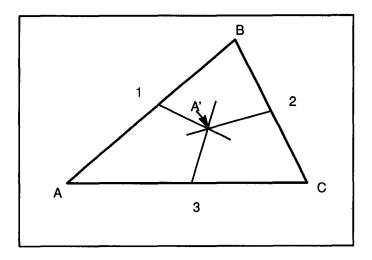


Figure 8-19. Bisecting the medians.

Bisection of the Angles of a Triangle. Determining the error triangle solution by bisecting the angles of the triangle is illustrated in Figure 8-20. The plotter must first determine the degree of each angle. Then each angle must be bisected. In Figure 8-20 the bisecting lines are drawn from angle A to point 1, from angle B to point 2, and from angle C to point 3. The solution (B') is the point where the three lines intersect. Conditions mentioned in the use of the bisecting the medians method must also be applied to the use of this method.

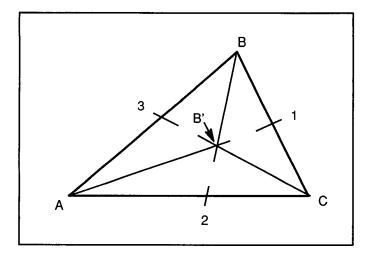


Figure 8-20. Bisecting the angles.

Steiner Point. The steiner point is the point at which the sum of its distances from the vertices of the triangle is at a minimum. The steiner point method is only used when speed and ease of analysis are required. The steiner point is located at the intersection of three lines drawn from the vertices of the triangle and making an angle of 120 degrees from each other. In an obtuse triangle having an angle of 120 degrees or greater, the vertex of that angle is the steiner point (Figure 8-21). For the remaining triangles having angles less than 120 degrees, the most practical method to place the steiner point is by constructing a simple equilateral template from transparent material.

To construct a template, draw a circle on a sheet of clear plastic. Ensure the circle is large enough in size to encircle your error triangles. Make a small hole in the exact center of the circle. Etch three lines from the center hole, exactly 120 degrees apart, to the outer circumference of the circle, thus trisecting the circle. Another method of template construction is to etch an appropriately sized equilateral triangle on a sheet of clear plastic. Then etch lines on the template from the vertices and punch a hole at the intersection. Either method of construction is equally accurate. When the template is completed, place the template over the error triangle formed after the three bearings are plotted. Rotate the template and align it until each of the 120 degree etched lines passes through each vertex of the triangle.

Mark the location (C') as illustrated in Figure 8-21. Place a pencil through the hole in the center of the template and mark this area. This is the steiner point or fix point. This mark is reported by grid coordinates as the most probable target emitter location.

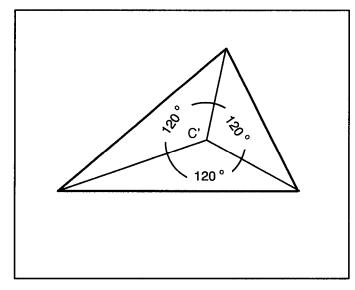


Figure 8-21. Steiner point.

Visual Inspection. Essentially, the visual inspection method involves analyzing all available data affecting the fix area and selecting a fix point based on all factors. The visual inspection method is the only analytical method approved by the United States Army Intelligence and Security Command (INSCOM) for use in strategic and EAC manual plotting analysis. This is the only method which applies an analysis of all five factors affecting DF capabilities. All of the factors may not be used in an analysis. The number of factors used depends on the unit mission, standing operating procedures (SOP), and equipment. Although this method consumes more time than other methods, it is the most accurate method available. The factors are as follows:

Angles of bearing intersection. More consideration is given to bearings that intersect at or near right angles. This is because bearings at a 90 degree angle of intersection result in a smaller linear deviation than any other angle of intersection. As an immoderate example, we will use the range of strategic DF (Figure 8-22, page 8-12). A bearing intersection at a distance of about 375 nautical miles (Nm) from two DF sites with an angular deviation of about plus or

minus 5 degrees from a right angle formed by bearings A and B represents about 52 nautical miles of linear deviation. At the same distance, an angular deviation of plus or minus 5 degrees from a 27 degree angle formed by bearings A1 and C represents about 149 nautical miles of linear deviation. In equilateral triangles, the fix point is placed in the center of the triangle.

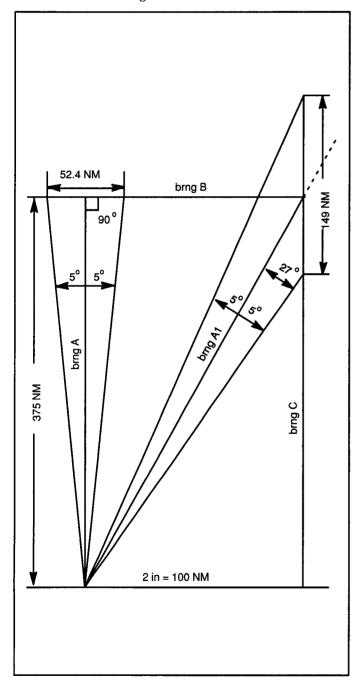


Figure 8-22. Bearing linear deviation.

Bearing classification. Some DF site operators measure the confidence factor (also known as degree of certainty or validity) in bearing accuracy. This measurement can be indicated by confirmed and doubtful tags on bearing returns. The confidence factor is produced by the DF operator. A confirmed bearing return indicates that the operator is sure the correct target has been acquired and the bearing is stable. A doubtful return signifies that either the operator is not sure it has been acquired or the bearing was not stable, or both. The DF plotter/analyst would trust a confirmed or high number bearing return more than a doubtful or low numbered bearing return.

Terrain. Since strategic DF systems measure the arrival angle of electromagnetic sky waves, terrain features have little effect on the measurement of the wave

Known reliability of the DF site based upon past performance. Standard deviation measures the reliability of each DF site. Systematic error (SE) measures the accuracy of each DF site. Together, these statistics provide a qualitative measure of each DF site's potential (in comparison to the other DF sites) by reflecting the average accuracy of the site's DF results. A site with a low SD should normally be more reliable than a site with a high SD. Therefore, more consideration is generally given to sites with lower SDs. If a DF site usually has a low SE, and then suddenly the SE fluctuates considerably in either a positive or negative direction, the bearings from that site must be considered less reliable until the SE is stabilized.

Distance that a radio wave travels before reaching the DF site. The more distance between a DF site and the target, the less accurate the bearing returns are likely to be. In plotting and analysis, a greater confidence would be placed on sites closer to the target area.

Modified Visual Inspection. Due to the high mobility of most tactical DF systems, some of the factors used in the visual inspection method cannot be analyzed. In tactical analysis, angles of intersection, terrain, and bearing classification were the most important factors.

Therefore, the plotting method is modified to reflect tactical considerations. The modified visual inspection method is dependent on five factors as follows:

- **Angles of bearing intersection.** Naturally, tactical systems have less range, but the linear deviations are still appreciable.
- Bearing classification. In some tactical systems the
 bearing confidence factor (or bearing validity) may
 be measured by a numbering system (or LOB quality
 factor). The higher the quality factor, the better the
 bearing return. This factor is dependent on the
 amount of integration time of the DF system, the
 amount of time the target stays active, and the
 amount of bearing deviation in the bearing calculations. The numbers may also indicate the number
 of samplings (shots) taken to obtain a mean bearing.
- Terrain features between the DF site and the target, at the target area, and around the DF site. With the exception of Quasi-Doppler and ARDF systems, terrain analysis is a very important factor when using tactical systems. Terrain features have a much more important role in tactical analysis. There are two parts to this analysis—the terrain between the DF site and the target and the terrain at the probable fix area.

NOTE: Terrain features between the DF site and the target, such as mountains and lakes, can deter the arrival angle of the bearing at the DF site. Therefore, the plotter/analyst would not place as much confidence in such a bearing return. Using the modified visual inspection method to produce the most probable target location, the DF plotter/analyst must examine the map in detail. When determining a fix point, the plotter/analyst must use common sense. The plotter/analyst must study the geographic qualities of the fix that have been produced. Should the indicated location be in the middle of a large lake, it is unlikely that the transmitter antenna has been accurately located. If the most probable fix location is atop an inaccessible crag or butte, the DF plotter/analyst must once again apply a little logic. The terrain features adjacent to the

indicated location must again be examined. Transmitter antennas that usually serve a command or headquarters are likely to be located where such troop units would logically be stationed or encamped. Camps, trails, roads, water supplies, and similar terrain features must be evaluated when formulating the most probable fix location.

- **Site statistics.** Because of the tactical site's mobility, site statistics may not be available. With the exception of some EAC DF systems, site statistics are not a major factor in tactical DF plotting and analysis.
- **Distance**. Distance has a role in tactical plotting and analysis but, due to the short to medium range of targets, distance may not have as much of an affect as it does in strategic plotting and analysis.

Modified Techniques

Methods similar to those explained in the *three-station fix* section of this chapter can be used for fixes of four or more bearings. Only visual and modified visual inspection analysis implements the myriad of factors involved in the fix. All other methods are deficient in the area. For intersections resulting in an *error quadrilateral* (a polygon of four sides), the following methods could theoretically be used—

- Intersection of the two diagonals of the error quadrilateral.
- Intersection of the two diagonals of the quadrilateral formed by the steiner points of each of the four triangles of the error quadrilateral.
- Steiner point of the triangle formed by the three steiner points of the three triangles of the error quadrilateral.

Obviously, the preceding methods are time consuming and difficult. The visual and modified visual inspection method are easier, faster, and more accurate. The analytical technique is the same as described in the *three-station fix* section of this chapter. The following illustrations (Figures 8-23 through 8-34, pages 8-14 through 8-17) show the complete visual inspection process.

Visual Inspection Process

Angle of bearing intersection. In Figure 8-23, site 2 and site 3 bearings intersect at a near right angle. This factor would influence the analyst to place the target plot in that corner of the fix area.

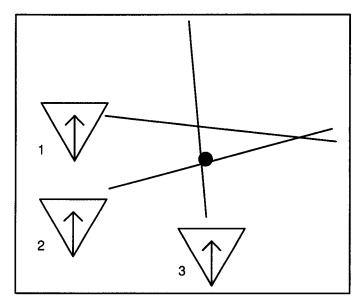


Figure 8-23. Angle of bearing intersection.

Distance factor. Distance is the influencing factor in Figure 8-24. Due to the distance of site 1 from the target, the analyst places more emphasis on the intersection of bearings from sites 2 and 3.

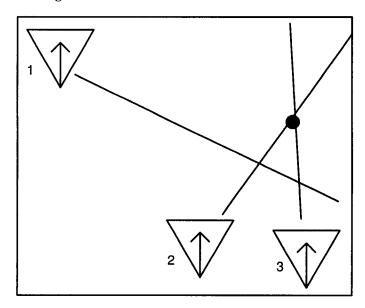


Figure 8-24. Distance factor.

Bearing classification. In Figure 8-25, site has a *doubtful* bearing return. The analyst would put more emphasis on the *certain* bearing returns of sites 2 and 3. The analyst places the fix point closer to the intersection of the certain bearing returns.

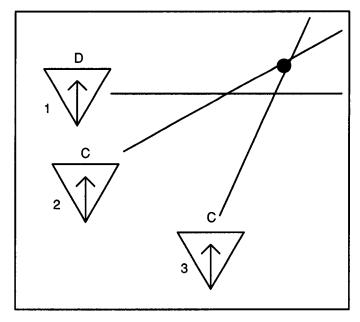


Figure 8-25. Bearing classification.

Equilateral triangle. When bearings form an equilateral triangle (as shown on Figure 8-26) and no other factors affect the analysis, the analyst would place the fix point in the exact center of the triangle.

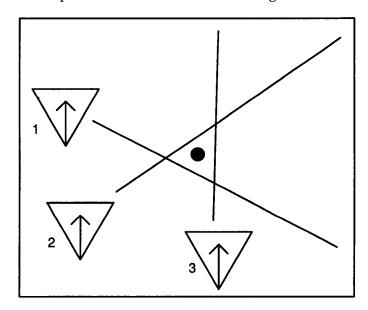


Figure 8-26. Equilateral triangle.

Site reliability. In Figure 8-27, site 3 has a high standard deviation. In this case, the analyst would place more emphasis on the bearing intersection of the lower SD sites (sites 1 and 2). The analyst would move the fix point to that part of the fix area.

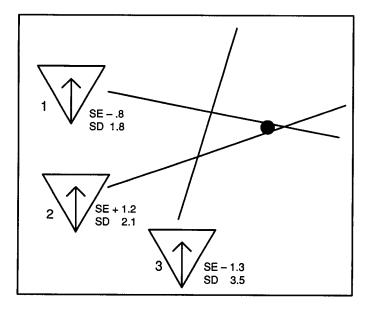


Figure 8-27. Site reliability.

Terrain. In Figure 8-28, a mountain interferes with the accuracy of site 1. Therefore, the analyst would place more emphasis on the intersection of bearings from sites 2 and 3, placing the fix point in that part of the fix area.

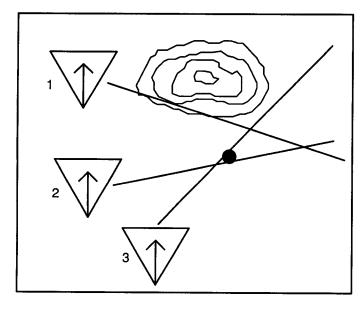


Figure 8-28. Terrain factor.

Up to this point, the fix analyst examples have been based on simple three site (station) triangulation with only one factor affecting analysis. In most DF nets, four or more sites are used to enhance productivity and accuracy. Numerous factors affecting analysis may be encountered in the selection of a single target's fix point within the probable fix area.

In example A (Figure 8-29), the best angle is formed by sites 2 and 4 (the most reliable sites). Site 1 has a doubtful bearing return and has a high SD. The bearing return from site 3 is probably not accurate because of the mountain. Considering these factors, the DF analyst would select a fix point closer to the bearing intersection of sites 2 and 4.

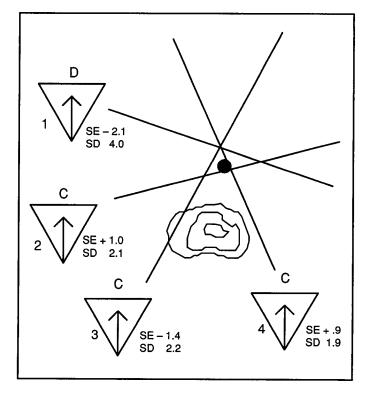


Figure 8-29. Example A.

In example B (Figure 8-30, page 8-16), although sites 1 and 3 form the best angle of intersection and are the most reliable sites, placing the fix point in that part of the fix area would put the target in the lake. Since the target is known to be a groundbased entity, the analyst would move the fix point onto the land.

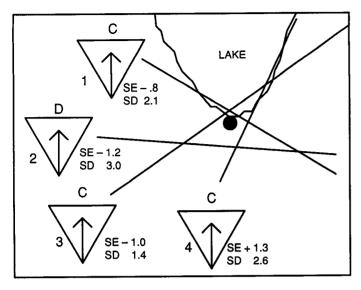


Figure 8-30. Example B.

In example C (Figure 8-31), site 2 has a doubtful bearing return and site 3 has a high SD. The best angle of bearing intersection is formed by sites 1 and 4. The analyst would place more emphasis on the best angle; plotting the target closer to the best angle of bearing intersection.

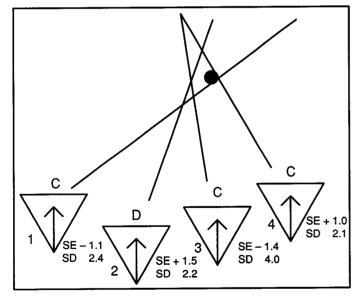


Figure 8-31. Example C.

In example D (Figure 8-32), site 4 has a doubtful bearing return and the highest SD. The analyst would rely more on the bearing returns of the other sites. Since sites 1 and 3 form the best angle of bearing intersection, the fix point would be plotted in that part of the fix area.

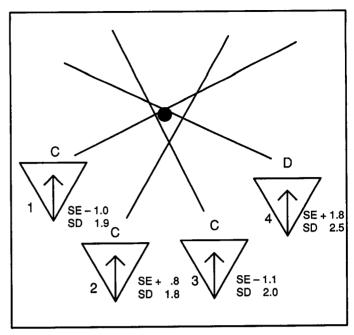


Figure 8-32. Example D.

In example E (Figure 8-33), site 1 has a doubtful bearing return and a high SD. Site 5 is near a mountain, which could cause some distortion. The best angle of bearing intersection is formed by the remaining three reliable sites. Since the analyst would not totally disregard the bearing returns from sites 1 and 5, **the** plot would be placed as illustrated to allow for their influence.

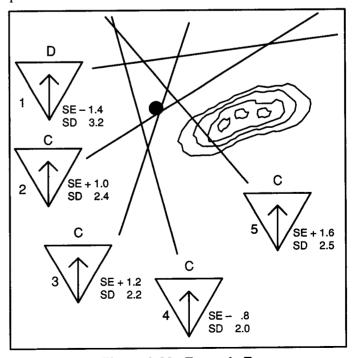


Figure 8-33. Example E.

In example F (Figure 8-34), the best angle of bearing intersection is formed by sites 2 and 4. Based on their SD, these sites are also the most reliable. Sites 1 and 3 have doubtful bearing returns. However, as indicated by the plotted bearing returns from the other sites, site 1 and site 3 bearings are within the area of probability and should be given some consideration. The analyst would shift the fix point from the best angle of intersection in order to include some influence from these sites.

In example G (Figure 8-35), a bow tie is created in the plot. The fix point is shifted toward the bearing generated by site 1 because of the reliability. Applying the secondary bearing (adding or subtracting twice the SD) to the configuration would move bearing 2 toward the area indicated by the other bearings. If twice the SD of site 2 had not entered the indicated fix region, the bearing would have been discarded as a wild bearing.

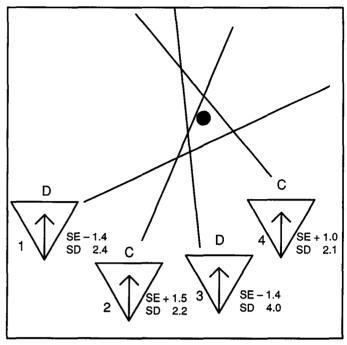


Figure 8-34. Example F.

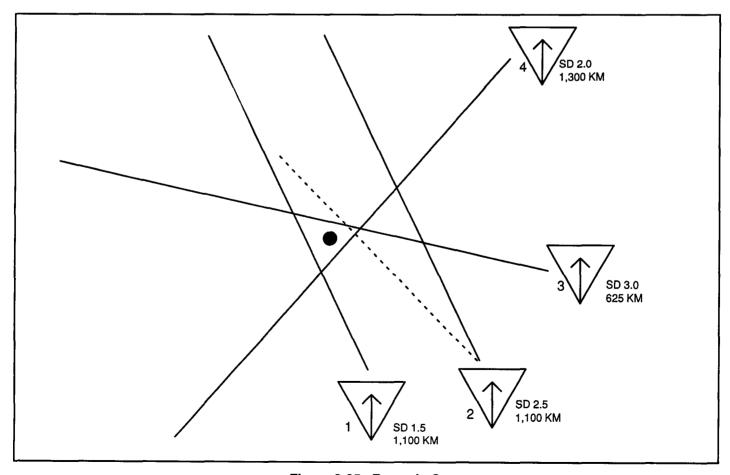


Figure 8-35. Example G.

Single Station Locator Plotting and Analysis

To plot the bearings from the SSL site, ordinary border coordinate or corrected compass rose (CCR) methods can be used (see Chapter 9). To plot the range from the SSL site, a series of semicircular or circular Range patterns can be placed equidistant from the SSL site that equate to various distances from the site (Figure 8-36). The increments of circular Ranges used depends on the operating distance of the particular SSL system.

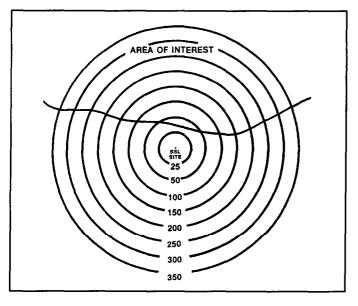


Figure 8-36. Circular Range pattern.

The analytical processing of SSL data is radically different from conventional methods of analysis. The SSL system relies on the propagation of skywaves by the ionosphere. Frequently, this reliance produces *multipath* solutions (Figure 8-37). This means the arriving electromagnetic waves have been propagated at two or more stratums (altitudes) of the ionosphere. The analyst must determine which elevation (or range) is correct. Due to this characteristic of the SSL system, it is important that the DF analyst maintain a close liaison with the traffic analysis (TA) element.

The actual fix point is determined by locating the range along the line of bearing (Figure 8-38). The coordinates are read in the same manner as previously discussed for tactical or strategic analysis.

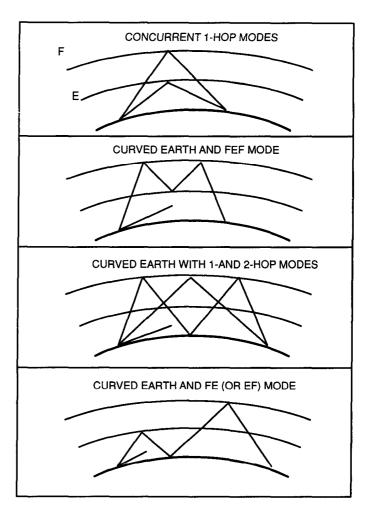


Figure 8-37. Alternative discrete mode propagation paths.

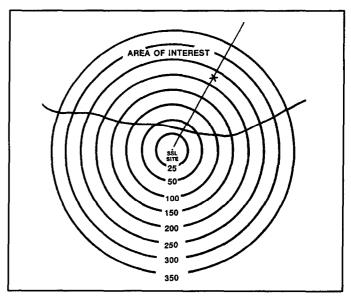


Figure 8-38. Fix point along the line of bearing.

Wild Bearings

In fixes using four or more station's bearings, it may become obvious to the plotter or analyst that a plot contains a *wild* bearing. This is a bearing that shows considerable deviation from the fix created by the other DF stations' bearings. For example, observe the plot illustrated in Figure 8-39. Obviously, site 2 is a wild bearing. In such a situation, the plotter or analyst can disregard the bearing completely when analyzing the fix area.

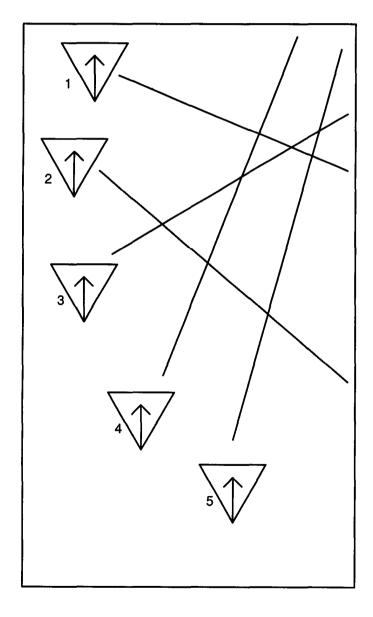


Figure 8-39. Wild bearing.

Radius Determination

A fix radius is a circular area wherein there is a high probability of a target's location. Radius determination can be used with all plotting or analysis methods and techniques with the exception of SSL plotting or analysis. In the past, the radius was determined by measuring from the fix point to the shortest line which joins the angles of intersection. Using this method, there is only a 25 percent probability that the target will be within the radius. Use of the *longest line* will increase the probability factor from 80 to 90 percent. However, such an enlarged radius diminishes the usefulness of the DF information to the consumer. Therefore, the radius shall include a majority but not all of the bearing intersections, thus providing a 45 to 60 percent probability. The procedure for applying a fix radius to your fix point on a tactical map is as follows:

- Place the length of a piece of paper (or measure with a ruler) along the fix point and the second farthest angle of the geometric figure (Figure 8-40, page 8-20).
- Mark on the paper (or measure) the locations of the fix point and the intersection at the second farthest angle (from the fix point).
- Place the paper (or ruler) on the scale at the bottom of the map to get the actual distance.

This distance, in a circular pattern centered at the fix point, is the fix radius or area of probability.

NOTE: The initial placement of the fix point (.) is the approximate center of geometric error area. The fix point is then moved considerably toward the 90 degree angle which is formed by sites 1 and 2. At their respective distances, sites 1 and 2 have the lowest SD of the three participating sites. The radius is computed to intersection B because a radius applied to B will encompass both intersections A and B, constituting a majority (two of three).

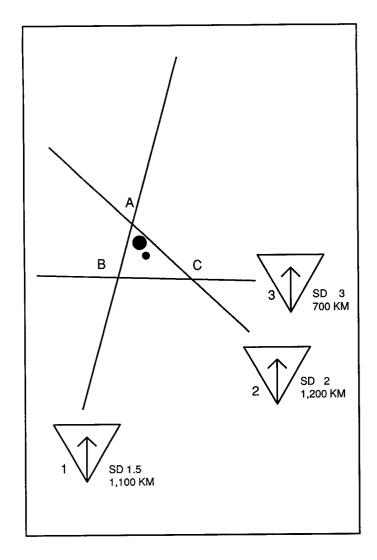


Figure 8-40. Initial placement of a fix.

The procedure for radius determination on gnomonic maps (strategic) is similar to that of UTM maps (tactical). The difference lies in the procedure for measuring the distance of the radius. Instead of equating the length on a tactical map to a given scale, the strategic analyst reads distance directly from the gnomonic map (Figure 8-41). Each square formed from the latitude and longitude lines on the map equates to a distance of 60 Nm. Inside of each square are three rows each of horizontally and vertically oriented dots that are parallel to the latitude and longitude lines. Each dot equates to 15 Nm distance. To determine radius, the length is measured in the same way as on a tactical map. The distance is calculated by placing the paper or ruler in the same area as the fix point, and using the dots inside the

square to estimate distance. The paper should be oriented along lines of longitude or latitude, depending on the alignment of the radius measurement. For example, if the line from the fix point to the angle **of** intersection is oriented along an east-west direction, then the distance measurement will be made using the east-west longitudinal dots. If the analyst wishes to convert the radius to statute miles (Sm), the analyst simply multiplies the determined radius in Nm by 1.15.

Some tactical DF systems have computers which will produce a fix point (in UTM or geographic coordinates) and an elliptical error probability (EEP) or circular error probability (CEP) radius. CEP is a radius that encompasses one-half of the errors in a two-dimensional error distribution system. It does not analyze geometric configurations. EEP determines the length (major axis) and width (minor axis) of the geometric figure, producing an elliptical radius that is based on error calculations similar to those in CEP evaluations.

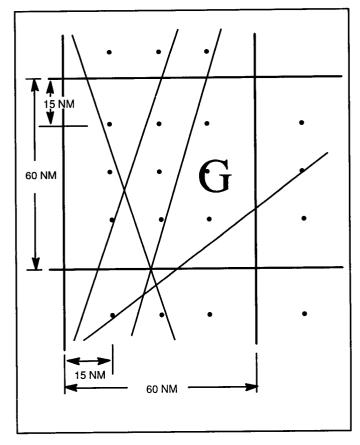


Figure 8-41. Reading distance from the gnomonic map.

Composite Plotting and Analysis

Composite plotting is the process of compiling and averaging bearings obtained over a period of time from a target entity. Composite plotting techniques enable the DF analyst to obtain a more accurate and refined fix area for an emitter under surveillance. The accuracy of the composite plot is also affected by the number of bearings available for averaging. The greater the number of bearings used in the computation, the more accurate the results. The term *composite plotting* is a misnomer. It is used to describe an arithmetic process. After the process is completed, the mean (averaged) bearings are plotted

To make a composite plot, past results are evaluated and a mean bearing is computed for each DF site.

The DF analyst first determines the mean bearing grouping (MBG) of the bearing from each DF site. The MBG is the close numeric grouping of bearings. Bearings are examined to determine if any bearing deviates plus or minus 10 degrees from all other bearings

in the group. Figure 8-42 and 8-43 illustrate this process. In this example, 42 degrees is removed from the calculation because it has a 12 degree deviation from the outermost bearing limit.

| SITE | <u>3</u> |
|------|----------|
| 170 | |
| 170 | |
| 180 | |
| 420 | |
| 170 | |
| 170 | |
| 180 | |
| 190 | |
| 180 | |
| 20° | |
| 180 | |
| 200 | |
| 220 | |
| 270 | |
| 25° | |
| 30° | |
| 28° | |
| 20° | |
| | |
| L | |

Figure 8-42. Compiled list of bearings.

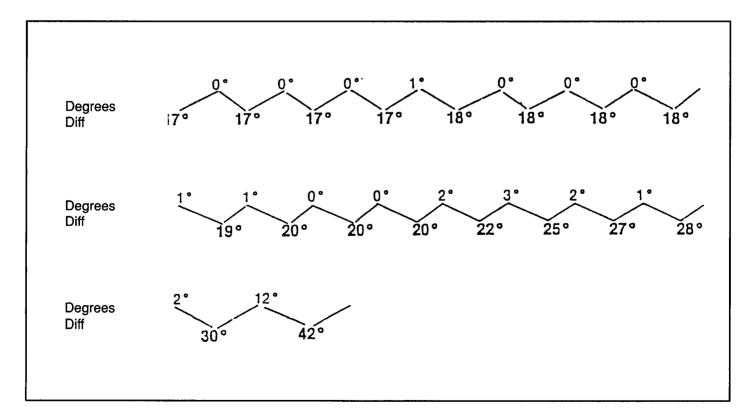


Figure 8-43. MBG determination.

After determining the MBG, the analyst eliminates from the list, any bearings which are more than 10 degrees beyond the upper and lower limits of the MBG. As illustrated in Figure 8-44, the limits of the adjusted MBG are 7 and 40 degrees. Any bearings less than 7 or more than 40 degrees are discarded.

Figure 8-44. Adjusted MBG.

The analyst now computes an initial mean bearing, as illustrated in Figure 8-45 and Figure 8-46. Studying these lists of bearings, the analyst will eliminate any bearings that are plus or minus 8 degrees from the initial mean bearing resulting in an intermediate mean bearing.

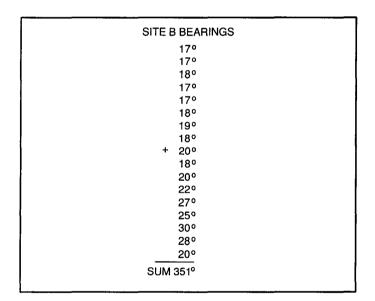


Figure 8-45. Initial mean bearing.

$$351 \text{ (sum of bearings)} \div 17 \text{ (number of bearings)} = ?$$

$$20.6 = 21^{\circ} \text{ (rounded to nearest whole degree)}$$

$$17) 351.0 = 34$$

$$11 = 0$$

$$110 = 102$$

$$8$$

Figure 8-46. Intermediate mean bearing.

The analyst then recomputes a final mean bearing from the remaining bearings. The analyst repeats the process of eliminating any bearings plus or minus 8 degrees from the intermediate mean bearing. A check of the computations in Figure 8-47 and a check of the list of bearings in Figure 8-48 shows that no bearing needs to be eliminated in the example. Therefore, the mean bearing of 20 degrees (Figure 8-49) is plotted as the final mean bearing for the example DF site. This process must be completed for each DF site.

Figure 8-47. Determining bearing limits.

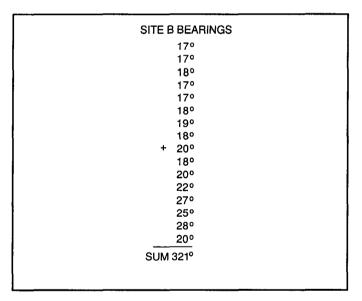


Figure 8-48. Bearing list.

321 (sum of bearings)
$$\div$$
 16 (number of bearings) = ?

$$\begin{array}{r}
20.0 \\
16) \overline{321.0} \\
\underline{32} \\
01 \\
\underline{0} \\
10 \\
\underline{10} \\
10
\end{array}$$

Figure 8-49. Final mean bearing.

Computer Plotting and Analysis

Computerized plotting and analysis of direction finding results is also possible in most strategic DF networks and some tactical systems. The tactical systems with computerized plotting and analysis provide the battalion operations center with near real-time direction finding fix information on targets of interest. In either case, the outstation's bearings are entered into a computer which is programmed to compute the fix location in either geographic or grid coordinates. A fix or no fix of the target transmitter's antenna is quickly determined. The basis for all computer plotting is called the *least square method*.

FFIX is a computer program written in formula translation (FORTRAN) that will compute a fix point and an interval estimate or confidence ellipse when given DF bearings. FFIX is used in all Army strategic DF site computer fix programs. Any other computer programs must be specifically approved by NSA. The input for FFIX consists of the site locations (latitude and longitude) and the SD associated with the respective site. The objective of the algorithm is to identify the largest consistent or cohesive subset of bearings by rejecting wild bearings and then computing the fix point and confidence region for that subset of bearings. (For analytical purposes, the confidence region can be considered the same as a circular radius.) The fix point is computed by the method of maximum likelihood, which is equivalent in this case to the method of least squares.

Currently, the FFIX site look-up table has been programmed for up to 32 or 55 DF sites. The exact number of site inputs depends upon the individual station's requirements. The look-up table stores all pertinent parameters for each site. For the composite fix version, the bearing arrays have been increased to handle 1,000 bearings.

Included in the input data provided to the program are the SD statistics for each site. This SD should represent the SD for targets at a range of 1,000 Nm. This is important because FFIX weighs each site SD as a function of the distance between the site and the fix point. Therefore, if mutually acceptable results are

desired among all users of the algorithm, then all users must use the same SD statistics. (It is the National Security Agency's intention to be in a position to provide the DF sites with the appropriate SD statistics.) If desired, such statistics can be obtained individually by developing site SD/distance curves (see Chapter 9).

Two methods of computer plotting are—

- Exhaustive method.
- Sequential method.

Exhaustive Method

The objective of the algorithm is to identify the largest consistent or cohesive subset of bearings and then compute the fix point and ellipse for that subset of data. In doing so, the program employs two methods for identifying the wild bearings to be rejected. The first approach, known as the *exhaustive* method, is used when 10 or less bearings are submitted. This approach begins by examining the consistency of all the submitted bearings. If all the bearings lack sufficient consistency to qualify as a fix, then the program examines all subsets of bearings until an acceptable fix is identified or until a lower limit on the bearing information is reached. In this approach, all combinations of bearings are exhaustively examined to identify the largest subset of consistent bearing information.

Sequential Method

The second approach, known as the *sequential* method, is used when a bearing set contains more than 10 bearings. It begins by examining the consistency of all the bearings. If all of the bearing responses lack sufficient consistency to qualify as a fix, then the bearing that is more inconsistent with the set of bearings is rejected. The remaining set of bearings is then reexamined in the same way to determine if they are sufficiently cohesive to qualify as a fix. In this manner, the most inconsistent and generally the wildest bearings are rejected sequentially. It is impossible to enter the exhaustive mode of bearing rejection once the program is in the sequential mode.

The same method of determining the confidence region is used in the exhaustive method and the sequential method. The determination of the confidence ellipse (similar to a circular radius) is based on the variance of

the bearings to the fix point. (Bearing errors and target errors are treated as differentials.) Therefore, the computation of the confidence ellipse is independent of the reported bearings. Further information about the FFIX (and the FORTRAN program) may be obtained by writing to:

National Security Agency/Central Security Service (NSACSS) ATTN: P38, DDI RNO Fort George G. Meade, Maryland

ROTATING ROSE PLOTTING

Tactical direction finding equipment will be very mobile in a fluid combat situation. This necessitates an easily adaptable plotting method such as the rotating rose method. The rotating rose method of plotting enables the DF plotter to plot bearings which have been adjusted to true north using a grid map. The intersections of these bearings form a geometric figure on the map where the target emitter's antenna is most probably located. The rotating rose method is used exclusively for tactical plotting on a UTM 1:50,000 map sheet. It is easy to construct and takes a minimum of time and materials. The following materials (Figure 8-50) are needed to construct a rotating rose:

- A 1:50,000 universal transverse mercator map projection.
- Grease pencil.
- Thumbtack.
- Pencil.
- Straightedge.
- Sheet of paper.
- Scotch tape.
- Acetate sheet large enough to cover the map projection.
- True rose (Figure 8-51).

To prepare a UTM 1:50,000 map sheet for rotating rose plotting, first place the map on a smooth, flat surface. Tape it down on all four corners. Ensure the map is stretched as flat as possible, otherwise it could affect the accuracy of the plotting. Once the map is in place, note the latitude-longitude tick marks on each side of the map. They are spaced at 5 degree intervals. There are a total of eight tick marks (Figure 8-52).

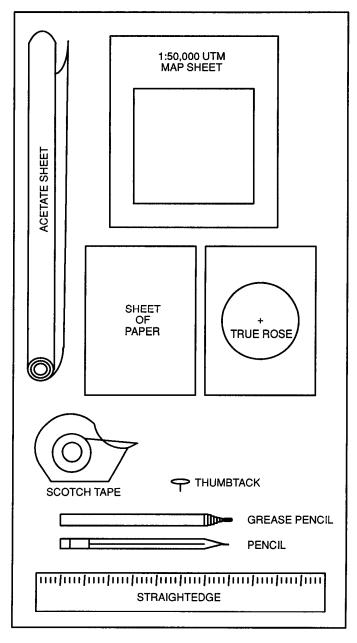


Figure 8-50. Materials needed to construct a rotating rose.

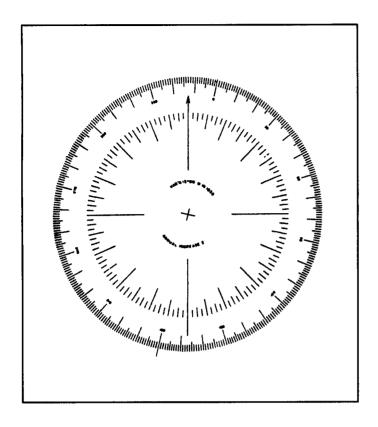


Figure 8-51. True rose.

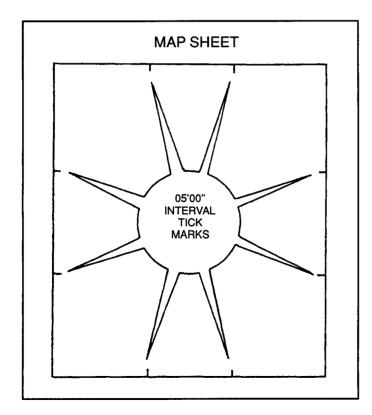


Figure 8-52. Tick marks.

Also note that on a 1:50,000 map sheet there are four cross tick marks-one in each quadrant (Figure 8-53).

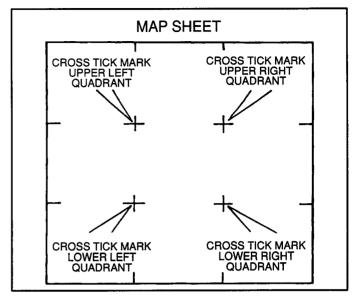


Figure 8-53. Locating the cross tick marks.

These lines indicate where the lines of latitude and longitude cross. Since all lines of longitude are true north-south lines, the latitude-longitude cross tick marks are used to establish a true north-south line on the map. The plotter must construct a true north-south line directly on the map sheet. To do this, use the following steps:

STEP 1. Locate the bottom left-hand tick mark on the map (Figure 8-54).

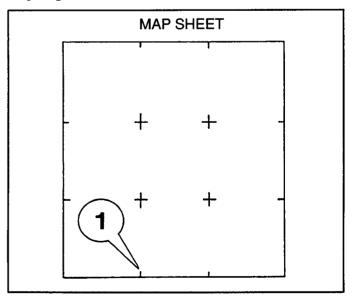


Figure 8-54. Locating tick marks.

STEP 2. Locate the exact center of the cross tick mark in the lower right quadrant of your map. Using a straightedge, draw a connecting diagonal line (Figure 8-55).

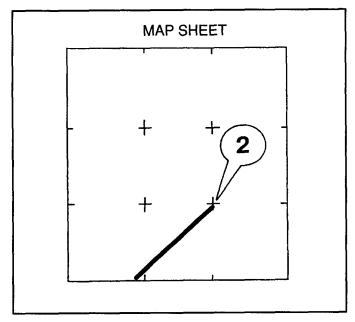


Figure 8-55. Connecting diagonal line.

STEP 3. Locate the exact center of the cross tick mark in the upper left quadrant. Draw a diagonal line connecting it with the center of the cross tick mark in the lower right quadrant (Figure 8-56).

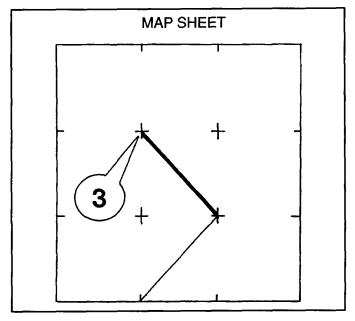


Figure 8-56. Connecting tick marks.

STEP 4. Locate the tick mark in the top right quadrant. Using the straightedge, connect it with the center of the cross tick mark in the upper left quadrant (Figure 8-57). The result is a zigzag pattern which extends the full length of the map.

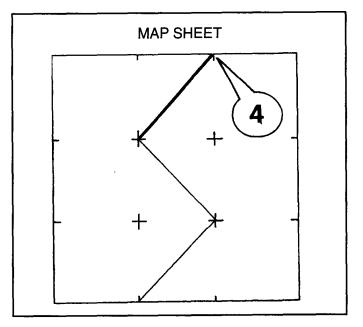


Figure 8-57. Zigzag pattern.

STEP 5. Now repeat the process in reverse. When completed, your map sheet should look the same as Figure 8-58.

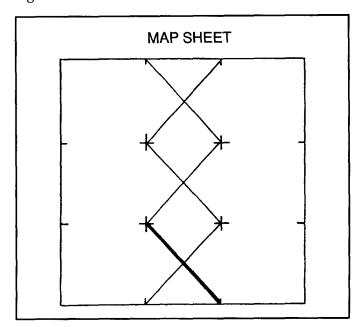


Figure 8-58. Double zigzag pattern.

STEP 6. Align the center points of the Xs with a straightedge and draw a line the complete length of the map (Figure 8-59). This is your true north-south line. Ensure this line is well defined on the map sheet. It will be used for reference when plotting.

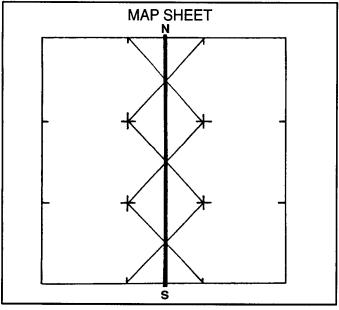


Figure 8-59. True north-south line.

The next step in rotating rose plotting is to locate the DF sites on the map (Figure 8-60). Ensure each site is pinpointed according to it's grid coordinates. Use the following steps:

STEP 1. Identify each site with a letter designation such as site A or site B (Figure 8-60). Use different colored pencils for ease in each site identification.

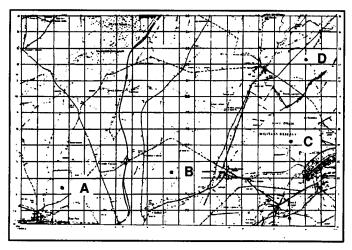


Figure 8-60. Placing DF sites on the map.

STEP 2. Once the sites have been clearly located and marked on your map sheet, lay a piece of acetate over the map (Figure 8-61).

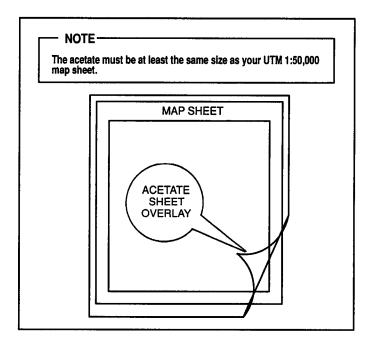


Figure 8-61. Placing acetate over the map.

STEP 3. Place the true rose in the center of your map and tape securely to the acetate (Figure 8-62).

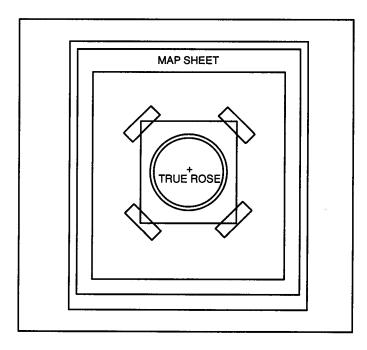


Figure 8-62. Placing the true rose on the map.

STEP 4. Align the 0/360 degree and 180 degree marks of the true rose with the center true north-south line previously drawn on the map (Figure 8-63).

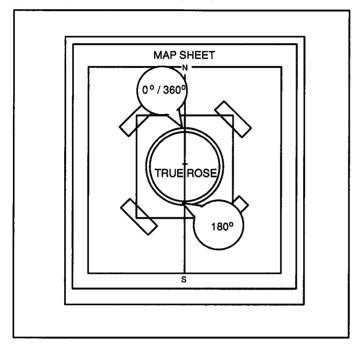


Figure 8-63. Aligning the true rose.

STEP 5. Push a thumbtack through the exact center of the true rose (Figure 8-64). The true rose should now be securely pinned to the map—but free to rotate.

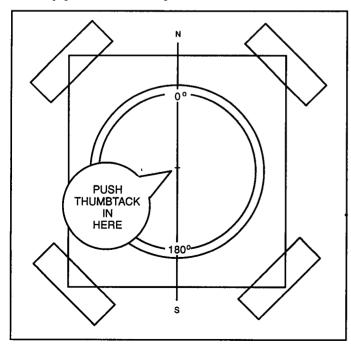


Figure 8-64. Thumbtack placement.

STEP 6. Transfer the locations onto the acetate. However, first ensure the 0/360 degree and 180 degree marks of the true rose are aligned with the true north-south line. Then mark the position of each previously located direction finding site onto the acetate overlay with your grease pencil. To differentiate between the sites marked on your map and those marked on the acetate, circle the letter designations on the acetate (Figure 8-65). The map is now ready to begin plotting.

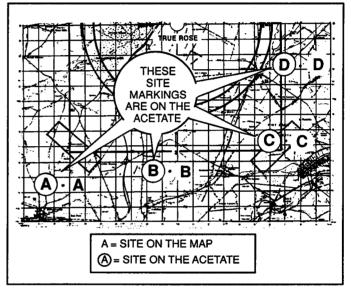


Figure 8-65. Placing DF sites onto the acetate.

To demonstrate how the rotating rose plotting is performed, the following illustrations are provided. Each plotting step is illustrated and is applicable to particular tactical situations. The method remains the same. The difference will be in the—

- Map used.
- Total number of DF sites.
- Site locations.
- Reported bearings.

Assuming that the sites are now clearly marked on the map and acetate as illustrated in Figure 8-65, we will plot the following bearings:

- SITE A 020°.
- SITE B 340°.
- SITE C 290°.
- SITE D 265°.

Initially, we will start with bearing A to illustrate a step-by-step plotting procedure. The reported bearing is 020 degrees. The following steps are used.

STEP 1. Rotate the compass rose until 020 degrees is aligned with the true north-south line on the map (Figure 8-66).

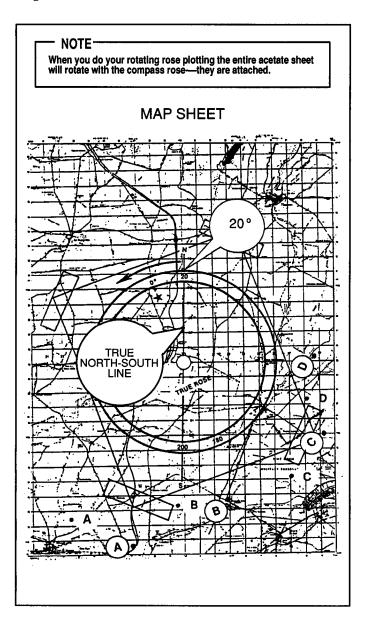


Figure 8-66. Plotting site A's bearing.

STEP 2. Take a sheet of paper and align the long edge with the center true north-south line and the bottom edge with site A on the acetate (Figure 8-67). Make a small tick mark on the bottom edge of the sheet of paper at the point where site A is aligned.

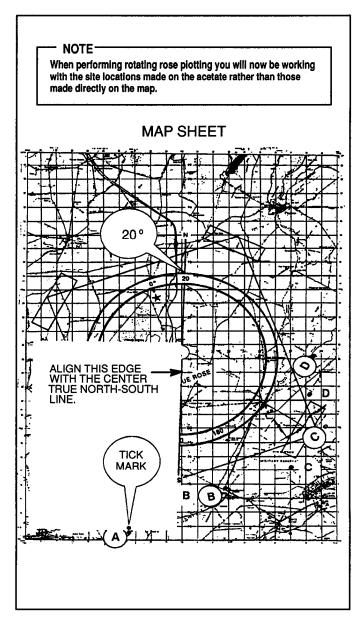


Figure 8-67. Aligning paper with center true north-south line and site A.

STEP 3. Slide the sheet of paper up along the true north-south line until the top edge is aligned with the tip of your map sheet. Ensure the long edge and the center true north-south line are as previously aligned. Place a tick mark on the acetate directly below the tick mark on the bottom edge of the paper (Figure 8-68). This was the tick mark that identified the location of site A.

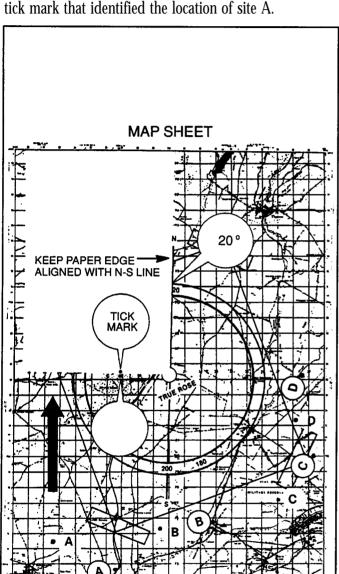


Figure 8-68. Tick mark placement.

STEP 4. Using a straightedge, align the tick mark just made with site A on the acetate. Using a grease pencil, connect these points and extend the line as far as possible (Figure 8-69).

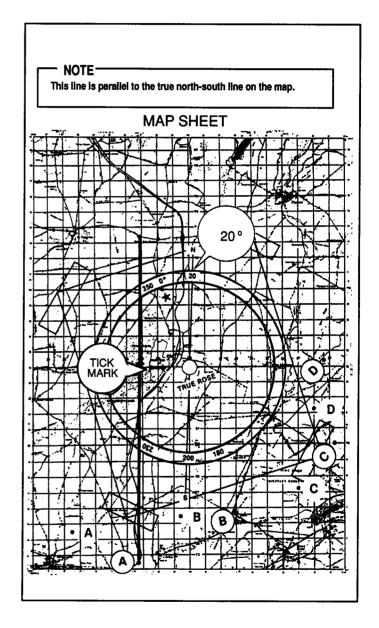


Figure 8-69. Line drawn between site A and tick mark.

STEP 5. Plot the 340 degree bearing for site B. Rotate the true rose to align the 340 degrees with the center true north-south line (Figure 8-70).

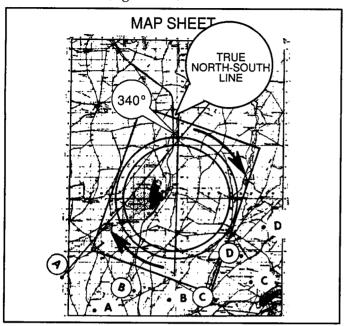


Figure 8-70. Plotting site B's bearing.

STEP 6. Align the long edge of the paper with the true north-south line and the bottom edge of the paper with site B on the acetate. As illustrated in Figure 8-71, make a tick mark on the paper at the point where site B is aligned.

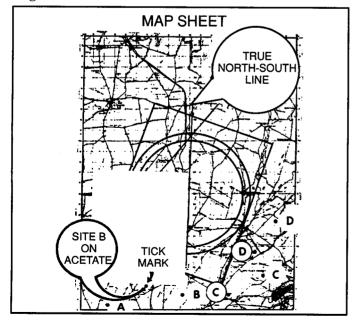


Figure 8-71. Placing tick mark on paper.

STEP 7. Slide the sheet of paper up until the top edge is at the top of the map sheet. Ensure the long edge is aligned with the true north-south line. Place a tick mark precisely below the tick mark on the bottom edge of the paper (Figure 8-72).

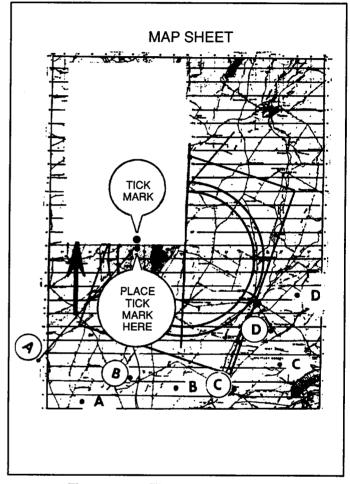


Figure 8-72. Tick mark placement.

STEP 8. Taking a straightedge, align the tick mark just made with site B on the acetate. Draw a line through the two points as far as possible (Figure 8-73).

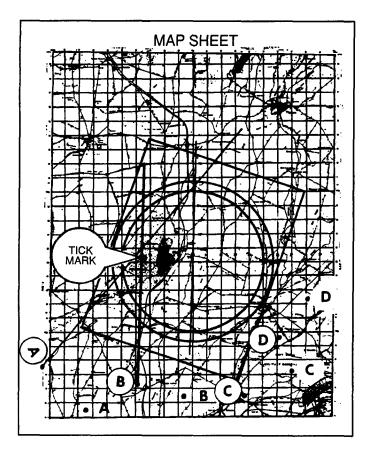


Figure 8-73. Line drawn between site B and tick mark.

Plotting the bearings for sites C and D are completed in exactly the same manner. Once the site C bearing of 290 degrees and site D bearing of 265 degrees are plotted, the acetate will indicate a fix area as illustrated in Figure 8-74. The most probable fix location can then be determined and reported in a 8-digit coordinate. Since the bearings were plotted using a grease pencil, they can now be erased from the acetate and the map is ready to plot the next bearing returns.

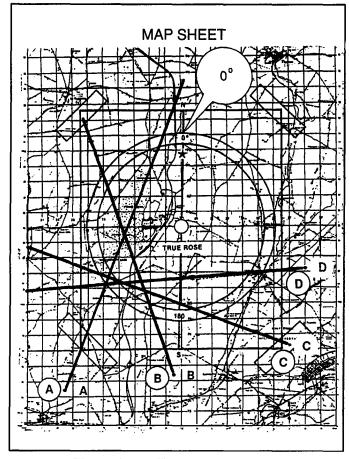


Figure 8-74. The completed plot.

CHAPTER 9

COMPUTATIONS

In Chapter 8, we discussed how maps used in tactical and strategic direction finding operations are developed. Normally, these maps are projected on a plane or a cylinder. Regardless of the projection technique used in developing a map, there will be some distortion. Most strategic DF plotting facilities use mathematical computations to correct this distortion. Tactical plotting operations normally do not compute for map distortion. This is because of the distance from the DF site to the target area (5 to 30 kilometers) and the limited personnel resources and time. It is also not feasible in a tactical environment due to the frequent movement of the DF sites.

We have also discussed how radio waves travel great circle paths. Therefore, using mathematical computations, it is possible to compute the true bearing and distance from a DF site to a known transmitter. These computations are then used to determine the performance of a direction finding site. Normally called statistical analysis, these mathematical computations can reveal DF equipment or operator error. As a management tool, computations can evaluate the DF site as well as the net performance.

MAP DISTORTION CORRECTION TECHNIQUES

The gnomonic projection is the most commonly used map projection for strategic DF plotting (Figure 9-1). It is derived by projecting the surface of the globe, from a center point, upon a planar surface. Its primary

characteristic is that all great circles appear as straight lines. This map is particularly useful when plotting across great expanses of ocean. Distortion on the gnomonic projection is minimal at the point of tangency.

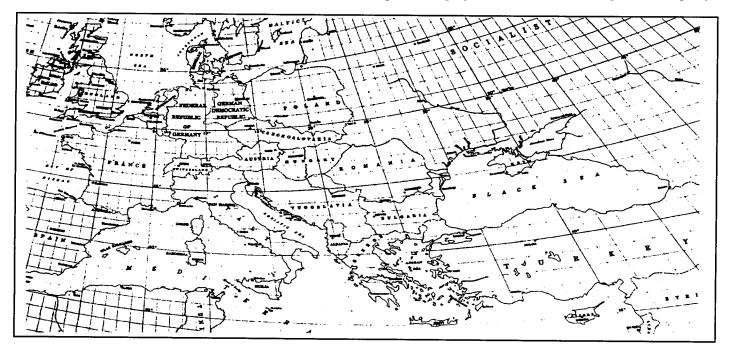


Figure 9-1. Gnomonic projection.

However, distortion increases as the distance from the point of tangency increases. For example, the boundaries near the edge of the map projection are badly distorted and are practically useless for determining true shapes and distances. This distortion does not affect plotting activities if the DF equipment is located within a 4-degree radius from the point of map tangency. Bearings can be plotted to any point on the chart without any appreciable error. However, if the DF station is located outside the 4-degree radius, angular correction must be applied before its bearings can be accurately plotted. The computation methods used to correct this distortion are—

- Border coordinates.
- Corrected compass rose.

Border Coordinates

Border coordinates are used to correct angular distortion on a gnomonic chart. They also provide what is perhaps the most accurate method of manually plotting DF bearings. Border coordinates divide the perimeter of the gnomonic chart into 1,000 equal spaces. The spaces are denoted by tick marks. Every tenth mark is numbered, starting with 00 at the upper left corner and continuing clockwise to 100 (Figure 9-2).

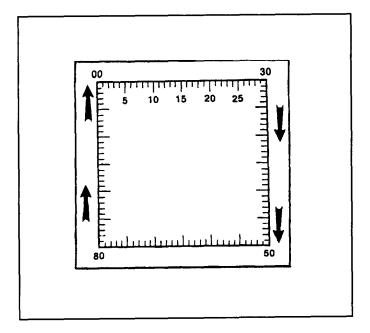


Figure 9-2. Border coordinates.

Border coordinates are constructed on the chart so that 00 through 30 are located on the top border. The numbers 30 through 50 are located on the right border. The bottom border contains 50 through 80. And 80 through 100 are located on the left border. The spaces between the tick marks can be mechanically interpolated into tenths (Figure 9-3).

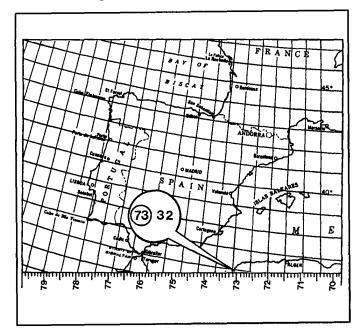


Figure 9-3. Bottom border coordinates.

This provides a total of 10,000 coordinates for plotting purposes (Figure 9-4).

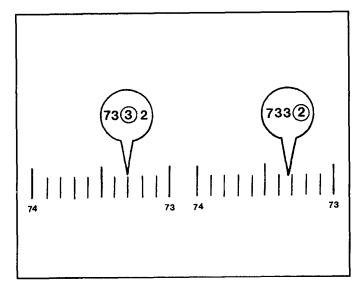


Figure 9-4. Interpolation.

Tables are constructed for each DF site, providing coordinates for all azimuths. When a bearing is reported by a DF site, it is converted to border coordinates. It is then plotted on the gnomonic chart by drawing a line between the coordinate and the DF site. Border coordinates and conversion tables are machine computed. They may be obtained on request from the National Security Agency/Central Security Service. The applicable gnomonic chart number and the exact latitude and longitude of each DF site located must be included in the request.

Corrected Compass Rose

A corrected compass rose is nothing more than a compass rose which has been corrected or expanded to compensate for angular distortion. In other words, the degree marks have been placed close together or moved apart. This is done according to the amount of map distortion present (Figure 9-5).

When situated on the gnomonic plotting chart, the CCR must have its center exactly over the DF site location. Bearings can then be plotted from the CCR. If desired, the rose can be extended to a line around the edge of the map. This is accomplished in the same manner as border coordinates. A corrected compass rose is constructed using the right-triangle method.

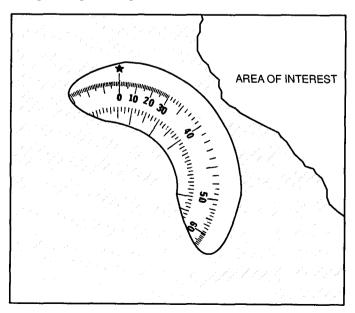


Figure 9-5. Corrected compass rose.

Right-Triangle Method. Constructing a CCR by the right-triangle method entails the computation of mathematical formulas. It is time consuming. However, this is compensated by the high degree of accuracy and reliability it provides. Since radio waves follow great circle paths, the right-triangle method of error correction is concerned with spherical trigonometry. Under theoretical conditions, the equator and the selected meridian would intersect at a right angle (Figure 9-6).

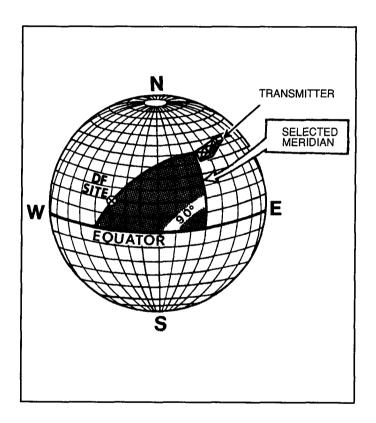


Figure 9-6. Spherical right triangle.

The azimuth from the DF site would intersect both the equator and the selected meridian. This forms a right triangle. A common logarithm of functions of angles in degrees and minutes table (Appendix A) is used to solve the unknown quantities of a spherical right triangle. For additional information on the principles and application of logarithms, refer to TM 11-684. The three known factors of the computation are the—

- Latitude and longitude of the DF site.
- Longitude of the selected meridian.
- Desired azimuth.

Right-Triangulation Computation Work Sheet. The selected meridian used during the computation should be in the approximate center of the area of interest. It also should be noted that one single meridian need not be

used for the computation of the entire CCR. Figure 9-7 illustrates the formula used in the right-triangle method of computation.

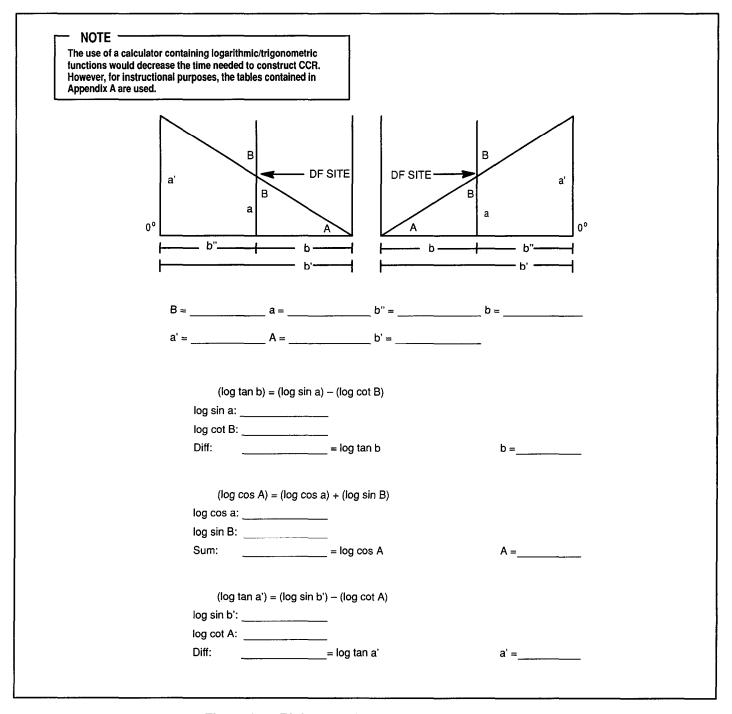


Figure 9-7. Right-triangle computation work sheet.

An explanation of the right-triangle computation work sheet is as follows:

- The bottom line, marked 0 degrees, represents the equator.
- Line a is the distance in degrees and minutes from the equator to the DF site or the latitude of the site.
- Angle B is the desired azimuth which is to be corrected for angular map distortion.
- Angle A is the angle the desired azimuth makes at the equator.

Note: Angles A and B do not total 90 degrees as in a true right triangle. This is because the right-triangle method deals with a right triangle only in theory. The functions are computed by spherical trigonometry.

- Line b is the distance in degrees and minutes of the difference in longitude between the DF site and the intersection of the azimuth with the equator.
- Line b" is the distance in degrees and minutes from the DF site to the selected meridian.
- Line b' is the difference in longitude of the intersection of the azimuth with the equator and the selected meridian. (Line b' is the sum of lines b and b".)

• The value of a' represents the latitude at which the bearing will intersect the selected meridian.

Common Logarithms of Functions of Angles in Degrees and Minutes Table. The table is used in solving the unknown quantities of a spherical right triangle. This information is used to construct a corrected compass rose. The use of common logarithms of functions of angles in degrees and minutes table is as follows:

- Degrees. Each page of the table in Appendix A is computed for eight different angles. Four are indicated in the upper left corner and four in the lower right comer. The fact that one page is sufficient for the functions of eight different angles is a result of the properties of trigonometric functions. For example, the sine of O degrees is numerically equal to the sine of 180 degrees. The cosine of 90 degrees is equal to the cosine of 270 degrees (Figure 9-8).
- Minutes. The minutes for each angle are found in the columns headed by the mathematical sign for minutes (') (Figure 9-9, page 9-6).

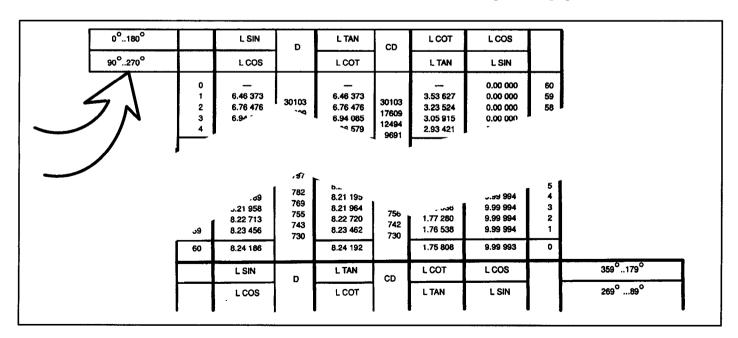


Figure 9-8. Properties of trigonometric functions.

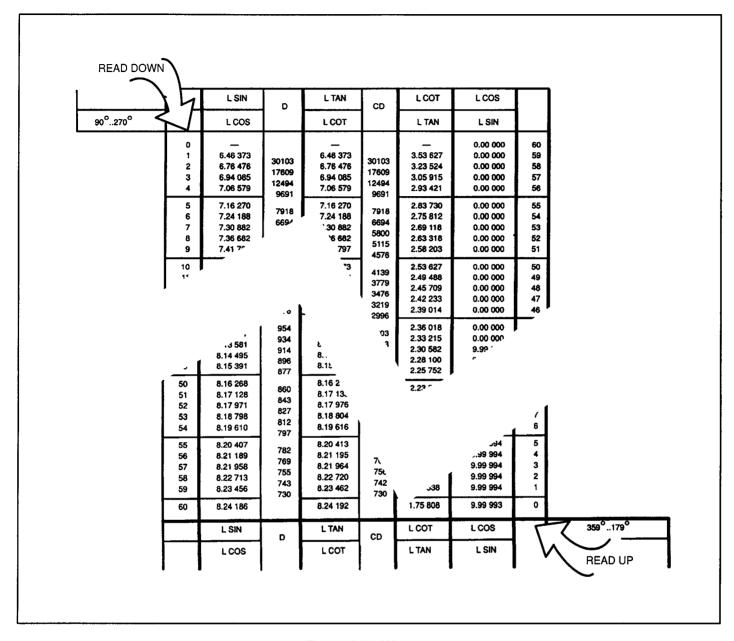


Figure 9-9. Minutes.

The minutes for the angles in the upper left corner are read *down* the left minute column. The minutes for the angles in the lower right corner are read *up* the right

use the following steps (Figure 9-10):

- **STEP 1.** Locate the page containing the angle of the trigonometric function (Figure 9-10(1)).
- STEP 2. Follow the angle's minute column either up or down until the exact minute reading is located (Figure 9-10 (2)).

step 3. Determine which function is appropriate by consulting the legend. Check both the top and the bottom of the table (Figure 9-10 3). Angle functions are *opposite* each angle or degree reading. The number found at the intersection of the function column and the logarithm row opposite the minute column is the logarithm of that angle.

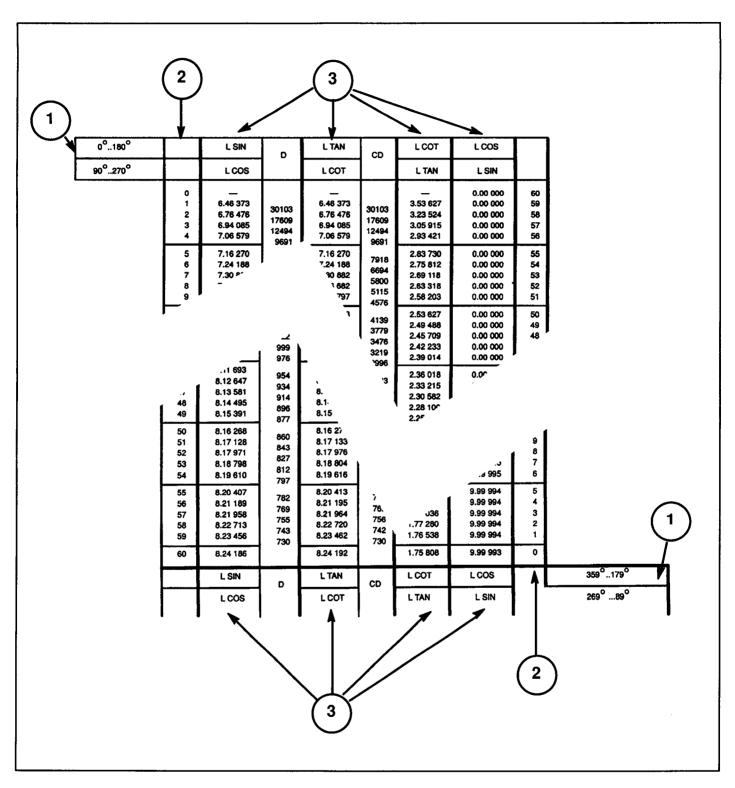


Figure 9-10. Use of the tables.

To determine the angle of a logarithm, use the following steps (Figure 9-11):

- **STEP 1.** Locate the logarithm which is *nearest* the given logarithm in the appropriate function column (Figure 9-11 (1)).
- **STEP 2.** The minute value will be selected from either the corresponding number in the left minute column or the right minute column (Figure 9-11 (2)).
- STEP 3. Note the corresponding angles of the function column, top left comer and bottom right comer. Select the *lowest* of the four angles (Figure 9-113). If the selected angle is at the top of the page, read the minute value from the left minute column. However, if the selected angle is taken from the bottom of the page, read the minute value from the right minute column.

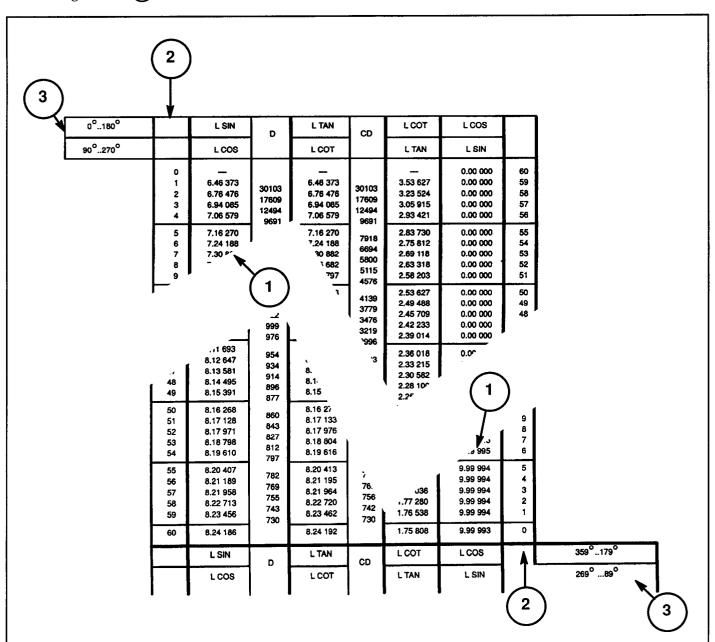


Figure 9-11. Determining the angle of a logarithm.

Right-Triangle Method Example. The desired azimuth (or angle B) which is to be corrected for angular distortion is 10 degrees. The latitude of the DF site (or line a) is 36 degrees. The difference in longitude between the DF site and selected meridian (or b") is 5 degrees. (Refer to Appendix A for logarithm table.)

STEP 1. Find b:

(log sin a) - (log cot B) = (log tan b) Log sin 36 degrees = 9.76922-10 (Figure 9-12) Log cot 10 degrees = 0.75368 (Figure 9-13)

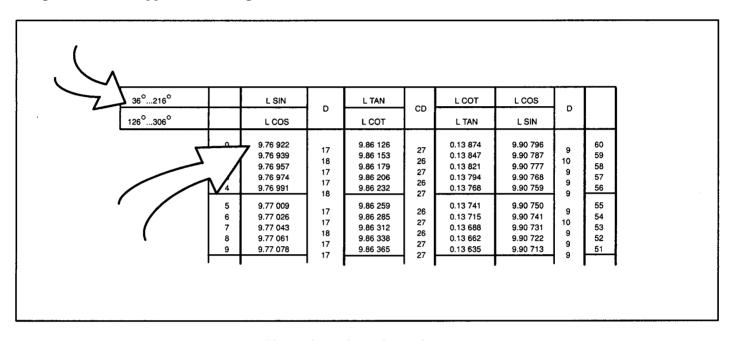


Figure 9-12. Log sin 36 degrees.

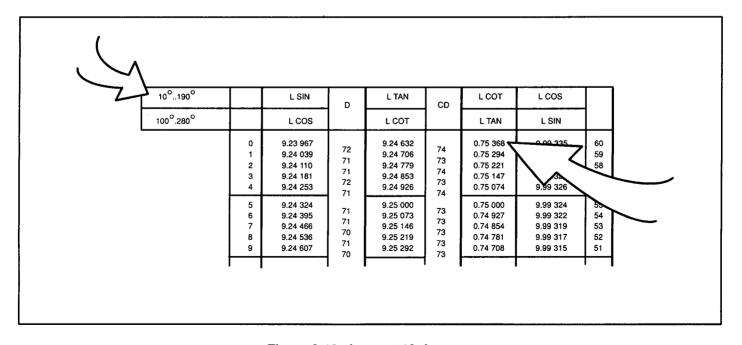


Figure 9-13. Log cot 10 degrees.

Log diff = 9.01554-10Log tan b = 9.01554-10

b = 5 degrees 55 minutes (Figure 9- 14)

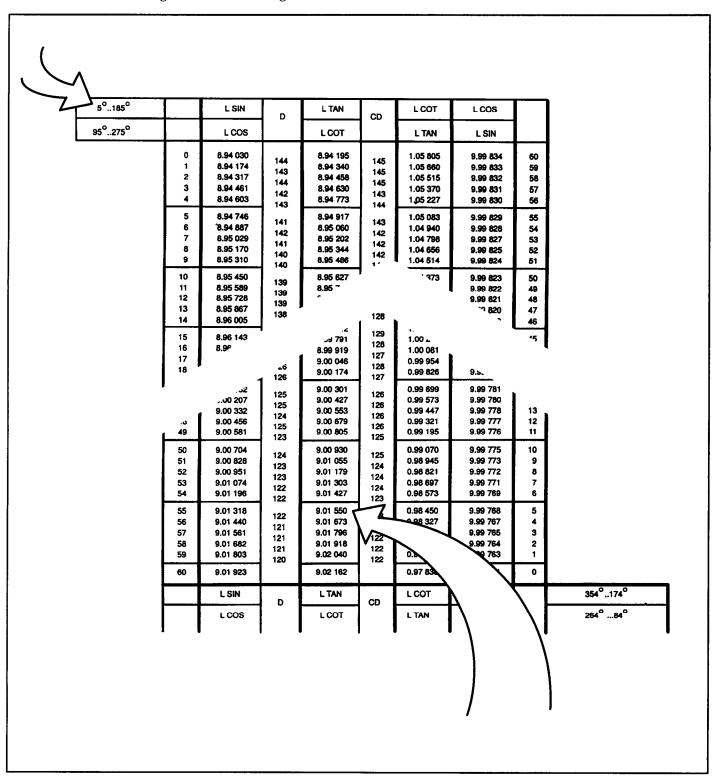


Figure 9-14. Determining the angle of log tan b (9.01554-10).

STEP 2. Find b':

(b'') + (b) = (b')

b" = 5 degrees

b = 5 degrees 55 minutes

b' = 10 degrees 55 minutes

STEP 3. Find A:

 $(\log \cos a) + (\log \sin B) = (\log \cos A)$

Log cos 36 degrees = 9.90796-10 (Figure 9-15)

Log sin 10 degrees = 9.23967-10 (Figure 9-16)

NOTE: Always select the lowest degree and minute reading.

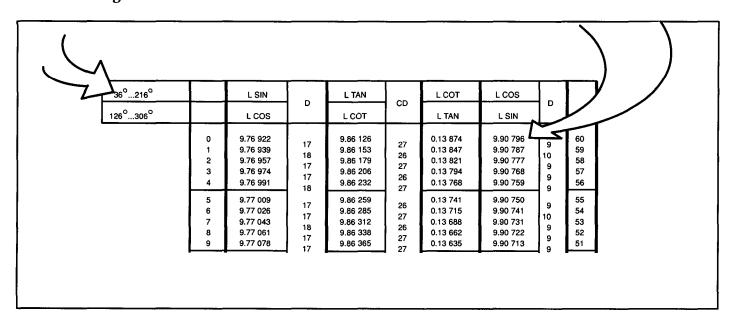


Figure 9-15. Log cos 36 degrees.

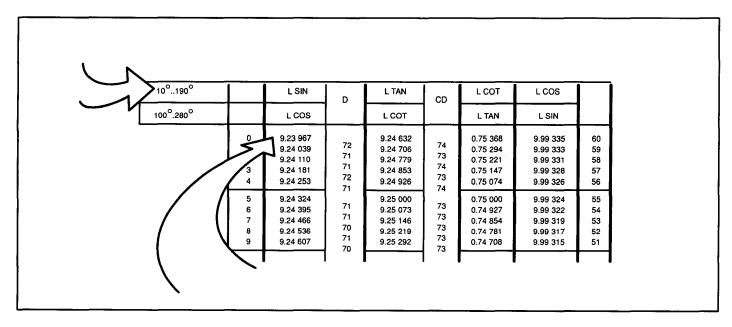


Figure 9-16. Log sin 10 degrees.

Log sum = 19.14763-20

Log cos A = 9.14763-10 (Figure 9-17)

A = 81 degrees 55 minutes

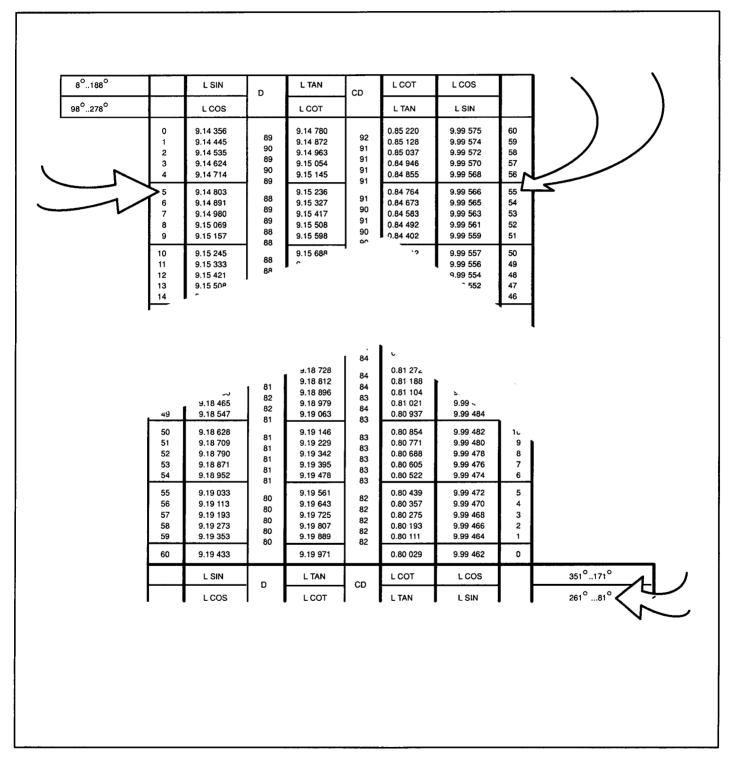


Figure 9-17. Determining the angle of log cos 9.14763-10.

STEP 4. Find a':

(log sin b') - (log cot A)= (log tan a') Log sin 10 degrees 55 minutes = 9.27734-10 (Figure 9-18) Log cot 81 degrees 55 minutes =9.15236-10 (Figure 9-19)

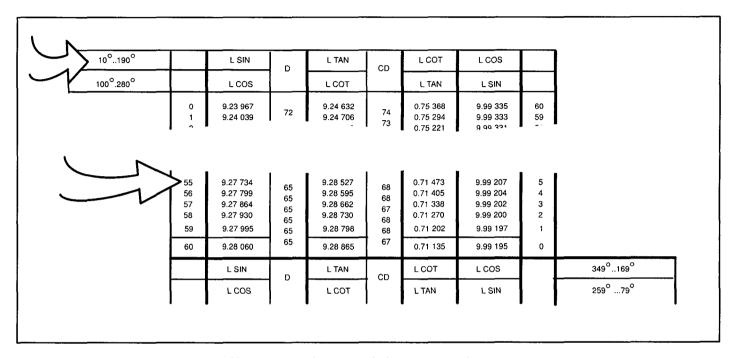


Figure 9-18. Log sin 10 degrees 55 minutes.

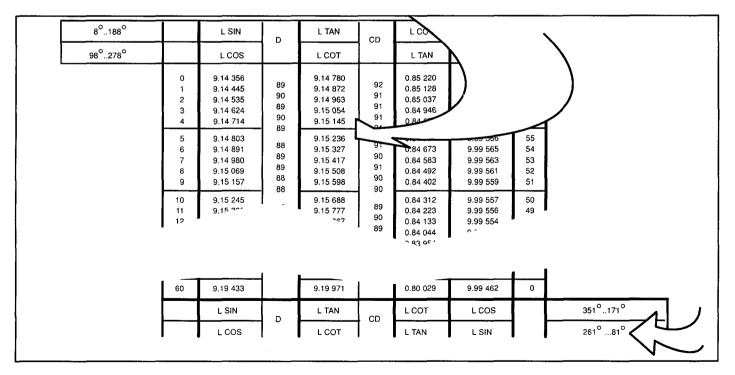


Figure 9-19. Log cot 81 degrees 55 minutes.

Log diff = 0.12498Log tan a' = 0.12498

> a' = 53 degrees 08 minutes (Figure 9-20)

STEP 5. A straightedge aligned with 53 degrees and 8 minutes latitude on the selected meridian indicates the corrected azimuth for 10 degrees. When constructing a corrected compass rose, a tick mark should be placed on the compass rose and numbered 10 degrees. Or a tick mark should be placed on the edge of the plotting chart and numbered 10 degrees.

A problem area may arise when computing desired azimuths around 90 or 270 degrees. To eliminate confusion, subtract the value of b from

90 degrees and complete the computations. This procedure should also be used approximately 5 degrees on either side of the 90 or 270 degree azimuth. This ensures standard accuracy.

NOTE: It is apparent that logarithm tables are constructed in such a manner so the area from 0 to 90 degrees represents the entire 360 degrees. Any computation using X degrees east as the selected meridian will also be correct for X degrees west and both reciprocals. Therefore, any single computation will yield four azimuths. Ninety computations are required to complete the entire compass rose.

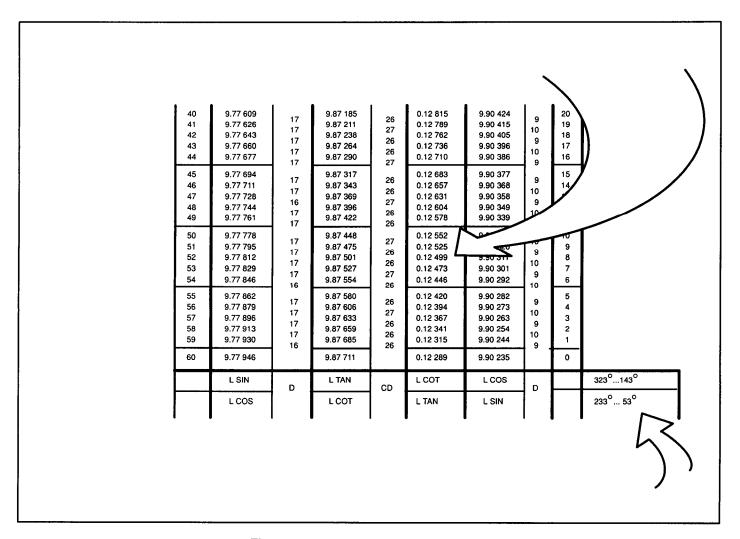


Figure 9-20. Log tan a' 0.12498 angle.

GREAT CIRCLE AZIMUTH AND DISTANCE

Radio waves follow great circle paths between the transmitting and receiving antennas. When the exact location of the signal source is known, it is possible to compute the true or great circle azimuth and distance (GCAD). This can be computed from the point of signal origin to any other point receiving the signal on the surface of the earth. The computations of great circle

azimuths are based on spherical trigonometry (Figure 9-21). They may be computed using the dead-reckoning altitude and azimuth table in Appendix B. This method is simpler and much faster than using other logarithmic methods. It is accurate to within one half a minute. Greater accuracy is possible by interpolating between table functions.

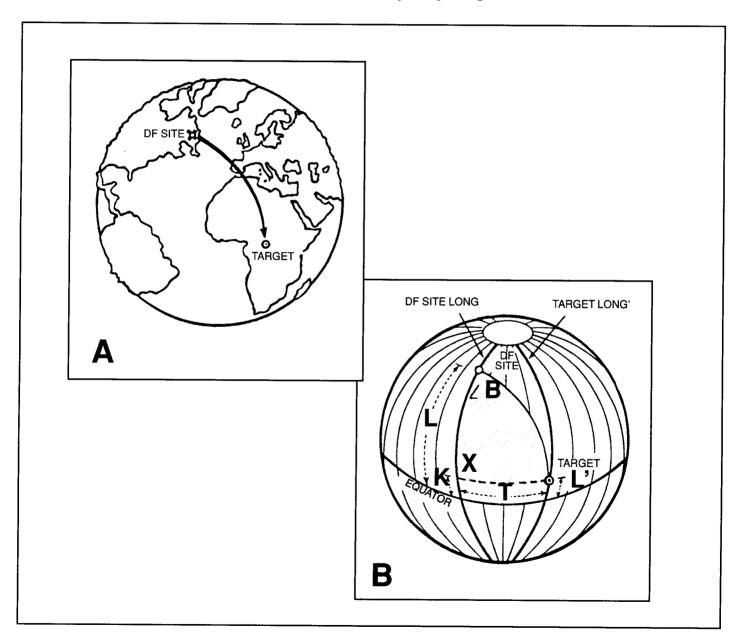


Figure 9-21. Spherical trigonometry.

Dead-Reckoning Altitude and Azimuth Table

The dead-reckoning altitude and azimuth table (Figure 9-22) is arranged in parallel *A* and *B* columns. The *A* columns contain log cosecants multiplied by 100,000. The *B* columns contain log secants also multiplied by 100,000. The *A* columns decrease in value from the front of the table toward the rear. The *B*

columns increase in value from the front of the table to the rear.

When determining degrees and minutes from the top of the table, read the minutes from the *left* column (Figure 9-22 1). However, when reading the degrees and minutes from the bottom of the table, read the minutes from the *right* column (Figure 9-222). If the desired degrees and minutes exceed 180 degrees, subtract 180 degrees before entering the table.

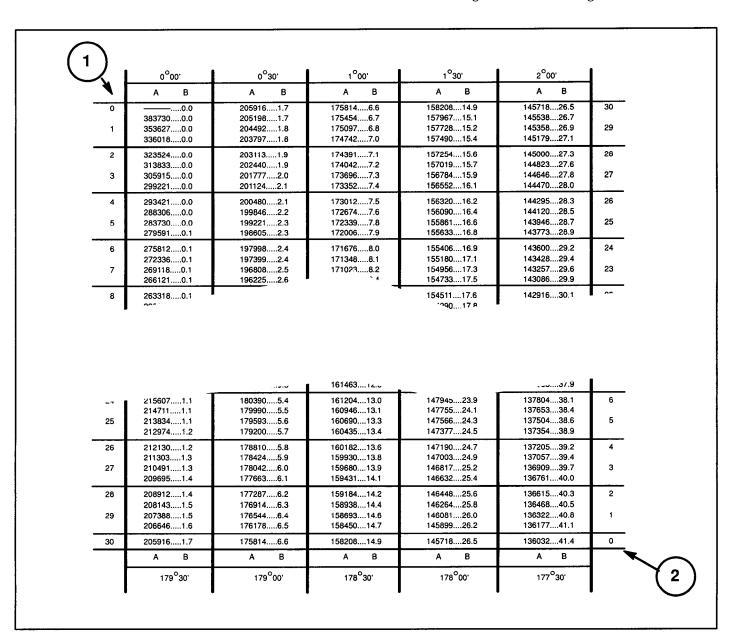


Figure 9-22. Dead-reckoning altitude and azimuth table.

Great Circle Azimuth and Distance Computation

Great circle azimuth and distance computations are based on spherical trigonometry. A terrestrial triangle has curved sides and is commonly referred to as a spherical triangle. Refer to Figure 9-21 B, page 9-15. The shaded portion of the illustration is a spherical triangle. The determination of the true azimuth and distance is reduced to simply completing the work sheet (Figure 9-23) using the dead-reckoning altitude and azimuth table.

| FROM:TO: | | T is determined by the following conditions: If long and lor are the same name SUBTRACT. If long and long' are differenames ADD. | | | |
|---------------------------------------|---------------------------|--|-------------------------|--|--|
| | | LONG': | | T | |
| LONG: ——— | CONG := | | | | |
| DEGREES/MINUTES | COL-1 (ADD) | COL -2 (SUBTRACT) | COL-3 (ADD) | CQL-4 (SUBTRACT) | |
| T: | _ A: | - | | | |
| L': | - B: | _ A: | | | |
| | A: | _ B: | B: | A: | |
| K: | - | A: | • | | |
| L: | = | | | | |
| | | | | | |
| KL: | | | B: | | |
| DARC: | | | | A: | |
| D ANG. (| | | | | |
| 80 x DEGREES | | | | A: | |
| +MINUTES | | | | <8 | |
| TOTAL | | | | | |
| TRUE AZIMUTH | | | | | |
| | | | | | |
| | | | | | |
| If other logarithm tables log secant. | are used instead of dead- | reckoning altitude and azimi | ıth tables, column A eq | uates to log cosecant, and column B equates to | |

Figure 9-23. GCAD computation work sheet.

Specific formula symbols used in the GCAD formula (Figure 9-24) are as follows:

- L or lat is the latitude of the initial position or the DF site.
- L' or lat' is the latitude of the final position or the check station.
- ∠ B is the great circle azimuth from the check station to the DF site.
- D arc is the great circle distance, in minutes of arc, between the target and the DF site. (One minute of arc equals one nautical mile.)
- X is the factor introduced to simplify the computation. It represents that point at which a great circle constructed perpendicular to the target's meridian crosses the meridian of the DF site.
- K is the latitude of point X or the arc from X to the equator (assumes the name of the latitude of the final position).
- KL is the difference between K and L.
- Long is the longitude of the DF site.
- Long' is the longitude of the check station.
- T is the distance from the target longitude to the line of longitude of the DF site.

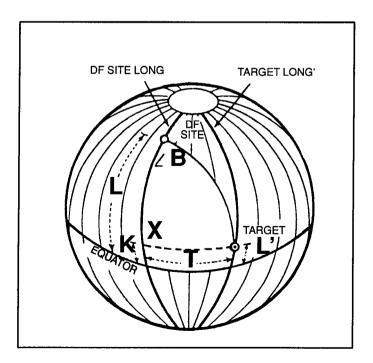


Figure 8-24. Spherical triangle symbols.

Special Rules. The fact that D arc maybe greater than 90 degrees has necessitated the following rules:

Rule 1. When L and L' are the same name (north or south), the following procedures are applicable:

- a. When T is *greater* than 90 degrees, select the K value from the bottom of the dead-reckoning altitude and azimuth table. When T is *less* than 90 degrees, select the K value from the top of the table.
- b. Record ∠ B from the top of the table when K is greater than L. When K is less than L select ∠ B from the bottom of the table.
- D arc is recorded from the top of the table except when T and KL are both greater than 90 degrees.

Rule 2. When L and L' are different names, the following procedures are applicable:

- a. When T is greater than 90 degrees, select the K value from the bottom of the table. When T is less than 90 degrees, select the K value from the top of the table.
- B from the bottom of the table except when KL is greater than 180 degrees.
- c. D arc is recorded from the bottom of the table *except* when T and KL are both *less* than 90 degrees.
- d. When KL exceeds 180 degrees, subtract 180 degrees before making a table computation.

Rule 3. Computation of \angle B. –

- a. When the initial position is in the Northern Hemisphere and is west of the final position, ∠ B is the true bearing.
 If the initial position is east of the final position, ∠ B is subtracted from 360 degrees to obtain the true bearing.
- b. When the initial position is in the Southern Hemisphere and is west of the final position, subtract ∠ B from 180 degrees. If the initial position is east of the final position, add 180 degrees to ∠ B to obtain the true bearing.

Great Circle Azimuth and Distance Work Sheet

To facilitate the computation process, a GCAD work sheet is illustrated in Figure 9-25. It is divided into a heading and the step-by-step procedure for determining true azimuth and distance. An explanation of the work sheet and the GCAD formula follows.

The heading contains the latitude and longitude of the direction finding site and the selected check station, containing abbreviations—

FROM: The name of the DF site.
LAT or L: The latitude of the DF site.
LONG: The longitude of the DF site.
TO: The name of the target station.

- LAT' or L': The latitude of the target station.
- LONG': The longitude of the target station.
- T: To determine T, one of the following two rules is applicable and must be followed.
 - Rule 1. If LONG and LONG' are in the same hemisphere (same names), *subtract* to determine the T value.
 - Rule 2. If LONG and LONG' are in different hemispheres (different names), add to determine the T value.

| LAT: DF Site La | atitude LAT: | nome of Target Statio Target Station Latiti Target Station Longi | de name | e same name SUBTRACT. II long and long' are different s ADD. |
|-----------------|--------------|--|-------------|---|
| DEGREES/MINUTES | COL-1 (ADD) | COL -2 (SUBTRACT) | COL-3 (ADD) | COL-4 (SUBTRACT) |
| T: | A: | _ | | |
| t': | B: | = ^: | • | |
| | A: | e: | _ B: | A: |
| K: | _ | A: | - | |
| L: | | | | |
| | | | | |
| KL: | | | B: | |
| D ARC: | | | D: | A: |
| | | | | |
| 60 X DEGREES | | | | A: |
| | | | | <b< td=""></b<> |
| | | | | |
| TRUE AZIMUTH | | | | |
| | | | | |

Figure 9-25. GCAD work sheet explanation.

The remainder of the work sheet is divided into the degrees/minutes column and column-1 through column-4. The mathematical function is indicated at the top of each column. Logarithms are entered at the spaces *A* and *B* beginning with column-1 and the appropriate function performed. If other logarithm tables are used instead of the dead-reckoning altitude and azimuth table, column A will equate to the log cosecant. Column B will equate to the log secant. Prior to beginning the computation, enter the T value in the appropriate space under the degrees/minutes column. Complete the work sheet as follows:

COL-1

- Locate the T value in the dead-reckoning altitude and azimuth table (Appendix B). Enter the figure found under the corresponding A column in the appropriate space under COL-1.
- Enter L' in the appropriate space under the DEGREES/MINUTES column.
- Locate the L' value in the table. Enter the corresponding B column number in the appropriate space under COL-1.
- Add the COL-1 A and B values. Enter the results under the final A space in COL-1.

COL-2.

- Locate the L' value in the table. Enter the corresponding A column figure in the appropriate space under COL-2.
- Locate the COL-1 final A value in the table. Enter the corresponding B figure in the appropriate space under COL-2.
- Subtract the COL-2 B value from the COL-2 value. The result is entered as the final COL-2 A value.
- Locate the final COL-2 A value in the table. The corresponding degrees and minutes will be entered as the K value under the DEGREES/ MINUTES column.

NOTE:

Before the K value is determined, refer to special rules 1 or 2. Determine which rule is applicable to the GCAD computation.

COL-3.

- The first COL-3 B value is a repeat of the COL-2 B value.
- Enter the L or LAT in the appropriate space under the DEGREES/MINUTES column.
- Determine the KL value under the DEGREES/ MINUTES column. *Subtract* the L or LAT value from the K value if they are the same name. If they are different names, *add K and L*
- Locate the KL value in the table. Enter the corresponding B column value in the appropriate COL-3 space.

NOTE:

If rule 2 is applicable to the computation, and the KL value exceeds 180 degrees, subtract 180 degrees before entering the table.

- •Add the COL-3 values. Enter the result as the final COL-3 B value.
- Locate the final COL-3 B value in the table. Enter the corresponding degrees and minutes as the D arc value under the DEGREES/MINUTES column.

NOTE:

Refer to applicable rule to determine if the D arc value is taken from the top or the bottom of the table.

COL-4.

- The first COL-4 A value is a repeat of the final COL-1 A value.
- Locate the final COL-3 B value in the table. Enter the corresponding A value in the appropriate COL-4 A space.
- Subtract the COL-4 A values and enter the difference in the space provided.
- Locate the final COL-4 A value in the table. Enter the corresponding degrees and minutes as the COL-4 ∠ B value.

NOTE:

Again refer to the applicable rule. Determine if \angle B is taken from the top or the bottom of the table. Determine if that value is the true azimuth.

Distance. To compute the great circle azimuth distance—

- Multiply the number of D arc degrees by 60.
- Add the D arc minutes to the result. The sum indicates the distance in nautical miles. To obtain statute miles, multiply the nautical miles by 1.15.

Great Circle Azimuth and Distance Example.

Determine the great circle azimuth and distance from Needham's Villa, USA, to London, England. The necessary coordinates are in Figure 9-26. Before beginning the computation, determine which rule is applicable. Since LONG and LONG' are the same name—west—rule 1 applies.

STEP 1. Determine the T value. Since LONG and LONG' are the same name—west—subtract to find the difference.

Needham's Villa LONG: 71° 36' London, England LONG': 00° 05' T 71° 31'

STEP 2. Locate the T value, 71 degrees 31 minutes, in the dead-reckoning altitude and azimuth table. The corresponding COL-1 A value from the table is 2300 (Figure 9-27).

FROM. Needham's Villa TO: London, England are the same name SUBTRACT. If long and long' are different names ADD.

LAT: 71° 36' West LONG: 00° 05' West TO: LONG:

Figure 9-26. Entering initial information on work sheet.

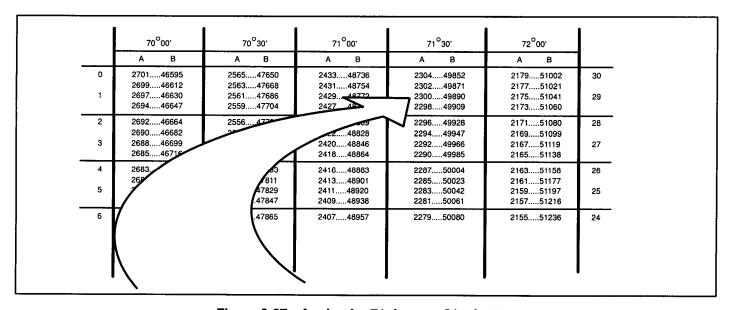


Figure 9-27. A value for 71 degrees 31 minutes.

STEP 3. Locate the L' value, 51 degrees 32 minutes, in the table. The corresponding COL-1 B value is 20617 (Figure 9-28).

STEP 4. Add COL-1 A and B values (Figure 9-29).

The result or 22917 is the final COL-1 A value.

A: 2300 B: + 20617

22917

50°00' 50°30' 51⁰30' 51 00° 11575....19193 11259....19649 10950....20113 10646 20585 10347 11569....19201 11254....19657 10945....20121 10640....20593 10342. 11564....19208 11249....19664 10939....20128 10635....20601 1033 11559....19216 11244....19672 10934....20136 10630....20609 2 11553....19223 11239....19680 10929....20144 10625....20617 10327....21098 11548....19231 11233....19687 10924....20152 10620....20625 10322....21106 11543....10238 11228....19695 10919....20160 10615....20633 10317....21114 27 11537....19246 11223....19703 10914....20167 10610....20641 10312....21122 4 11532....19253 11218....19710 10909....20175 10605....20649 10307....21131 26 11527....19261 11213....19718 10904....20183 10600....20657 10302....21139 5 11522....19269 11207....19726 10899....20191 10595....20665 10298....21147 25 11516....19276 11202.. .19733 10894....20199 10590... .20672 10293....21155 6 11511....19284 11197....19741 10888....20207 10585....20680 10288....21163 11506....19291 11192....19749 10883...20214 10580....20688 10283....21171 11501....19299 11187....19756 10878....20222 10575....20696 10278....21179 23 11495....19306 11181....19764 10873....20230 10570....20704 10273....21187 8 11490....19314 11176....19772 10868....20238 10565....20712 10268....21195 11485....19321 11171....19779 10863....20246 10560....20720 10263....21204 11479....19329 11166...19787 10858....20254 10555....20728 10258....21212 21 11474....19337 11161....19795 10853....20261 10550....20736 10253....21220 10 11469....19344 11156....19803 10848....20269 10545...20744 10248....21228 20 11464....19352 11150....19810 10843....20277 10540....20752 10243....21236

Figure 9-28. B value for 51 degrees 32 minutes.

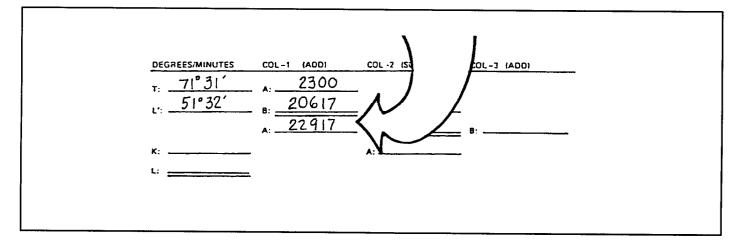


Figure 9-29. Final COL-1 A value.

STEP 5. Locate the L' value, 51 degrees 32 minutes, in the table (Figure 9-30). The corresponding COL-2 A value is 10625.

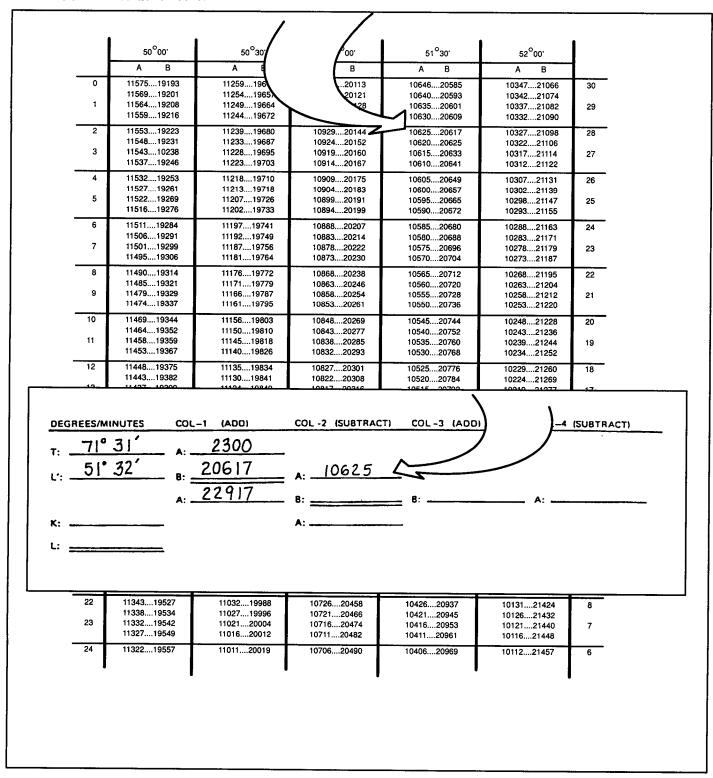


Figure 9-30. A value for 51 degrees 32 minutes.

STEP 6. Locate the COL-1 final A value, 22917, in the table (Figure 9-3 1). The corresponding COL-2 B value is 9292.

-92921333

10625

A:

B:

STEP 7. Subtract the COL-2 B value, 9292, from the COL-2 A value—10625. The remainder is 1333 and the final COL-2 A value (Figure 9-32).

23934.....8766

23925.....8770

23916.....8775

233

12

36⁰00' 36⁰30' 37°00' 35°30' Α 0 24141.....8663 23605.....8931 23078.....9204 22561....9482 22054....9765 30 24132.....8668 23596.....8936 23069.....9209 22553....9487 22045....9770 1 24123.....8672 23587.....8940 23061.....9213 22544....9492 22037....9775 29 24114.....8677 23578.....8945 23052.....9218 22536....9496 22029....9779 24105.....8681 2 23569 8949 23043 9223 22527 9501 22020 9784 28 23560 8954 23035...9227 24096.....8686 22519....9505 22012....9789 3 24087 8690 23551 8958 23026 9232 25510 9510 22003 9794 27 21995....9798 24078.....8694 23543.....8963 23017.....9236 22501....9515 4 24069.....8699 23534.....8967 23009.....9241 22493....9520 21987....9803 26 24060....8703 23525.....8972 23000.....9246 22484....9524 21978....9808 5 24051.....8708 23516.....8976 22991.....9250 22476....9529 21970....9813 25 24042....8712 23507.....8981 22983.....9255 22467....9534 21962....9818 24033....8717 23498.....8986 22974....9259 22459....9538 21953....9822 24 6 24024.....8721 23490.....8990 22965....9264 22450....9543 21945....9827 7 24015.....8726 29957.....9269 21937....9832 23 23481.....8995 22442....9548 24006.....8730 23472.....8999 22948.....9273 22433....9552 21928....9837 8 23997.....8734 23463. ..9004 22939.....9278 22425....9557 21920....9841 22 23988....8739 23454 ..9008 22931.....9282 22416....9562 21912....9846 9 23979.....8743 23446. ..9013 22922....9287 22408....9566 21903....9851 21 23970....8748 23437 22913.....9292 22399....9571 21895....9856 10 23961....8752 234 22905.....9296 22391....9576 21887....9861 20 21878....9865 23952....8757 22896.....9301 22382....9581 11 23943 8761 22887 9305 22374 9585 21870 9870 19

Figure 9-31. A value of 22917.

22879.....9310

22870.....9315

22862.....9319

22366....9590

22357....9595

22349....9599

21862....9875

21853....9880

21845....9885

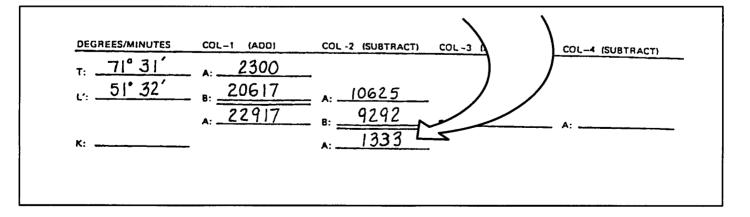


Figure 9-32. Final COL-2 A value.

STEP 8. Locate the final COL-2 A value, 1333, in the table. The corresponding degrees and minutes, 75 degrees 52 minutes 30 seconds, represents the K value (Figure 9-33).

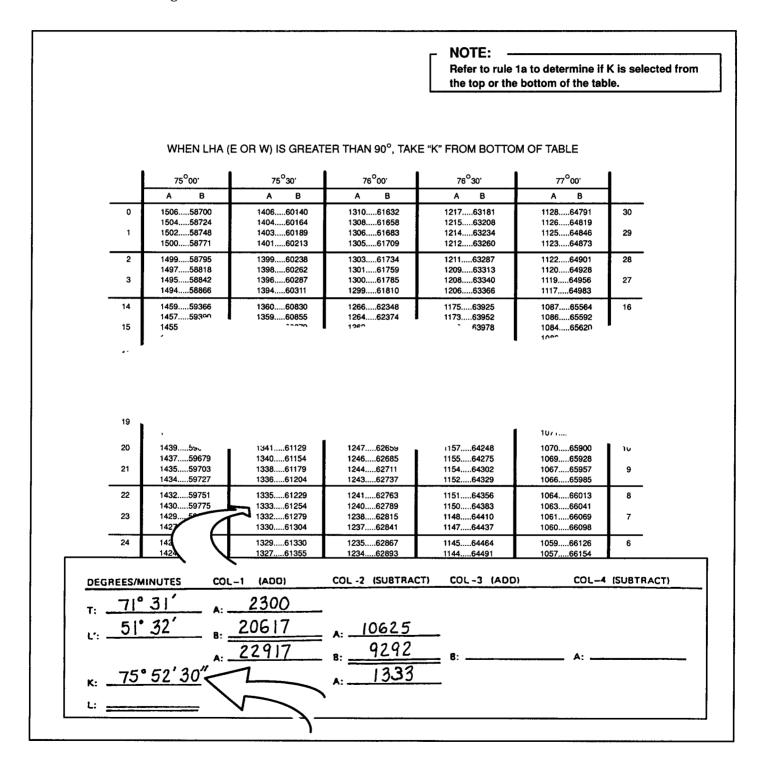


Figure 9-33. Determining K value.

- STEP 9. Record the first COL-3 B value as 9292 (Figure 9-34 1). It is a repeat of the COL-2 B value.
- STEP 10. Enter the value for LAT, or 42 degrees 33 minutes, under the DEGREES/MINUTES column in the appropriate space (Figure 9-34 2).
- STEP 11. Determine the value for KL by subtracting LAT, 42 degrees 33 minutes, from the K value of 75 degrees 52 minutes 30 seconds. The remainder is 33 degrees 19 minutes 30 seconds (Figure 9-34(3)).

K: 75 degrees 52 minutes 30 seconds

L: <u>- 42 degrees 33 minutes</u>

KL = 33 degrees 19 minutes 30 seconds

| DEGREES/MINUTES COL-1 (ADD) | COL -2 (SUBTRACT) | COL-3 (ADD) | COL-4 (SUBTRACT) |
|--|--------------------------------|---------------|------------------|
| T: 71° 31′ A: 2300 L': 51° 32′ B: 20617 A: 22917 K: 75° 52′ 30″ L: 42° 33′ (2) | A: 10625 B: 9292 A: 1333 | 9292 (|) A: |
| KL: 33° 19'30"(3) | | B: | A: |
| 60 × DEGREES | | | A: |
| TOTAL | | | |
| TRUE AZIMUTH | | | |

Figure 9-34. Work sheet entries.

STEP 12. Locate the KL value, 33 degrees 19 minutes 30 seconds, in the table. The corresponding B value is 7802 (Figure 9-35).

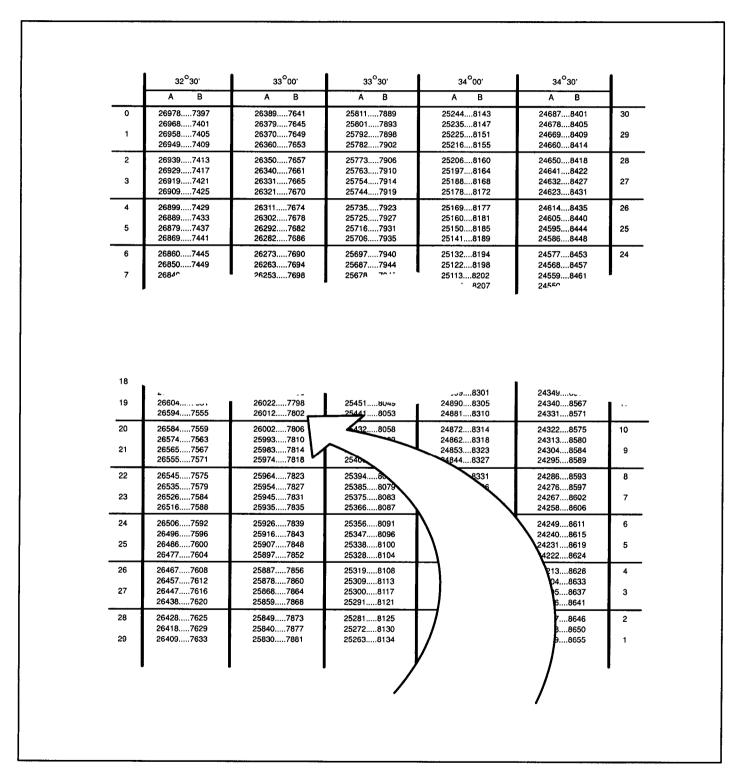


Figure 9-35. B value for 33 degrees 19 minutes 30 seconds.

D.

STEP 13. Add the COL-3 B values. The sum and final B value is 17094 (Figure 9-36 (1)). 9292

| I | =17094 |
|---------|--|
| FROM. N | eedham's Villa To: London, England 42° 33' North LAT': 51° 32' North 71° 36' West LONG: 00° 05' West T is determined by the following conditions; if long and long' are different names ADD. 71° 31' |
| | DEGREES/MINUTES COL-1 (ADD) COL-2 (SUBTRACT) COL-3 (ADD) COL-4 (SUBTRACT) |
| | T: $\frac{71^{\circ} 31'}{51^{\circ} 32'}$ A: $\frac{2300}{20617}$ A: $\frac{10625}{9292}$ B: $\frac{9292}{42^{\circ} 33'}$ A: $\frac{1333}{1333}$ B: $\frac{9292}{42^{\circ} 33'}$ A: $\frac{1333}{1333}$ |
| | KL: 33° 19'30" B: 7802 B: 17094 A: |
| | 60 × DEGREES |
| | + MINUTES <b< td=""></b<> |
| | TRUE AZIMUTH |

STEP 14. Record the first COL-4 A value as 22917 (Figure 9-36 2). It is a repeat of the final COL-1 A value.

Figure 9-36. GCAD work sheet entries.

STEP 15. Locate the COL-3 final B value, 17094, in the table (Figure 9-37(1)). The corresponding COL-4 A value is 13185.

A: <u>– 13185</u>

A:

22917

= 9732

STEP 16. Subtract the COL-4 A value, 13185 (Figure 9-37 (2)), from the 22917. The final COL-4 value is 9732 (Figure 9-37 (3)).

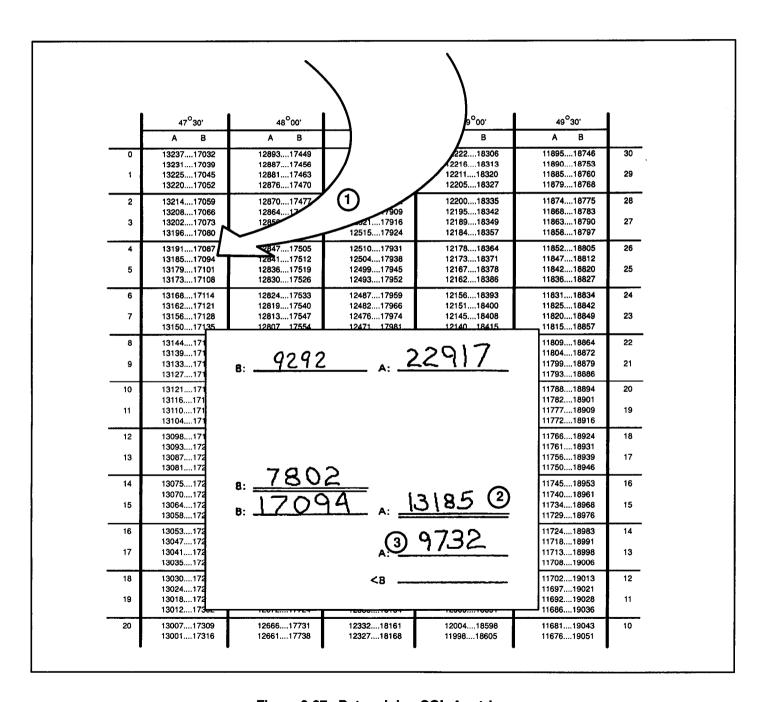


Figure 9-37. Determining COL-4 entries.

STEP 17. Locate the COL-4 final A value, 9732, in the table (Figure 9-38). Again refer to rule 1 and determine if ∠ B is taken from the top or the bottom of the table. Since K is greater than L, ∠ B is selected from the top of the table. Therefore, ∠B or the true azimuth from

Needham's Villa to London, England, is 53 degrees 03 minutes 30 seconds. Refer to rule 3 and determine if∠ B is the true bearing. The initial position is west of the final position. Therefore, 53 degrees 03 minutes 30 seconds is the true azimuth.

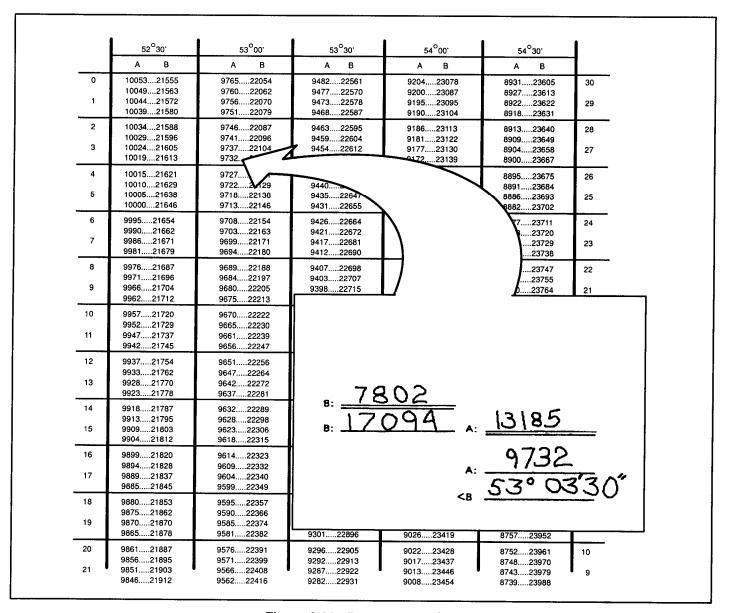


Figure 9-38. Determining \angle B.

STEP 18. To determine D arc, locate the final COL-3 B value, 17094, in the table (Figure 9-39 1). Refer to rule 1 to determine if D arc is taken from the top or the bottom of the table. Since T and KL are both less than 90 degrees, D arc is taken from the top of the table. It is 47 degrees 34 minutes 30 seconds (Figure 9-39 2).

STEP 19. To compute the distance from the initial to the final position in nautical miles, multiply D arc by 60. To obtain statute miles, multiply the total nautical miles by 1.15.

D arc = 47 degrees 34 minutes 30 seconds $47 \times 60 = 2820$ (Figure 9-39 3) + 34.5 (Figure 9-39 4)

Total nautical miles = 2854.5 (Figure 9-39 5) $\times 1.15$ 142725 28545

Total statute miles = 3282.675

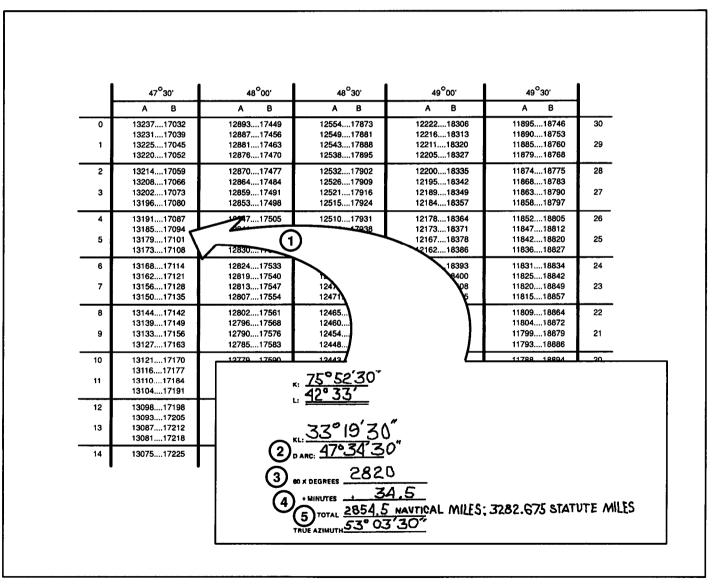


Figure 9-39. Determining D arc and total distance.

STATISTICAL FACTORS

Statistical analysis is an invaluable management tool for measuring direction finding performance. An estimate of the amount of error found in individual bearings is provided through the proper application of statistics. The probable amount of error of the DF site or even the complete DF net can also be determined. Normally, plotting and evaluation centers are responsible for performing accuracy studies. However, direction finding supervisors and analysts must be knowledgeable of statistical analysis procedures. They must be able to compute the analytical computations outlined in this section.

Systematic Error

Systematic error represents the difference between the true bearing and the mean bearing of a transmitter. The true bearing is determined by computing a great circle azimuth from the DF site to the selected target station. The average bearing is determined by taking a large number of bearings on the selected transmitter-a minimum of 200-and computing the average or mean bearing of the sample.

The following criteria is considered when selecting a check station:

- The frequency should be compatible with operational targets.
- The location should be within the area of interest or within a very close proximity.
- The distance should not be significantly different from that of operational targets.

The following definitions are used:

- Bearing mean (BM) is the mean bearing between the DF site and the selected check station.
- Bearing true (BT) is the true bearing between the DF site and the selected check station.

NOTE: Systematic error is computed using the formula:

SE= BM minus BT

The following steps outline the procedure for computing the systematic error:

- **STEP 1.** Visually inspect the reported bearings. Eliminate the wild bearings. (A wild bearing is considered plus or minus 8 degrees from the *true* bearing.)
- **STEP 2.** Mathematically compute the mean bearing from the remaining bearings.
- **STEP 3.** Determine the difference between the mean and true bearings. The difference is the systematic error.

NOTE: Systematic error must always be expressed as a negative or positive error. If the mean bearing is smaller than the true bearing, the error is negative. However if the mean bearing is larger than the true bearing, the error is positive.

The following example illustrates the computation of systematic error using the formula SE = BM - BT. The true azimuth of the check station is 029 degrees. The following bearings were observed on the selected check station: 028, 034, 013, 023, 029, 036, 058, 029, 032, 035, 033, 038, 021, 028, 031, 027, and 031 degrees.

NOTE: In practical applications, at least 200 bearings must be obtained on the selected check station.

- STEP 1. Inspect all reported bearings to ensure there are no wild bearings. In this example, 013, 038, and 058 degrees are wild; they are removed from our computation.
- **STEP 2.** Compute the mean bearing.

```
028° 033°
034° 0210
023° 028°
029° 031°
036° 027°
029° <u>031°</u>
032° 417° divided by 14 = 29.7857 degrees
035°
```

STEP 3. Determine the difference between the mean and true bearings. The difference is the systematic error.

SE = BM-BT

SE = 029.79 - 029.0 degrees

SE = +0.79 degrees

Variance

Variance is used as a reliability factor and indicates the quality of bearings used in the computation of the mean bearing. Variance provides the measure of spread or the dispersion of bearings around the mean bearing. The analysis of either site or individual operator variance on selected check stations provides the supervisor with an additional management tool for evaluating efficiency. The formula for computing variance is:

- σ^2 is the symbol for variance.
- **≤** jindicates the algebraic sum.
- (BM BO)² is the bearing observed (BO) subtracted from the mean bearing. The difference or remainder is then squared.
- N is the total number of bearings within plus or minus 8 degrees of the mean bearing.

The following steps outline the procedure for computing variance:

- **STEP 1.** Visually inspect all reported bearings and eliminate the obvious wild bearings.
- **STEP 2.** Mathematically compute the mean bearing from the remaining bearings.
- **STEP 3.** Eliminate any of the remaining bearings which deviate more than plus or minus 8 degrees from the computed mean bearing.

- **STEP 4.** Recompute the mean bearing, if necessary.
- **STEP 5.** Determine the deviation of each observed bearing from the mean bearing. Square each deviation.
- **STEP 6.** Add the squared deviations. Divide the sum by the total number of bearings used. The result is the variance.

NOTE: Due to the squaring process in step 5, the negative sign no longer applies.

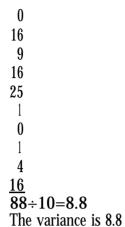
For example, the following bearings were observed on a selected check station: 330, 326, 333, 334, 325, 331, 330,329,328, and 334 degrees.

NOTE: In practical applications, at least 200 bearings must be obtained on the selected check station.

- **STEP 1.** A visual inspection proves there are no obvious wild bearings.
- **STEP 2.** Compute the mean bearing.
- STEPS 3 and 4. Since there are no bearings which deviate over plus or minus 8 degrees from the computed mean, proceed to step 5.
- **STEP 5.** Determine the deviation of each observed bearing from the mean bearing. Square each deviation.

| BM | BO | Remair | nder | Squared |
|---------------|--------|--------------|------|---------|
| 330° | - 330° | 0° | = | 0 |
| 330° | – 326° | 4° | = | 16 |
| 330° | – 333° | -3° | = | 9 |
| 330° | – 334° | -4° | = | 16 |
| 330° | – 325° | -5° | = | 25 |
| 330° | - 3310 | -1° | = | 1 |
| 330° | – 330° | 0° | = | 0 |
| 330° | – 329° | 1° | = | 1 |
| 330° | – 328° | 20 | = | 4 |
| 330° | – 334° | -4° | = | 16 |

STEP 6. Add the squared deviations and divide by the number of bearings used. The result is the variance.



Square Root

Although standard deviation is another direction finding statistical factor, before it can be addressed, it is necessary to be able to manually compute square root. Pocket calculators and other machine aids can perform this function much faster. However, the need for manual computation of square root may arise. The following steps outline the procedure for obtaining the square root of the number 3.4:

STEP 1. Starting at the decimal point, mark off the digits in pairs in both directions. Add zeros, as necessary.

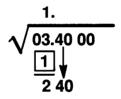
$$\sqrt{03.4000}$$

STEP 2. Place the decimal point for the answer directly above the decimal point that appears under the radical sign.

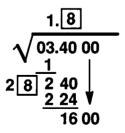
STEP 3. Determine by inspection the largest number that can be squared without exceeding the first pair of digits-03. The answer is 1. This is because the square of any number larger than 1 will be greater than 03, Place the 1 above the first pair of digits.

$$\sqrt{\frac{1.}{03.40\ 00}}$$

STEP 4. Multiply 1 by itself. This equals 1. Place the 1 under the 03. Subtract 1 from 03. This equals 2. Then bring down the next pair of digits.



STEP 5. Double the answer or quotient of 1 (1 doubled equals 2). Place the 2 to the immediate left of 240. Determine the number that can be multiplied by 2 and that same number, but do not exceed 240. The answer is 8 since $28 \times 8 = 224$. (The number 9 would prove to be too large since $29 \times 9 = 261$.) Place the number 8 to the right of the decimal in the quotient. Subtract the 224 from 240 and bring down the next pair of numbers-00.



STEP 6. Disregarding the decimal point, double the quotient 18, obtaining 36. Place the 36 to the left of the 1600. Determine the number that can be multiplied by 36 and that same number, but do not exceed 1600. The answer is 4 as $364 \times 4 = 1456$. (The number 5 would be too large since $365 \times 5 = 1825$.) Place the 4 above the second pair of digits.

$$\begin{array}{r}
1.84 \\
\sqrt{03.4000} \\
28240 \\
224 \\
364 \\
1600 \\
1456 \\
144
\end{array}$$

Depending on the degree of accuracy desired, you can continue the process indefinitely by adding zeros. For direction finding purposes, two places to the right of the decimal are sufficient. The square root of 3.40 is 1.84 or $1.84^2 = 3.3856$.

Standard Deviation

Standard deviation is perhaps the best statistical method of evaluating direction finding site performance. Systematic error is indicative of average error. Standard deviation is a representative of site reliability. Standard deviation is a probability figure which indicates the spread of bearings on one or more targets. In this respect, the smaller the number or SD, the greater the reliability that is attributed to the direction finding site. Standard deviation is computed using the formula:

- BT is the true bearing between the DF site and the selected check station.
- BO is the observed bearing of the selected check station,
- N is the total number of bearings, within plus or minus 8 degrees of the mean bearing, used in the computation.
- (SE)² is the systematic error squared.

The following steps outline the procedure for computing the standard deviation:

- **STEP 1.** Compute the SE of a selected check station using a minimum of 200 bearings.
- STEP 2. For each observed bearing, determine the deviation in degrees from the true bearings. (If the true bearing on the selected check station is not known, a great circle azimuth must be computed.)
- STEP 3. Square each deviation.
- STEP 4. Add the squared deviations. Divide the sum by the total number of bearings used in the computation, within plus or minus 8 degrees of the mean bearing. This step satisfies the (BT-BO)² portion of the formula.

STEP 5. Square the SE obtained in step 1. Subtract the (SE)² from the number obtained in step 4.

STEP 6. Compute the square root of the number obtained in step 5. The square root represents the standard deviation of the direction finding site.

The following example illustrates the computation of standard deviation. To prevent a lengthy illustration, only 10 bearings are used. The following information is provided:

SE = -001 degree BT = 031 degrees The following bearings were observed on the selected check station: 029, 025, 032, 029, 034, 032, 030, 028, 034, and 027 degrees.

STEP 1. An SE of -001 degree is provided.

STEP 2. Subtract the BO from the BT.

| BT | ВО | R | emaind | ler |
|---------------|-----------------|---|--------------|-----|
| 0310 | - 029° | = | 2° | |
| 0310 | $-~025^{\circ}$ | = | 6° | |
| 031° | -032° | = | -1° | |
| 031° | $-~029^{\circ}$ | = | 2° | |
| 0310 | -034° | = | -3° | |
| 031° | -032° | = | -10 | |
| 0310 | -030° | = | 1° | |
| 031° | – 028° | = | 3° | |
| 031° | -034° | = | -3° | |
| 031° | - 027° | = | 4° | |

STEP 3. Square the remainder obtained in step 2.

| Remainder | Squared |
|-------------|---------|
| 2° | 4 |
| 6° | 36 |
| -10 | 1 |
| 2° | 4 |
| -3° | 9 |
| -10 | 1 |
| 1° | 1 |
| 3° | 9 |
| -3° | 9 |
| 4° | 16 |

STEP 4. Add the squared deviations and divide by the total number of bearings used in the computation.

This step satisfies $(BT-BO)^2$ portion of the formula.

STEP 5. Square the SE and subtract the result from the number obtained in step 4.

$$\sqrt{\frac{9-(SE)^2}{\sqrt{9-(-001)^2}}}$$
 $\sqrt{\frac{9-1}{8}}$

STEP 6. Compute the square root.

The standard deviation is 2.82

Standard Deviation/Distance Curve

It is difficult to visualize the effect that distance has on bearings without periodically computing a SD/distance curve for each DF site within the net (Figure 9-40). The SD/distance curve for the SSL varies from those of conventional DF systems because the SSL has a better ability to discriminate against the effects of multipath propagation (Figure 9-4 1). Therefore, at distances beyond 1,000 km (below 10 MHz) and 100 Nm (above 10 MHz), the curve for the SSL continues in a straight line and has no further deviation. The primary reason for the SD/distance curve is to show accurate SD information at the various ranges from each DF site.

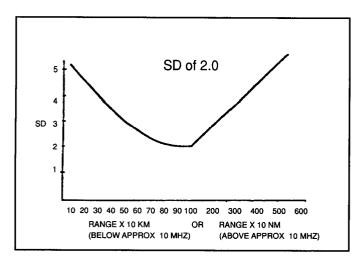


Figure 9-40. SD/distance curve for conventional DF systems.

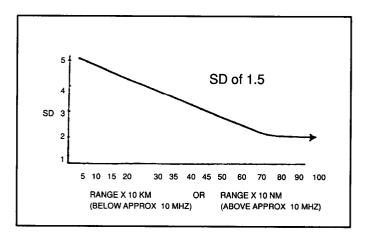


Figure 9-41. SD/distance curve for SSL.

The following formulas are variations taken from the FFIX computer algorithm and should be used to compute SD/distance tables for each site.

For frequencies less than approximately 10 MHz: SD (.285714 + .714256 R)= range weighted SD where R is greater than or equal to 10. SD $(3 - .402R + .204 R^2)$ = range weighted SD where R is less than 10.

R is distance in 100 km units.

For frequencies above approximately 10 MHz, use the same formulas and change R to be the distance in 100 Nm units.

Standard Deviation Probability Graph

As stated previously, the statistical measure of SD is dependant on the number and quality of bearings used in the formula (expressed as BM and N). The standard deviation probability graph (Figure 9-42, page 9-38) can be used to calculate the probable accuracy of any data set where the number of bearings (samples) are 1,000 or less. This chart is useful in determining how close an estimated SD will be to the true SD of the site. The vertical axis of the graph represents the total number of samples used to compute the mean bearing (BM). The horizontal axis represents the percentage of accuracy of the BM from the true bearing (BT). The diagonal line represents the percentage of time that the BM will be within the percentage of accuracy which is required. For example, assume you are working at a site which requires the BM to be accurate to within plus or minus 10 percent of the BT, 80 percent of the time. Locate the accuracy requirement of 10 percent on the bottom horizontal line of the graph. Follow that line upward until it intersects with the diagonal line (Y = .80). This

indicates the percentage of time. Now look to the left

for such accuracy requirements, a minimum of 90

the BM.

along the vertical line of the graph and you will see that

bearings (samples) must be used in the computation of

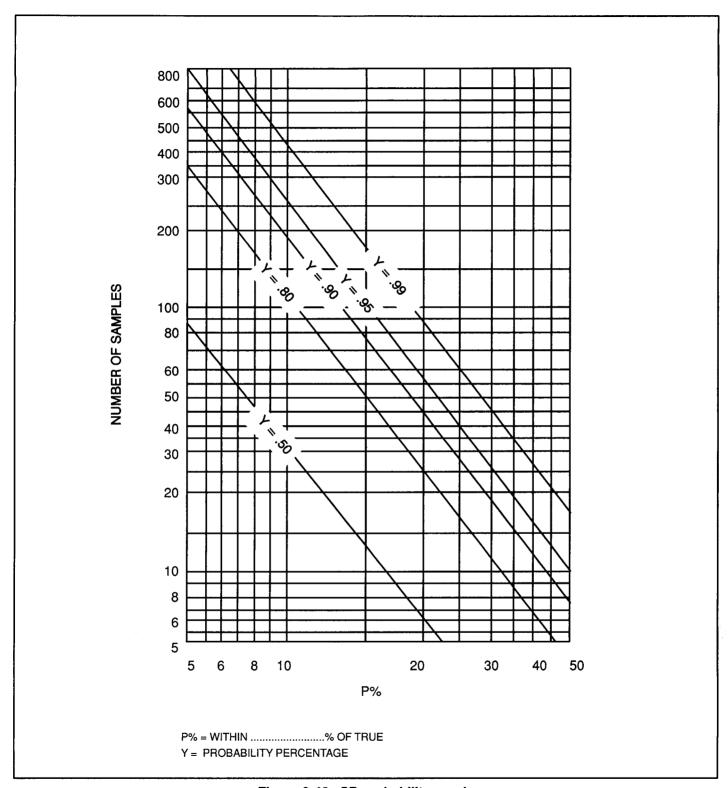


Figure 9-42. SD probability graph.

APPENDIX A

COMMON LOGARITHMS OF FUNCTIONS OF ANGLES IN DEGREES AND MINUTES TABLE

| | r | | _ | | | | | | 1 |
|---------|----------|----------------------|--------------|----------------------|--------------|----------------------|----------------------|----------|----------|
| 0°180° | | L SIN | D | L TAN | CD | L COT | L COS | | |
| 90°270° | | L COS | | L COT | | L TAN | L SIN | | |
| | ٥ | _ | | _ | | | 0.00 000 | 60 | |
| | 1 | 6.46 373 | l | 6.46 373 | | 3.53 627 | 0.00 000 | 59 | |
| | 2 | 6.76 476 | 30103 | 6.76 476 | 30103 | 3.23 524 | 0.00 000 | 58 | l . |
| | 3 | 6.94 085 | 17609 | 6.94 085 | 17609 | 3.05 915 | 0.00 000 | 57 | |
| | 4 | 7.06 579 | 12494 | 7.06 579 | 12494 | 2.93 421 | 0.00 000 | 56 | |
| | | 7 40 070 | 9691 | 7.40.070 | 9691 | 0.00.700 | | | 1 |
| | 5 | 7.16 270 | 7918 | 7.16 270 | 7918 | 2.83 730 | 0.00 000 | 55 | |
| | 6 | 7.24 188 | 6694 | 7.24 188 | 6694 | 2.75 812 | 0.00 000 | 54 50 | |
| | 7 | 7.30 882 | 5800 | 7.30 882 | 5800 | 2.69 118 | 0.00 000 | 53 | |
| | 8 9 | 7.36 682 7.41 797 | 5115 | 7.36 682 7.41 797 | 5115 | 2.63 318 2.58 203 | 0.00 000 0.00 000 | 52 51 | |
| | | 7.41707 | 4576 | 7.41 707 | 4576 | 2.50 205 | 0.00 000 | 31 | |
| | 10 | 7.46 373 | 4139 | 7.46 373 | 4139 | 2.53 627 | 0.00 000 | 50 | |
| | - 11 | 7.50 512 | 3779 | 7.50 512 | 3779 | 2.49 488 | 0.00 000 | 49 | |
| | 12 | 7.54 291 | 3476 | 7.54 291 | 3476 | 2.45 709 | 0.00 000 | 48 | |
| | 13 | 7.57 767 | 3218 | 7.57 767 | 3219 | 2.42 233 | 0.00 000 | 47 | |
| | 14 | 7.60 985 | 2997 | 7.60 986 | 2996 | 2.39 014 | 0.00 000 | 46 | |
| | 15 | 7.63 982 | | 7.63 982 | • | 2.36 018 | 0.00 000 | 45 | |
| | 16 | 7.66 784 | 2802 | 7.66 785 | 2803 | 2.33 215 | 0.00 000 | 44 | |
| | 17 | 7.69 417 | 2633 | 7.69 418 | 2633 | 2.30 582 | 9.99 999 | 43 | l |
| | 18 | 7.71 900 | 2483 | 7.71 900 | 2482 | 2.28 100 | 9.99 999 | 42 | |
| | 19 | 7.74 248 | 2348 | 7.74 248 | 2348 | 2.25 752 | 9.99 999 | 41 | |
| | 20 | 7.76 475 | 2227 | 7 76 476 | 2228 | 2 22 524 | 0.00.000 | 40 | 1 |
| | | | 2119 | 7.76 476 | 2119 | 2.23 524 | 9.99 999 | 40 | |
| | 21 | 7.78 594 | 2021 | 7.78 595 | 2020 | 2.21 405 | 9.99 999 | 39 | |
| | 22 23 | 7.80 615 7.82 545 | 1930 | 7.80 615 7.82 546 | 1931 | 2.19 385 2.17 454 | 9.99 999 9.99 999 | 38 37 | |
| | 24 | 7.84 393 | 1848 | 7.84 394 | 1848 | 2.17 454 | 9.99 999 | 36 | |
| | | 7.04 000 | 1773 | 7.04 334 | 1773 | 2.13 000 | 3.33 333 | 30 | |
| | 25 | 7.86 166 | 1704 | 7.86 167 | 1704 | 2.13 833 | 9.99 999 | 35 | |
| | 26 | 7.87 870 | 1639 | 7.87 871 | 1639 | 2.12 129 | 9.99 999 | 34 | |
| | 27 | 7.89 509 | 1579 | 7.89 510 | 1579 | 2.10 490 | 9.99 999 | 33 | |
| | 28 | 7.91 088 | 1524 | 7.91 089 | 1524 | 2.08 911 | 9.99 999 | 32 | |
| | 29 | 7.92 612 | 1472 | 7.92 613 | 1473 | 2.07 387 | 9.99 998 | 31 | |
| | 30 | 7.94 084 | | 7.94 086 | | 2.05 914 | 9.99 998 | 30 | |
| | 31 | 7.95 508 | 1424 | 7.95 510 | 1424 | 2.04 490 | 9.99 998 | 29 | |
| | 32 | 7.96 887 | 1379 | 7.96 889 | 1379 | 2.03 111 | 9.99 998 | 28 | 1 |
| | 33 | 7.98 223 | 1336 1297 | 7.98 225 | 1336 | 2.01 775 | 9.99 998 | 27 | |
| | 34 | 7.99 520 | 1259 | 7.99 522 | 1297 1259 | 2.00 478 | 9.99 998 | 26 | |
| | 35 | 8.00 779 | 1200 | 8.00 781 | 1 .200 | 1.99 219 | 9.99 998 | 25 | |
| | 36 | 8.02 002 | 1223 | 8.02 004 | 1223 | 1.97 996 | 9.99 998 | 24 | |
| | 37 | 8.03 192 | 1190 | 8.03 194 | 1190 | 1.96 806 | 9.99 997 | 23 | |
| | 38 | 8.04 350 | 1158 | 8.04 353 | 1159 | 1.95 647 | 9.99 997 | 22 | |
| | 39 | 8.05 478 | 1128 | 8.05 481 | 1128 | 1.94 519 | 9.99 997 | 21 | |
| | | 0.00.570 | 1100 | 0.00.504 | 1100 | | | | |
| | 40 | 8.06 578 | 1072 | 8.06 581 | 1072 | 1.93 419 | 9.99 997 | 20 | |
| | 41 | 8.07 650 | 1046 | 8.07 653 | 1047 | 1.92 347 | 9.99 997 | 19 | |
| | 42 43 | 8.08 696 8.09 718 | 1022 | 8.08 700 8.09 722 | 1022 | 1.91 300 1.90 278 | 9.99 997 9.99 997 | 18 17 | |
| | 44 | 8.10 717 | 999 | 8.09 722 8.10 720 | 998 - | 1.89 280 | 9.99 996 | 16 | |
| | | | 976 | | 976 | | | | |
| | 45 | 8.11 693 | 954 | 8.11 696 | 955 | 1.88 304 | 9.99 996 | 15 | |
| | 46 | 8.12 647 | 934 | 8.12 651 | 934 | 1.87 349 | 9.99 996 | 14 | |
| | 47 | 8.13 581 | 914 | 8.13 585 | 915 | 1.86 415 | 9.99 996 | 13 | |
| | 48 | 8.14 495 | 896 | 8.14 500 | 895 | 1.85 500 | 9.99 996 | 12 | |
| | 49 | 8.15 391 | 877 | 8.15 395 | 878 | 1.84 605 | 9.99 996 | 11 | |
| | 50 | 8.16 268 | 960 | 8.16 273 | 960 | 1.83 727 | 9.99 995 | 10 | |
| | 51 | 8.17 128 | 860 | 8.17 133 | 860 | 1.82 867 | 9.99 995 | 9 | |
| | 52 | 8.17 971 | 843 827 | 8.17 976 | 843 828 | 1.82 024 | 9.99 995 | 8 | |
| | 53 | 8.18 798 | 812 | 8.18 804 | 812 | 1.81 106 | 9.99 995 | 7 | |
| | 54 | 8.19 610 | 797 | 8.19 616 | 797 | 1.80 384 | 9.99 995 | 6 | |
| | 55 | 8.20 407 | | 8.20 413 | | 1.79 587 | 9.99 994 | 5 | |
| | 56 | 8.21 189 | 782 | 8.21 195 | 782 | 1.78 805 | 9.99 994 | 4 | |
| | 57 | 8.21 958 | 769 | 8.21 964 | 769 | 1.78 036 | 9.99 994 | 3 | |
| | 58 | 8.22 713 | 755 | 8.22 720 | 756 | 1.77 280 | 9.99 994 | 2 | |
| | 59 | 8.23 456 | 743 | 8.23 462 | 742 | 1.76 538 | 9.99 994 | 1 | |
| | 60 | 8.24 186 | 730 | 8.24 192 | 730 | 1.75 808 | 9.99 993 | 0 | |
| | | L SIN | | L TAN | | L COT | L COS | | 359°179° |
| | | LCOS | D | LCOT | CD | L TAN | L SIN | | 269°89° |
| | | 2000 | | 1 2001 | | 2 1014 | LON | | £0 60's |

| 1°181° | | L SIN | D | L TAN | CD | L COT | L COS | | ĺ |
|---------|----------|----------|-------------|--------------|------------|----------|----------|----------|----------|
| 91°271° | | L COS | ١ | L COT | | L TAN | L SIN | | |
| · ··· | , | 8.24 186 | | 8.24 192 | | 1.75 808 | 9.99 993 | 60 | |
| | 1 | 8.24 903 | 717 | 8.24 910 | 718 | 1.75 090 | 9.99 993 | 59 | i |
| | | | 706 | 8.25 616 | 706 | 1.74 384 | 9.99 993 | 58 | ı |
| | 2 | 8.25 609 | 695 | | 696 | | 9.99 993 | | 1 |
| | 3 | 8.26 304 | 684 | 8.26 312 | 684 | 1.73 688 | | 57 | i |
| | 4 | 8.26 988 | 673 | 8.26 996 | 673 | 1.73 004 | 9.99 992 | 56 | 1 |
| | 5 | 8.27 661 | | 8.27 669 | 1 | 1.72 331 | 9.99 992 | 55 | i |
| | 6 | 8.28 324 | 663 | 8.28 332 | 663 | 1.71 668 | 9.99 992 | 54 | i |
| | 7 | 8.28 977 | 653 | 8.28 986 | 654 | 1.71 014 | 9.99 992 | 53 | 1 |
| | | | 644 | 8.29 629 | 643 | 1.70 371 | 9.99 992 | 52 | |
| | 8 | 8.29 621 | 634 | | 634 | | | 52 51 | 1 |
| | 9 | 8.30 255 | 624 | 8.30 263 | 625 | 1.69 737 | 9.99 991 | 91 | 1 |
| | 10 | 8.30 879 | | 8.30 888 | 617 | 1.69 112 | 9.99 991 | 50 | 1 |
| | 11 | 8.31 495 | 616 | 8.31 505 | 617 | 1.68 495 | 9.99 991 | 49 | 1 |
| | 12 | 8.32 103 | 608 | 8.32 112 | 607 | 1.67 888 | 9.99 990 | 48 | |
| | 13 | 8.32 702 | 599 | 8.32 711 | 599 | 1.67 289 | 9.99 990 | 47 | Ė |
| | 14 | 8.33 292 | 590 | 8.33 302 | 591 | 1.66 698 | 9.99 990 | 46 | |
| | <u> </u> | | 583 | 5.55 5.5 | 584 | | | | İ |
| | 15 | 8.33 875 | 575 | 8.33 886 | 575 | 1.66 114 | 9.99 990 | 45 | ĺ |
| | 16 | 8.34 450 | 568 | 8.34 461 | 568 | 1.65 539 | 9.99 989 | 44 | i |
| | 17 | 8.35 018 | 560 | 8.35 029 | 561 | 1.64 971 | 9.99 989 | 43 | i |
| | 18 | 8.35 578 | 553 | 8.35 590 | 553 | 1.64 410 | 9.99 989 | 42 | i |
| | 19 | 8.36 131 | 547 | 8.36 143 | 533 546 | 1.63 857 | 9.99 989 | 41 | i |
| | | 0.00.000 | ' "' | 0.00.000 | 1 *** | 1.62.044 | 0.00.000 | 40 | i |
| | 20 | 8.36 678 | 539 | 8.36 689 | 540 | 1.63 311 | 9.99 988 | 40 | i |
| | 21 | 8.37 217 | 533 | 8.37 229 | 533 | 1.62 771 | 9.99 988 | 39 | ĺ |
| | 22 | 8.37 750 | 526 | 8.37 762 | 527 | 1.62 238 | 9.99 988 | 38 | i |
| | 23 | 8.38 276 | 520 | 8.38 289 | 520 | 1.61 711 | 9.99 987 | 37 | i |
| | 24 | 8.38 796 | 514 | 8.38 809 | 514 | 1.61 191 | 9.99 987 | 36 | i |
| | 25 | 8.39 810 | | 8.39 323 | 1 | 1.60 677 | 9.99 987 | 35 | i |
| | 26 | 8.39 818 | 506 | 8.39 832 | 509 | 1.60 168 | 9.99 986 | 34 | i |
| | 27 | 8.40 320 | 502 | 8.40 334 | 502 | 1.59 666 | 9.99 986 | 33 | 1 |
| | 28 | 8.40 816 | 496 | 8.40 830 | 496 | 1.59 170 | 9.99 986 | 32 | 1 |
| | 29 | 8.41 307 | 491 | 8.41 321 | 491 | 1.58 679 | 9.99 985 | 31 | 1 |
| | | 0.41 307 | 485 | 0.41 021 | 486 | 1.50 075 | 0.00 000 | | 1 |
| | 30 | 8.41 792 | 480 | 8.41 807 | 480 | 1.58 193 | 9.99 985 | 30 | 1 |
| | 31 | 8.42 272 | | 8.42 287 | | 1.57 713 | 9.99 985 | 29 | 1 |
| | 32 | 8.42 746 | 474 | 8.42 762 | 475 | 1.57 238 | 9.99 984 | 28 | |
| | 33 | 8.43 216 | 470 | 8.43 232 | 470 | 1.56 768 | 9.99 984 | 27 | į. |
| | 34 | 8.43 680 | 464 450 | 8.43 696 | 464 460 | 1.56 304 | 9.99 984 | 26 | i |
| | | | 459 | | +00 | | | | 1 |
| | 35 | 8.44 139 | 455 | 8.44 156 | 455 | 1.55 844 | 9.99 983 | 25 | 1 |
| | 36 | 8.44 594 | 450 | 8.44 611 | 450 | 1.55 389 | 9.99 983 | 24 | 1 |
| | 37 | 8.45 044 | 445 | 8.45 061 | 446 | 1.54 939 | 9.99 983 | 23 | 1 |
| | 38 | 8.45 489 | 441 | 8.45 507 | 441 | 1.54 493 | 9.99 982 | 22 | 1 |
| | 39 | 8.45 930 | 436 | 8.45 948 | 437 | 1.54 052 | 9.99 982 | 21 | |
| | 40 | 8.46 366 | | 8.46 385 | 1 | 1.53 615 | 9.99 982 | 20 | 1 |
| | 41 | 8.46 799 | 433 | 8.46 817 | 432 | 1.53 183 | 9.99 981 | 19 | i |
| | 42 | 8.47 226 | 427 | 8.47 245 | 428 | 1.53 755 | 9.99 981 | 18 | İ |
| | 43 | 8.47 650 | 424 | 8.47 669 | 424 | 1.52 331 | 9.99 981 | 17 | i |
| | 44 | 8.48 069 | 419 | 8.48 089 | 420 | 1.52 331 | 9.99 980 | 16 | i |
| | | 0.70 005 | 416 | 0.70 008 | 416 | 1.51 911 | 3.53 300 | اٽ ا | i |
| | 45 | 8.48 485 | ا .,, ا | 8.48 505 | اميدا | 1.51 495 | 9.99 980 | 15 | į. |
| | 46 | 8.48 896 | 411 | 8.48 917 | 412 | 1.51 083 | 9.99 979 | 14 | Í |
| | 47 | 8.49 304 | 408 | 8.49 325 | 408 404 | 1.50 675 | 9.99 979 | 13 | i |
| | 48 | 8.49 708 | 404 | 8.49 729 | | 1.50 271 | 9.99 979 | 12 | i |
| | 49 | 8.50 108 | 400 396 | 8.50 130 | 401 397 | 1.49 870 | 9.99 978 | 11 | i |
| | | | 350 | | 35/ | | 0.05.555 | | i |
| | 50 | 8.50 504 | 393 | 8.50 527 | 393 | 1.49 473 | 9.99 978 | 10 | i |
| | 51 | 8.50 897 | 390 | 8.50 920 | 390 | 1.49 080 | 9.99 977 | 9 | i |
| | 52 | 8.51 287 | 386 | 8.51 310 | 386 | 1.48 690 | 9.99 977 | 8 | i |
| | 53 | 8.51 673 | 382 | 8.51 696 | 383 | 1.48 304 | 9.99 977 | 7 | i |
| | 54 | 8.52 055 | 379 | 8.52 079 | 380 | 1.47 921 | 9.99 976 | 6 | i |
| | 55 | 8.52 434 | | 8.52 459 | 1 | 1,47 541 | 9,99 976 | 5 | i |
| | 56 | 8.52 810 | 376 | 8.52 835 | 376 | 1.47 165 | 9.99 975 | 4 | i |
| | 56 57 | 8.53 183 | 373 | 8.53 208 | 373 | 1.47 103 | 9.99 975 | 3 | İ |
| | 57 58 | 8.53 552 | 369 | 8.53 578 | 370 | 1.46 /92 | 9.99 974 | 2 | İ |
| | | | 367 | | 367 | | | | i |
| | 59 | 8.53 919 | 363 | 8.53 945 | 363 | 1.46 055 | 9.99 974 | 1 | i |
| | 60 | 8.54 282 | | 8.54 308 | | 1.45 692 | 9.99 974 | 0 | |
| | | | | L TAN | | L COT | L COS | | 358°178° |
| | | L SIN | ם | L 1/114 | CD I | | | | l |
| | | L SIN | D | LCOT | CD | L TAN | L SIN | | 268°88° |

| 2°182° | | L SIN | D | L TAN | CD | L COT | L COS | | |
|---------|----------|-------------------------------|-----|----------------------|-----|----------------------|----------------------|----------|----------|
| 92°272° | | L COS | | L COT | | L TAN | L SIN | | |
| | | 8.54 282 | | 8.54 308 | | 1.45 692 | 9.99 974 | 60 | |
| | 1 | 8.54 642 | 360 | 8.54 669 | 361 | 1.45 331 | 9.99 973 | 59 | |
| | 2 | 8.54 999 | 357 | 8.55 027 | 358 | 1.44 973 | 9.99 973 | 58 | 1 |
| | 3 | 8.55 354 | 355 | 8.55 382 | 355 | 1.44 618 | 9.99 972 | 57 | 1 |
| | 4 | 8.55 705 | 351 | 8.55 734 | 352 | 1.44 266 | 9.99 972 | 56 | l . |
| | 5 | 8.56 054 | 349 | 8.56 083 | 349 | 1.43 917 | 9.99 971 | 55 | 1 |
| | 6 | 8.56 400 | 346 | 8.56 429 | 346 | 1.43 577 | 9.99 971 | 54 | |
| | 7 | 8.56 743 | 343 | 8.56 773 | 344 | 1.43 227 | 9.99 970 | 53 | |
| | 8 | 8.57 084 | 341 | 8.57 114 | 341 | 1.42 886 | 9.99 970 | 52 | |
| | 9 | 8.57 421 | 337 | 8.57 452 | 338 | 1.43 548 | 9.99 969 | 51 | |
| | 10 | 8.57 757 | 336 | 8.57 788 | 336 | 1.42 212 | 9.99 969 | 50 | 1 |
| | 11 | 8.58 089 | 332 | 8.58 121 | 333 | 1.42 212 | 9.99 968 | 49 | |
| | 12 | 8.58 419 | 330 | 8.58 451 | 330 | 1.41 5/9 | 9.99 968 | 48 | |
| | 13 | 8.58 747 | 328 | 8.58 779 | 328 | 1.41 221 | 9.99 967 | 47 | |
| | 14 | 8.59 072 | 325 | 8.59 105 | 326 | 1.40 895 | 9.99 967 | 46 | |
| | | | 323 | | 323 | | | | • |
| | 15 | 8.59 395 | 320 | 8.59 428 | 321 | 1.40 572 | 9.99 967 | 45 | I |
| | 16 17 | 8.59 715 | 318 | 8.59 749 | 319 | 1.40 251 | 9.99 966 | 44 | |
| | 17 18 | 8.60 033 | 316 | 8.60 068 | 316 | 1.39 932 | 9.99 966 | 43 | |
| | 19 | 8.60 349 8.60 662 | 313 | 8.60 384 8.60 698 | 314 | 1.39 616 1.39 302 | 9.99 965 9.99 964 | 42 41 | |
| | | | 311 | | 311 | 1.39 302 | | *1 | 4 |
| | 20 | 8.60 973 | 309 | 8.61 009 | 310 | 1.38 991 | 9.99 964 | 40 | |
| | 21 | 8.61 282 | 307 | 8.61 319 | 307 | 1.38 681 | 9.99 963 | 39 | |
| | 22 | 8.61 569 | 305 | 8.61 626 | 305 | 1.38 374 | 9.99 963 | 38 | |
| | 23 24 | 8.61 894 8.62 196 | 302 | 8.61 931 8.62 234 | 303 | 1.38 069 | 9.99 962 | 37 | |
| | | 0.02 190 | 301 | 0.02 234 | 301 | 1.37 766 | 9.99 962 | 36 | ł. |
| | 25 | 8.62 497 | 298 | 8.62 535 | 299 | 1.37 465 | 9.99 961 | 35 | i |
| | 26 | 8.62 795 | 296 | 8.62 834 | 297 | 1.37 166 | 9.99 961 | 34 | |
| | 27 | 8.63 091 | 294 | 8.63 131 | 295 | 1.36 869 | 9.99 960 | 33 | |
| | 28 29 | 8.63 385 8.63 678 | 293 | 8.63 426 | 292 | 1.36 574 1.36 282 | 9.99 960 | 32 31 | |
| | 25 | 0.03 678 | 290 | 8.63 718 | 291 | 1.36 262 | 9.99 959 | 31 | ł. |
| | 30 | 8.63 963 | 288 | 8.64 009 | 289 | 1.35 991 | 9.99 959 | 30 | |
| | 31 | 8.64 256 | 287 | 8.64 298 | 287 | 1.35 702 | 9.99 958 | 29 | |
| | 32 | 8.64 543 | 284 | 8.64 585 | 285 | 1.35 415 | 9.99 958 | 28 | |
| | 33 34 | 8.64 827 8.65 110 | 283 | 8.64 870 8.65 154 | 284 | 1.35 130 | 9.99 957 | 27 | |
| | | 8.65 110 | 281 | 8.65 154 | 281 | 1.34 846 | 9.99 956 | 26 | |
| | 35 | 8.65 391 | 279 | 8.65 435 | 280 | 1.34 565 | 9.99 956 | 25 | |
| | 36 | 8.65 670 | 277 | 8.65 715 | 278 | 1.34 285 | 9.99 955 | 24 | |
| | 37 | 8.65 947 | 276 | 8.65 993 | 276 | 1.34 007 | 9.99 955 | 23 | |
| | 38 39 | 8.66 223 8.66 497 | 274 | 8.66 269 8.66 543 | 274 | 1.33 731 1.33 457 | 9.99 954 | 22 21 | |
| | | | 272 | 0.00 343 | 273 | 1.33 457 | 9.99 954 | 21 | 1 |
| | 40 | 8.66 769 | 270 | 8.66 816 | 271 | 1.33 184 | 9.99 953 | 20 | |
| | 41 | 8.67 039 | 269 | 8.67 087 | 269 | 1.32 913 | 9.99 952 | 19 | Ī |
| | 42 43 | 8.67 308 | 267 | 8.67 356 8.67 624 | 268 | 1.32 644 | 9.99 952 | 18 | Ī |
| | 44 | 8.67 575 8.67 841 | 266 | 8.67 624 8.67 890 | 266 | 1.32 376 1.32 110 | 9.99 951 9.99 951 | 17 16 | |
| | | | 263 | | 264 | | | | • |
| | 45 | 8.68 104 | 263 | 8.68 154 | 263 | 1.31 846 | 9.99 950 | 15 |] |
| | 46 47 | 8.68 367 | 260 | 8.68 417 | 261 | 1.31 583 | 9.99 949 | 14 | |
| | 47 48 | 8.68 627 8.68 886 | 259 | 8.68 678 8.68 938 | 260 | 1.31 322 1.31 062 | 9.99 949 9.99 948 | 13 | I |
| | 49 | 8.69 144 | 258 | 8.69 196 | 258 | 1.31 062 | 9.99 948 9.99 948 | 12 11 | |
| | | | 256 | | 257 | | | | 1 |
| | 50 51 | 8.69 400 8.69 654 | 254 | 8.69 453 8.69 708 | 255 | 1.30 547 | 9.99 947 | 10 | ì |
| | 52 | 8.69 907 | 253 | 8.69 962 | 254 | 1.30 202 1.30 038 | 9.99 946 9.99 946 | 9 8 | |
| | 53 | 8.70 159 | 252 | 8.70 214 | 252 | 1.29 786 | 9.99 945 | 7 | |
| | 54 | 8.70 409 | 250 | 8.70 465 | 251 | 1.29 535 | 9.99 944 | 6 | |
| | | | 249 | | 249 | | | | ł |
| | 55 56 | 8.70 658 8.70 905 | 247 | 8.70 714 | 248 | 1.29 286 | 9.99 944 | 5 | |
| | 56 57 | 8.70 905 8.71 1 <i>5</i> 1 | 246 | 8.70 962 8.71 208 | 246 | 1.29 038 1.28 792 | 9.99 943 | 4 | I |
| | 58 | 8.71 395 | 244 | 8.71 208 8.71 453 | 245 | 1.28 /92 1.28 547 | 9.99 942 9.99 942 | 3 2 | Ī |
| | 59 | 8.71 638 | 243 | 8.71 697 | 244 | 1.28 303 | 9.99 942 | 1 | |
| | | | 242 | | 243 | | | | |
| | 60 | 8.71 880 | | 8.71 940 | | 1.28 060 | 9.99 940 | 0 | |
| | | L SIN | D | L TAN | CD | L COT | LCOS | | 357°177° |
| | | L COS | | L COT | " | L TAN | L SIN | | 267°87° |
| | f (| | | | | | | | 20, |

| 3°183° | | L SIN | | L TAN | CD | L COT | L COS | |
|----------------------------------|----------|----------------------|------------|----------|-------|----------------------|----------|----------|
| 93 [°] 273 [°] | | L COS | Ĺ | L COT | Ĺ | L TAN | L SIN | |
| | | 0.74.000 | 1 | 0.74.040 | | 4.00.000 | 0.00.040 | |
| | 0 | 8.71 880 | 240 | 8.71 940 | 241 | 1.28 060 | 9.99 940 | 60 |
| | 1 1 | 8.72 120 | 239 | 8.72 181 | 239 | 1.27 819 | 9.99 940 | 59 |
| | 2 | 8.72 359 | 239 | 8.72 420 | 239 | 1.27 580 | 9.99 939 | 58 |
| | 3 | 8.72 597 | 237 | 8.72 659 | 237 | 1.27 341 | 9.99 938 | 57 |
| | 4 | 8.72 834 | 235 | 8.72 896 | 236 | 1.27 104 | 9.99 938 | 56 |
| | | 0.70.000 | 1 200 | 0.70.100 | 1 -~ | 1.00.000 | 0.00.027 | |
| | 5 | 8.73 069 | 234 | 8.73 132 | 234 | 1.26 868 1.26 634 | 9.99 937 | 55 54 |
| | 6 | 8.73 303 | 232 | 8.73 366 | 234 | | 9.99 936 | 54 |
| | 7 | 8.73 535 | 232 | 8.73 600 | 232 | 1.26 400 | 9.99 936 | 53 |
| | 8 | 8.73 767 | 230 | 8.73 832 | 230 | 1.26 168 | 9.99 935 | 52 |
| | 9 | 8.73 997 | 229 | 8.74 063 | 229 | 1.25 937 | 9.99 934 | 51 |
| | 10 | 8.74 226 | | 8.74 292 | 1 | 1.25 708 | 9.99 934 | 50 |
| | 11 | 8.74 454 | 228 | 8.74 521 | 229 | 1.25 479 | 9.99 933 | 49 |
| | 12 | 8.74 680 | 226 | 8.74 748 | 227 | 1.25 252 | 9.99 932 | 48 |
| | 13 | 8.74 906 | 226 | 8.74 974 | 226 | 1.25 026 | 9.99 932 | 47 |
| | 14 | 8.75 130 | 224 | 8.75 199 | 225 | 1.24 801 | 9.99 931 | 46 |
| | | 0.70 100 | 223 | 0.73 103 | 224 | 1.24 001 | 0.00 001 | <u> </u> |
| | 15 | 8.75 353 | 222 | 8.75 423 | 222 | 1.24 577 | 9.99 930 | 45 |
| | 16 | 8.75 575 | 222 | 8.75 645 | 222 | 1.24 355 | 9.99 929 | 44 |
| | 17 | 8.75 795 | 220 | 8.75 867 | 222 | 1.24 133 | 9.99 929 | 43 |
| | 18 | 8.76 015 | 219 | 8.76 087 | 219 | 1.23 913 | 9.99 928 | 42 |
| | 19 | 8.76 234 | 219 | 8.76 306 | 219 | 1.23 694 | 9.99 927 | 41 |
| | | 0.76.454 | 1 ''' | P 76 F0F | 1 -'' | 1 00 475 | 0.00.000 | |
| | 20 | 8.76 451 | 216 | 8.76 525 | 217 | 1.23 475 | 9.99 926 | 40 |
| | 21 | 8.76 667 | 216 | 8.76 742 | 216 | 1.23 258 | 9.99 926 | 39 |
| | 22 | 8.76 883 8.77 007 | 214 | 8.76 958 | 215 | 1.23 042 | 9.99 925 | 38 |
| | 23 | 8.77 097 | 213 | 8.77 173 | 214 | 1.22 827 | 9.99 924 | 37 |
| | 24 | 8.77 610 | 212 | 8.77 387 | 213 | 1.22 613 | 9.99 923 | 36 |
| | 25 | 8.77 522 | | 8.77 600 | | 1.22 400 | 9.99 923 | 35 |
| | 26 | 8.77 733 | 211 | 8.77 811 | 211 | 1.22 189 | 9.99 922 | 34 |
| | 27 | 8.77 943 | 210 | 8.78 022 | 211 | 1.21 978 | 9.99 921 | 33 |
| | 28 | 8.78 152 | 209 | 8.78 232 | 210 | 1.21 768 | 9.99 920 | 32 |
| | 29 | 8.78 360 | 208 | 8.78 441 | 209 | 1.21 559 | 9.99 920 | 31 |
| | <u> </u> | | 208 | | 208 | | | |
| | 30 | 8.78 568 | 206 | 8.78 649 | 206 | 1.21 351 | 9.99 919 | 30 |
| | 31 | 8.78 774 | 205 | 8.78 855 | 206 | 1.21 145 | 9.99 918 | 29 |
| | 32 | 8.78 979 | 204 | 8.79 061 | 205 | 1.20 939 | 9.99 917 | 28 |
| | 33 | 8.79 138 | 203 | 8.79 266 | 204 | 1.20 734 | 9.99 917 | 27 |
| | 34 | 8.79 386 | 202 | 8.79 470 | 203 | 1.20 530 | 9.99 916 | 26 |
| | 35 | 8.79 588 | | 8.79 673 | | 1.20 327 | 9.99 915 | 25 |
| | 36 | 8.79 789 | 201 201 | 8.79 875 | 202 | 1.20 125 | 9.99 914 | 24 |
| | 37 | 8.79 990 | | 8.80 076 | 201 | 1.19 924 | 9.99 913 | 23 |
| | 38 | 8.80 189 | 199 | 8.80 277 | 201 | 1.19 723 | 9.99 913 | 22 |
| | 39 | 8.80 388 | 199 | 8.80 476 | 199 | 1.19 524 | 9.99 912 | 21 |
| | | | 197 | | 198 | | | |
| | 40 | 8.80 585 | 197 | 8.80 674 | 198 | 1.19 326 | 9.99 911 | 20 |
| | 41 | 8.80 782 | 196 | 8.80 872 | 196 | 1.19 128 | 9.99 910 | 19 |
| | 42 | 8.80 978 | 195 | 8.81 068 | 196 | 1.18 932 | 9.99 909 | 18 |
| | 43 | 8.81 173 | 194 | 8.81 264 | 195 | 1.18 736 | 9.99 909 | 17 |
| | 44 | 8.81 367 | 193 | 8.81 459 | 194 | 1.18 541 | 9.99 908 | 16 |
| | 45 | 8.81 560 | 1 | 8.81 653 | | 1.18 347 | 9.99 907 | 15 |
| | 46 | 8.81 752 | 192 | 8.81 846 | 193 | 1.18 154 | 9.99 906 | 14 |
| | 47 | 8.81 944 | 192 | 8.82 038 | 192 | 1.17 962 | 9.99 905 | 13 |
| | 48 | 8.82 134 | 190 | 8.82 230 | 192 | 1.17 770 | 9.99 904 | 12 |
| | 49 | 8.82 324 | 190 | 8.82 420 | 190 | 1.17 580 | 9.99 904 | 11 |
| | E0. | 0.00.510 | 189 | 0 00 640 | 190 | 1 17 200 | 0.00.000 | 10 |
| | 50 | 8.82 513 | 188 | 8.82 610 | 189 | 1.17 390 | 9.99 903 | 10 |
| | 51 | 8.82 701 | 187 | 8.82 799 | 188 | 1.17 201 | 9.99 902 | 9 |
| | 52 52 | 8.82 888 | 187 | 8.82 987 | 188 | 1.17 013 | 9.99 901 | 8 7 |
| | 53 54 | 8.83 075 | 186 | 8.83 175 | 186 | 1.16 825 | 9.99 900 | 7 |
| | 54 | 8.83 261 | 185 | 8.83 361 | 186 | 1.16 639 | 9.99 899 | 6 |
| | 55 | 8.83 446 | 16. | 8.83 547 | 405 | 1.16 453 | 9.99 898 | 5 |
| | 56 | 8.83 630 | 184 | 8.83 732 | 185 | 1.16 268 | 9.99 898 | 4 |
| | 57 | 8.83 813 | 183 | 8.83 916 | 184 | 1.16 084 | 9.99 897 | 3 |
| | 58 | 8.83 996 | 183 | 8.84 100 | 184 | 1.15 900 | 9.99 896 | 2 |
| | 59 | 8.84 177 | 181 181 | 8.84 282 | 182 | 1.15 718 | 9.99 895 | 1 |
| | 60 | 8.84 358 | 101 | 8.84 464 | 182 | 1.15 536 | 9.99 894 | 0 |
| | | L SIN | | L TAN | | L COT | L COS | |
| | | L COS | D | L COT | CD | L TAN | L SIN | |
| | | 1 2005 | | [[| | LIAN | r SIN | |

| 4°184° | T | L SIN | | L TAN | | L COT | L COS | <u> </u> | } |
|----------------------------------|----------|----------------------|------------|----------------------|------------|----------------------|----------------------|----------|----------|
| 94 ⁰ 274 ⁰ | | L COS | D | L COT | CD | L TAN | L SIN | Ì | |
| | 0 | 8.84 358 | 404 | 8.84 464 | | 1.15 536 | 9.99 894 | 60 | 1 |
| | 1 | 8.84 539 | 181 | 8.84 646 | 182 | 1.15 354 | 9.99 893 | 59 | |
| | 2 | 8.84 718 | 179 | 8.84 826 | 180 | 1.15 174 | 9.99 892 | 58 | |
| | 3 | 8.84 897 | 179 | 8.85 006 | 180 | 1.14 994 | 9.99 891 | 57 | |
| | 4 | 8.85 075 | 178 177 | 8.85 185 | 179 178 | 1.14 815 | 9.99 891 | 56 | 1 |
| | 5 | 8.85 252 | 1 ''' | 0.05.262 | 1 '′° | 1 14 607 | 0.00.000 | | 1 |
| | 6 | 8.85 429 | 177 | 8.85 363 8.85 540 | 177 | 1.14 637 | 9.99 890 | 55 | |
| | 7 | 8.85 605 | 176 | 8.85 717 | 177 | 1.14 460 1.14 283 | 9.99 889 | 54 52 | Ĭ |
| | 8 | 8.85 780 | 175 | 8.85 893 | 176 | | 9.99 888 | 53 | |
| | 9 | 8.85 955 | 175 | 8.86 069 | 176 | 1.14 107 1.13 931 | 9.99 887 9.99 886 | 52 51 | |
| | <u> </u> | 0.00 000 | 173 | 0.00 003 | 174 | 1.13 931 | 3.33 000 | 3 | 1 |
| | 10 | 8.86 128 | 173 | 8.86 243 | 174 | 1.13 757 | 9.99 885 | 50 | |
| | 11 | 8.86 301 | 173 | 8.86 417 | 174 | 1.13 583 | 9.99 884 | 49 | |
| | 12 | 8.86 474 | 171 | 8.86 591 | 172 | 1.13 409 | 9.99 883 | 48 | |
| | 13 | 8.86 645 | 171 | 8.86 763 | 172 | 1.13 237 | 9.99 882 | 47 | |
| | 14 | 8.86 816 | 171 | 8.86 935 | 171 | 1.13 065 | 9.99 881 | 46 | |
| | 15 | 8.86 987 | | 8.87 106 | | 1.12 894 | 9.99 880 | 45 | · |
| | 16 | 8.87 156 | 169 | 8.87 277 | 171 | 1.12 723 | 9.99 879 | 44 | 1 |
| | 17 | 8.87 325 | 169 169 | 8.87 447 | 170 | 1.12 553 | 9.99 879 | 43 | 1 |
| | 18 | 8.87 494 | 167 | 8.87 616 | 169 | 1.12 384 | 9.99 878 | 42 | i |
| | 19 | 8.87 661 | 168 | 8.87 785 | 169 168 | 1.12 215 | 9.99 877 | 41 | |
| | 20 | 8.87 829 | Ì | 8.87 953 | 1 | 1.12 047 | 9.99 876 | 40 | 1 |
| | 21 | 8.87 995 | 166 | 8.88 120 | 167 | 1.11 880 | 9.99 875 | 39 | |
| | 22 | 8.88 161 | 166 | 8.88 287 | 167 | 1.11 713 | 9.99 874 | 38 | |
| | 23 | 8.88 326 | 165 | 8.88 453 | 166 | 1.11 547 | 9.99 873 | 37 | |
| | 24 | 8.88 490 | 164 | 8.88 618 | 165 | 1.11 382 | 9.99 872 | 36 | |
| | 05 | 0.00.054 | 164 | | 165 | | | | 1 |
| | 25 26 | 8.88 654 8.88 817 | 163 | 8.88 783 | 165 | 1,11 217 | 9.99 871 | 35 | |
| | 27 | 8.88 980 | 163 | 8.88 948 8.89 111 | 163 | 1.11 052 1.10 889 | 9.99 870 | 34 | i |
| | 28 | 8.89 142 | 162 | 8.89 274 | 163 | 1.10 869 | 9.99 869 9.99 868 | 33 32 | |
| | 29 | 8.89 304 | 162 | 8.89 437 | 163 | 1.10 720 | 9.99 867 | 31 | 1 |
| | | | 160 | 0.05 407 | 161 | 1.10 303 | 9.99 007 | 3 | 1 |
| | 30 | 8.89 464 | 161 | 8.89 598 | 162 | 1.10 402 | 9.99 866 | 30 | |
| | 31 | 8.89 625 | 159 | 8.89 760 | 160 | 1.10 240 | 9.99 865 | 29 | |
| | 32 | 8.89 784 | 159 | 8.89 920 | 160 | 1.10 080 | 9.99 864 | 28 | |
| | 33 34 | 8.89 943 | 159 | 8.90 080 | 160 | 1.09 920 | 9.99 863 | 27 | |
| | 34 | 8.90 102 | 158 | 8.90 240 | 159 | 1.09 760 | 9.99 862 | 26 | |
| | 35 | 8.90 260 | 457 | 8.90 399 | | 1.09 601 | 9.99 861 | 25 | |
| | 36 | 8.90 417 | 157 157 | 8.90 557 | 158 | 1.09 443 | 9.99 860 | 24 | |
| | 37 | 8.90 574 | 156 | 8.90 715 | 158 157 | 1.09 285 | 9.99 859 | 23 | |
| | 38 | 8.90 730 | 155 | 8.90 872 | 157 | 1.09 128 | 9.99 858 | 22 | |
| | 39 | 8.90 885 | 155 | 8.91 029 | 156 | 1.08 971 | 9.99 857 | 21 | |
| | 40 | 8.91 040 | | 8.91 185 | 1 | 1.08 815 | 9.99 856 | 20 | 1 |
| | 41 | 8.91 195 | 155 | 8.91 340 | 155 | 1.08 660 | 9.99 855 | 19 | I |
| | 42 | 8.91 349 | 154 | 8.91 495 | 155 | 1.08 505 | 9.99 854 | 18 | |
| | 43 | 8.91 502 | 153 153 | 8.91 650 | 155 153 | 1.08 350 | 9.99 853 | 17 | 1 |
| | 44 | 8.91 655 | 152 | 8.91 803 | 154 | 1.08 197 | 9.99 852 | 16 | |
| | 45 | 8.91 807 | | 8.91 957 | | 1.08 043 | 9.99 851 | 15 | |
| | 46 | 8.91 959 | 152 | 8.92 110 | 153 | 1.07 890 | 9.99 850 | 14 | |
| | 47 | 8.92 110 | 151 | 8.92 262 | 152 | 1.07 738 | 9.99 848 | 13 | |
| | 48 | 8.92 261 | 151 | 8.92 414 | 152 | 1.07 586 | 9.99 847 | 12 | |
| | 49 | 8.92 411 | 150 150 | 8.92 665 | 151 151 | 1.07 435 | 9.99 846 | 11 | |
| | 50 | 8.92 561 | 130 | 8.92 716 | 151 | 1.07 284 | 9.99 845 | 10 | |
| | 51 | 8.92 710 | 149 | 8.92 866 | 150 | 1.07 284 | 9.99 844 | 9 | |
| | 52 | 8.92 859 | 149 | 8.92 016 | 150 | 1.06 984 | 9.99 843 | 8 | |
| | 53 | 8.93 077 | 148 | 8.93 165 | 149 | 1.06 835 | 9.99 842 | 7 | |
| | 54 | 8.93 154 | 147 | 8.93 313 | 148 | 1.06 687 | 9.99 841 | 6 | |
| | 55 | 9 00 201 | 147 | 0.00.400 | 149 | 1.00.500 | | | |
| | 55 56 | 8.93 301 8.93 448 | 147 | 8.93 462 | 147 | 1.06 538 | 9.99 840 | 5 | |
| | 56 57 | 8.93 448 8.93 594 | 146 | 8.93 609 8.93 756 | 147 | 1.06 391 | 9.99 839 | 4 | |
| | 58 | 8.93 740 | 146 | 8.93 756 8.93 903 | 147 | 1.06 244 1.06 097 | 9.99 838 9.99 837 | 3 | |
| | 59 | 8.93 885 | 145 | 8.94 049 | 146 | 1.05 951 | 9.99 836 | 2 | |
| | | | 145 | | 146 | 1.00 001 | 3.33 030 | · | |
| 1 | 60 | 8.94 030 | | 8.94 195 | | 1.05 805 | 9.99 834 | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | | 355°175° |
| | | L COS | | L COT | | L TAN | L SIN | | 265°85° |
| | l (| | l | | | | | | |

| | | | | | | | | | A |
|----------------------------------|-------------|----------|-------|----------------------|-------|---------------------------------------|----------|----------|----------|
| 5 ⁰ 185 ⁰ | | L SIN | D | L TAN | CD | LCOT | L COS | | |
| 95 [°] 275 [°] | | L COS | | L COT | | L TAN | L SIN | | |
| | | | | | | _ | | · | |
| | 0 | 8.94 030 | 144 | 8.94 195 | 145 | 1.05 805 | 9.99 834 | 60 | İ |
| | 1 | 8.94 174 | 143 | 8.94 340 | 145 | 1.05 660 | 9.99 833 | 59 | L |
| | 2 | 8.94 317 | | 8.94 458 | | 1.05 515 | 9.99 832 | 58 | £ |
| | 3 | 8.94 461 | 144 | 8.94 630 | 145 | 1.05 370 | 9.99 831 | 57 | |
| | 4 | 8.94 603 | 142 | 8.94 773 | 143 | 1.05 227 | 9.99 830 | 56 | |
| | <u> </u> | | 143 | | 144 | | | | i |
| | 5 | 8.94 746 | 141 | 8.94 917 | 143 | 1.05 083 | 9.99 829 | 55 | 1 |
| | 6 | 8.94 887 | 1 | 8.95 060 | | 1.04 940 | 9.99 828 | 54 | |
| | 7 | 8.95 029 | 142 | 8.95 202 | 142 | 1.04 798 | 9.99 827 | 53 | 4 |
| | 8 | 8.95 170 | 141 | 8.95 344 | 142 | 1.04 656 | 9.99 825 | 52 | |
| | l š | 8.95 310 | 140 | 8.95 486 | 142 | 1.04 514 | 9.99 824 | 51 | |
| | | 0.000.0 | 140 | 0.00 400 | 141 | 1.04 0.14 | 3.55 024 | - | 1 |
| | 10 | 8.95 450 | 120 | 8.95 627 | 440 | 1.04 373 | 9.99 823 | 50 | |
| | 11 | 8.95 589 | 139 | 8.95 767 | 140 | 1.04 233 | 9.99 822 | 49 | |
| | 12 | 8.95 728 | 139 | 8.95 908 | 141 | 1.04 092 | 9.99 821 | 48 | |
| | 13 | 8.95 867 | 139 | 8.96 047 | 139 | 1.03 953 | 9.99 820 | 47 | |
| | 14 | 8.96 005 | 138 | 8.96 187 | 140 | 1.03 813 | 9.99 819 | 46 | |
| | | | 138 | | 138 | | | | 4 |
| | 15 | 8.96 143 | 127 | 8.96 325 | | 1.03 675 | 9.99 817 | 45 | |
| | 16 | 8.96 280 | 137 | 8.96 464 | 139 | 1.03 536 | 9.99 816 | 44 | |
| | 17 | 8.96 417 | 137 | 8.96 602 | 138 | 1.03 398 | 9.99 815 | 43 | |
| | 18 | 8.96 553 | 136 | 8.96 739 | 137 | 1.03 261 | 9.99 814 | 42 | |
| | 19 | 8.96 689 | 136 | 8.96 877 | 138 | 1.03 123 | 9.99 813 | 41 | |
| | | | 136 | | 136 | | | <u> </u> | ł |
| | 20 | 8.96 825 | 135 | 8.97 013 | 137 | 1.02 987 | 9.99 812 | 40 | |
| | 21 | 8.96 960 | 1 | 8.97 150 | | 1.02 850 | 9.99 810 | 39 | |
| | 22 | 8.97 095 | 135 | 8.97 285 | 135 | 1.02 715 | 9.99 809 | 38 | |
| | 23 | 8.97 229 | 134 | 8.97 421 | 136 | 1.02 579 | 9.99 808 | 37 | |
| | 24 | 8.97 363 | 134 | 8.97 556 | 135 | 1.02 444 | 9.99 807 | 36 | |
| | <u> </u> | 0.0. 000 | 133 | | 135 | | 0.00 001 | | 4 |
| | 25 | 8.97 496 | 133 | 8.97 691 | 134 | 1.02 309 | 9.99 806 | 35 | |
| | 26 | 8.97 629 | 133 | 8.97 825 | 134 | 1.02 175 | 9.99 804 | 34 | |
| | 27 | 8.97 762 | | 8.97 959 | | 1.02 041 | 9.99 803 | 33 | |
| | 28 | 8.97 894 | 132 | 8.98 002 | 133 | 1.01 908 | 9.99 802 | 32 | |
| | 29 | 8.98 026 | 132 | 8.98 225 | 133 | 1.01 775 | 9.99 801 | 31 | |
| | | | 131 | | 133 | | | | 1 |
| | 30 | 8.98 157 | 131 | 8.98 358 | 132 | 1.01 642 | 9.99 800 | 30 | |
| | 31 | 8.98 288 | 131 | 8.98 490 | 132 | 1.01 510 | 9.99 798 | 29 | |
| | 32 | 8.98 419 | 130 | 8.98 622 | 131 | 1.01 378 | 9.99 797 | 28 | |
| | 33 | 8.98 549 | | 8.98 753 | | 1.01 247 | 9.99 796 | 27 | |
| | 34 | 8.98 679 | 130 | 8.98 884 | 131 | 1.01 116 | 9.99 795 | 26 | 4 |
| | — | | 129 | | 131 | · · · · · · · · · · · · · · · · · · · | | | 4 |
| | 35 | 8.98 808 | 129 | 8.99 015 | 130 | 1.00 985 | 9.99 793 | 25 | |
| | 36 | 8.98 937 | 129 | 8.9 9 145 | 130 | 1.00 855 | 9.99 792 | 24 | 1 |
| | 37 | 8.99 066 | 128 | 8.99 275 | 130 | 1.00 725 | 9.99 791 | 23 | |
| | 38 | 8.99 194 | | 8.99 405 | | 1.00 595 | 9.99 790 | 22 | |
| | 39 | 8.99 322 | 128 | 8.99 534 | 129 | 1.00 466 | 9.99 788 | 21 | |
| | | | 128 | | 128 | | | | 1 |
| | 40 | 8.99 450 | 127 | 8.99 662 | 129 | 1.00 338 | 9.99 787 | 20 | |
| | 41 | 8.99 577 | 127 | 8.99 791 | 128 | 1.00 209 | 9.99 786 | 19 | |
| | 42 | 8.99 704 | 126 | 8.99 919 | 127 | 1.00 081 | 9.99 785 | 18 | |
| | 43 | 8.99 830 | 126 | 9.00 046 | 128 | 0.99 954 | 9.99 783 | 17 | |
| | 44 | 8.99 956 | 126 | 9.00 174 | 127 | 0.99 826 | 9.99 782 | 16 | |
| | 45 | 0.00.000 |] '20 | 0.00.004 | 1 '"′ | 0.00.000 | 0.00.704 | 4- | 1 |
| | 45 | 9.00 082 | 125 | 9.00 301 | 126 | 0.99 699 | 9.99 781 | 15 | 1 |
| | 46 | 9.00 207 | 125 | 9.00 427 | 126 | 0.99 573 | 9.99 780 | 14 | 1 |
| | 47 | 9.00 332 | 124 | 9.00 553 | 126 | 0.99 447 | 9.99 778 | 13 | 1 |
| | 48 | 9.00 456 | 125 | 9.00 679 | 126 | 0.99 321 | 9.99 777 | 12 | 1 |
| | 49 | 9.00 581 | 123 | 9.00 805 | 125 | 0.99 195 | 9.99 776 | 11 |] |
| | 50 | 9.00 704 | 1 | 9.00 930 | ľ | 0.99 070 | 9.99 775 | 10 | I |
| | 51 | 9.00 828 | 124 | 9.01 055 | 125 | 0.98 945 | | | i |
| | 52 | | 123 | | 124 | | 9.99 773 | 9 | |
| | | 9.00 951 | 123 | 9.01 179 | 124 | 0.98 821 | 9.99 772 | 8 | Ì |
| | 53 | 9.01 074 | 122 | 9.01 303 | 124 | 0.98 697 | 9.99 771 | 7 | Ĭ |
| | 54 | 9.01 196 | 122 | 9.01 427 | 123 | 0.98 573 | 9.99 769 | 6 | i |
| | 55 | 9.01 318 | | 9.01 550 | | 0.98 450 | 9.99 768 | 5 | Í |
| | 56 | 9.01 440 | 122 | 9.01 673 | 123 | 0.98 327 | 9.99 767 | 4 | İ |
| | 57 | 9.01 561 | 121 | | 123 | | | | ĺ |
| | | | 121 | 9.01 796 | 122 | 0.98 204 | 9.99 765 | 3 | 1 |
| | 58 | 9.01 682 | 121 | 9.01 918 | 122 | 0.98 082 | 9.99 764 | 2 | 1 |
| | 59 | 9.01 803 | 120 | 9.02 040 | 122 | 0.97 960 | 9.99 763 | 1 | i |
| | 60 | 9.01 923 |] | 9.02 162 | | 0.97 838 | 9.99 761 | 0 | ĺ |
| | — | L SIN | | L TAN | _ | 1 007 | 1.000 | | 354°174° |
| | | L OIN | D | LIAN | CD | L COT | L COS | | |
| | 1 | L COS | i | L COT | 1 | L TAN | L SIN | | 264°84° |
| | 1 | | | |] ! | | | | 1 |

| -00 | | r : | · | | Γ | | <u> </u> | | 1 |
|---------|----------|----------------------|------------|----------------------|------------|----------------------|----------------------|----------|----------|
| 6°186° | | L SIN | D | L TAN | CD | L COT | L COS | • | |
| 96°276° | | L COS | | L COT | | L TAN | L SIN | | |
| | 0 | 9.01 923 | | 9.02 162 | | 0.97 838 | 9.99 761 | 60 | |
| | 1 | 9.02 043 | 120 | 9.02 283 | 121 | 0.97 717 | 9.99 760 | 59 | |
| | 2 | 9.02 163 | 120 | 9.02 404 | 121 | 0.97 596 | 9.99 759 | 58 | |
| | 3 | 9.02 283 | 120 | 9.02 525 | 121 | 0.97 475 | 9.99 757 | 57 | |
| | 4 | 9.02 402 | 119 | 9.02 645 | 120 | 0.97 355 | 9.99 756 | 56 | |
| | | 9.02 520 | 118 | 0.00.700 | 121 | 0.07.004 | 0.00.755 | | • |
| | 5 | | | 9.02 766 | l | 0.97 234 | 9.99 755 | 55 | |
| | 6 7 | 9.02 639 9.02 757 | 119 | 9.02 885 9.03 005 | 119 | 0.97 115 0.96 995 | 9.99 753 | 54 53 | |
| | 8 | 9.02 874 | 118 | 9.03 003 | 120 | 0.96 995 | 9.99 752 9.99 751 | 53 52 | |
| | 9 | 9.02 992 | 117 | 9.03 242 | 119 | 0.96 758 | 9.99 749 | 51 | |
| | | 0.02.002 | 118 | 3.00 242 | 118 | 0.30 730 | 3.33 743 | ٠,٠ | i |
| | 10 | 9.03 109 | 117 | 9.03 361 | 119 | 0.96 639 | 9.99 748 | 50 | |
| | 11 | 9.03 226 | 117 | 9.03 479 | 118 | 0.96 521 | 9.99 747 | 49 | |
| | 12 | 9.03 423 | 116 | 9.03 597 | 118 | 0.96 403 | 9.99 745 | 48 | |
| | 13 | 9.03 458 | 116 | 9.03 714 | 117 | 0.96 286 | 9.99 744 | 47 | |
| | 14 | 9.03 574 | 116 | 9.03 832 | 118 | 0.96 168 | 9.99 742 | 46 | |
| | 15 | 9.03 690 | 116 | 9.03 948 | 116 | 0.96 052 | 9.99 741 | 45 | |
| | 16 | 9.03 805 | 115 | 9.04 065 | 117 | 0.95 935 | 9.99 740 | 44 | 5 |
| | 17 | 9.03 920 | 115 | 9.04 181 | 116 | 0.95 819 | 9.99 738 | 43 | |
| | 18 | 9.04 034 | 114 | 9.04 297 | 116 | 0.95 703 | 9.99 737 | 42 | |
| | 19 | 9.04 149 | 115 | 9.04 413 | 116 | 0.95 587 | 9.99 736 | 41 | |
| | 20 | 9.04 262 | 113 | 9.04 528 | 115 | 0.95.470 | 0.00.724 | 40 | 1 |
| | 20 21 | 9.04 262 9.04 376 | | 9.04 528 9.04 643 | | 0.95 472 0.95 357 | 9.99 734 9.99 733 | 40 39 | |
| | 22 | 9.04 490 | 114 | 9.04 758 | 115 | 0.95 357 | 9.99 731 | 38 | |
| | 23 | 9.04 603 | 114 | 9.04 873 | 115 | 0.95 127 | 9.99 730 | 37 | l e |
| | 24 | 9.04 715 | 113 | 9.04 987 | 115 | 0.95 013 | 9.99 728 | 36 | |
| | | | 112 | 0.01 00. | 114 | 0.00 0.0 | 0.00 720 | | |
| | 25 | 9.04 828 | 113 | 9.05 101 | 114 | 0.94 899 | 9.99 727 | 35 | |
| | 26 | 9.04 940 | 112 | 9.05 214 | 113 | 0.94 786 | 9.99 726 | 34 | |
| | 27 | 9.05 052 | 112 | 9.05 328 | 114 | 0.94 672 | 9.99 724 | 33 | |
| | 28 | 9.05 164 | 112 | 9.05 441 | 113 | 0.94 559 | 9.99 723 | 32 | |
| | 29 | 9.05 275 | 111 | 9.05 553 | 112 | 0.94 447 | 9.99 721 | 31 | |
| | 30 | 9.05 386 | 111 | 9.05 666 | 113 | 0.94 334 | 9.99 720 | 30 | |
| | 31 | 9.05 497 | 111 | 9.05 778 | 112 | 0.94 222 | 9.99 718 | 29 | |
| | 32 | 9.05 607 | 110 | 9.05 890 | 112 | 0.94 110 | 9.99 717 | 28 | |
| | 33 | 9.05 717 | 110 | 9.06 002 | 112 | 0.93 998 | 9.99 716 | 27 | |
| | 34 | 9.05 827 | 110 | 9.06 113 | 111 | 0.93 887 | 9.99 714 | 26 | |
| | 35 | 9.05 937 | 110 | 9.06 224 | 111 | 0.93 776 | 9.99 713 | 25 | |
| | 36 | 9.06 046 | | 9.06 335 | | 0.93 776 | 9.99 713 | 24 | |
| | 37 | 9.06 155 | 109 | 9.06 445 | 111 | 0.93 555 | 9.99 710 | 23 | |
| | 38 | 9.06 264 | 109 109 | 9.06 556 | 110 111 | 0.93 444 | 9.99 708 | 22 | |
| | 39 | 9.06 372 | 108 | 9.06 666 | 110 | 0.93 334 | 9.99 707 | 21 | |
| | | | 109 | | 109 | | | | |
| | 40 | 9.06 481 | | 9.06 775 | | 0.93 225 | 9.99 705 | 20 | |
| | 41 | 9.06 589 | 108 | 9.06 885 | 110 | 0.93 115 | 9.99 704 | 19 | |
| | 42 43 | 9.06 696 9.06 804 | 107 | 9.06 994 | 109 | 0.93 006 | 9.99 702 9.99 701 | 18 | |
| | 43 | 9.06 804 | 108 | 9.07 103 9.07 211 | 109 | 0.92 897 0.92 789 | 9.99 699 | 17 16 | |
| | | | 107 | | 108 | | 3.55 088 | - " | |
| | 45 | 9.07 018 | 107 | 9.07 320 | 109 | 0.92 680 | 9.99 698 | 15 | |
| | 46 | 9.07 124 | 106 | 9.07 428 | 108 | 0.92 572 | 9.99 696 | 14 | |
| | 47 | 9.07 231 | 107 | 9.07 536 | 108 | 0.92 464 | 9.99 695 | 13 | |
| | 48 | 9.07 337 | 106 | 9.07 643 | 107 | 0.92 357 | 9.99 693 | 12 | |
| | 49 | 9.07 442 | 105 | 9.07 751 | 108 | 0.92 249 | 9.99 692 | 11 | |
| | 50 | 9.07 548 | 106 | 9.07 858 | 107 | 0.92 142 | 9.99 690 | 10 | |
| | 51 | 9.07 653 | 105 | 9.07 964 | 106 | 0.92 036 | 9.99 689 | 9 | |
| | 52 | 9.07 758 | 105 | 9.08 071 | 107 | 0.91 929 | 9.99 687 | 8 | |
| | 53 | 9.07 863 | 105 | 9.08 177 | 106 | 0.91 823 | 9.99 686 | 7 | |
| | 54 | 9.07 968 | 105 | 9.08 283 | 106 | 0.91 717 | 9.99 684 | 6 | |
| | 66 | 9.08 072 | 104 | 9.08 389 | 106 | 0.01.011 | 0.00.000 | | |
| | 55 56 | 9.08 072 | ' | 9.08 389 |] | 0.91 611 0.91 505 | 9.99 683 | 5 | l . |
| | 56 57 | 9.08 176 | 104 | 9.08 495 | 106 | 0.91 505 | 9.99 681 | 4 | f |
| | 58 | 9.08 383 | 104 | 9.08 706 | 105 | 0.91 400 | 9.99 680 9.99 678 | 3 2 | |
| | 59 | 9.08 486 | 103 | 9.08 706 | 105 | 0.91 295 | 9.99 677 | 1 | |
| | | | 103 | | 105 | | | _ | |
| | 60 | 9.08 589 | 103 | 9.08 914 | 104 | 0.91 086 | 9.99 675 | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | | 353°173° |
| | | L COS | | LCOT | | L TAN | L SIN | | 263°83° |
| | | | | | |] | | | |

| 7°187° | <u> </u> | L SIN | | L TAN | | L COT | L COS | | ì |
|------------|----------|----------------------|----------|----------------------|------------|----------------------|----------------------|----------|----------|
| 97°277° | | | D | | CD | - | | | |
| 97"277" | _ | L COS | | L COT | | L TAN | L SIN | | l |
| | | 9.08 589 | 103 | 9.08 914 | 105 | 0.91 086 | 9.99 675 | 60 | |
| | | 9.08 692 | 103 | 9.09 019 | 104 | 0.90 981 | 9.99 674 | 59 | |
| | | 9.08 795 9.08 897 | 102 | 9.09 123 | 104 | 0.90 877 | 9.99 672 | 58 | ŧ |
| | | 9.08 999 | 102 | 9.09 227 9.09 330 | 103 | 0.90 773 0.90 670 | 9.99 670 9.99 669 | 57 56 | i |
| <u> </u> | | - | 102 | | 104 | | | | ł |
| | | 9.09 101 | 101 | 9.09 434 | 103 | 0.90 566 | 9.99 667 | 55 | i |
| | | 9.09 202 9.09 304 | 102 | 9.09 537 | 103 | 0.90 463 | 9.99 666 | 54 | i |
| | | 9.09 405 | 101 | 9.09 640 9.09 742 | 102 | 0.90 360 0.90 258 | 9.99 664 9.99 663 | 53 52 | ĺ |
| | | 9.09 506 | 101 | 9.09 845 | 103 | 0.90 155 | 9.99 661 | 51 | i |
| <u> </u> | | 0.00.000 | 100 | | 102 | | | | i |
| | | 9.09 606 9.09 707 | 101 | 9.09 947 9.10 049 | 102 | 0.90 053 0.89 951 | 9.99 659 | 50 | |
| | | 9.09 807 | 100 | 9.10 150 | 101 | 0.89 850 | 9.99 656 9.99 656 | 49 48 | i |
| | • | 9.09 907 | 100 | 9.10 252 | 102 | 0.89 748 | 9.99 655 | 47 | i |
| 1 | 14 | 9.10 006 | 99 | 9.10 353 | 101 | 0.89 647 | 9.99 653 | 46 | i |
| | 15 | 9.10 106 | 100 | 9.10 454 | 101 | 0.89 546 | | 45 | 1 |
| | | 9.10 205 | 99 | 9.10 454 | 101 | 0.89 546 | 9.99 651 9.99 650 | 45 44 | 1 |
| | | 9.10 304 | 99 | 9.10 666 | 101 | 0.89 344 | 9.99 648 | 43 | 1 |
| | | 9.10 402 | 98 | 9.10 756 | 100 | 0.89 244 | 9.99 647 | 42 | 1 |
| | | 9.10 501 | 99 98 | 9.10 856 | 100 100 | 0.89 144 | 9.99 645 | 41 | 1 |
| 2 | 20 ! | 9.10 599 | | 9.10 956 | 1 | 0.89 044 | 9.99 643 | 40 | 1 |
| | | 9.10 697 | 98 | 9.11 056 | 100 | 0.88 944 | 9.99 642 | 39 | 1 |
| | | 9.10 795 | 98 98 | 9.11 155 | 99 | 0.88 845 | 9.99 640 | 38 | 1 |
| | | 9.10 893 | 98 97 | 9.11 254 | 99 99 | 0.88 746 | 9.99 638 | 37 | 1 |
| 2 | 24 ! | 9.10 990 | 97 | 9.11 353 | 99 | 0.88 647 | 9.99 637 | 36 | 1 |
| 2 | 25 | 9.11 087 | | 9.11 452 | | 0.88 548 | 9.99 635 | 35 | i |
| 2 | 26 9 | 9.11 184 | 97 97 | 9.11 551 | 99 98 | 0.88 449 | 9.99 633 | 34 | i |
| | | 9.11 281 | 96 | 9.11 649 | 98 | 0.88 351 | 9.99 632 | 33 | 1 |
| | | 9.11 377 | 97 | 9.11 747 | 98 | 0.88 253 | 9.99 630 | 32 | i i |
| | 29 (| 9.11 474 | 96 | 9.11 845 | 98 | 0.88 155 | 9.99 629 | 31 | i |
| 3 | 30 9 | 9.11 570 | 96 | 9.11 943 | 97 | 0.88 057 | 9.99 627 | 30 | İ |
| | | 9.11 666 | 95 | 9.12 040 | 98 | 0.87 960 | 9.99 625 | 29 | i |
| | | 9.11 761 | 96 | 9.12 138 | 97 | 0.87 862 | 9.99 624 | 28 | i i |
| | | 9.11 857 9.11 952 | 95 | 9.12 235 9.12 332 | 97 | 0.87 765 0.87 668 | 9.99 622 9.99 620 | 27 26 | |
| <u> </u> | | | 95 | | 96 | | | | i |
| | | 9.12 047 9.12 142 | 95 | 9.12 428 | 97 | 0.87 572 | 9.99 618 | 25 | 1 |
| | | 9.12 236 | 94 | 9.12 525 9.12 621 | 96 | 0.87 475 0.87 379 | 9.99 617 9.99 615 | 24 23 | 1 |
| | | 9.12 331 | 95 | 9.12 717 | 96 | 0.87 283 | 9.99 613 | 22 | |
| | | 9.12 425 | 94 | 9.12 813 | 96 | 0.87 187 | 9.99 612 | 21 | |
| | 40 9 | 9.12 519 | 94 | 9.12 909 | 96 | 0.87.001 | 0.00.610 | 20 | i |
| | | 9.12 612 | 93 | 9.12 909 | 95 | 0.87 091 0.86 996 | 9.99 610 9.99 608 | 20 19 | 1 |
| | • | 9.12 706 | 94 | 9.13 099 | 95 | 0.86 901 | 9.99 607 | 18 | 1 |
| | | 9.12 799 | 93 | 9.13 194 | 95 | 0.86 806 | 9.99 605 | 17 | 1 |
| [4 | 44 1 | 9.12 892 | 93 93 | 9.13 289 | 95 95 | 0.86 711 | 9.99 603 | 16 | 1 |
| 4 | 45 9 | 9.12 985 | | 9.13 384 | | 0.86 616 | 9.99 601 | 15 | i |
| | | 9.13 078 | 93 | 9.13 478 | 94 | 0.86 522 | 9.99 600 | 14 | i |
| | 47 9 | 9.13 171 | 93 92 | 9.13 573 | 95 94 | 0.86 427 | 9.99 598 | 13 | i |
| | | 9.13 263 | 92 | 9.13 667 | 94 94 | 0.86 333 | 9.99 596 | 12 | i |
| 4 | 19 9 | 9.13 355 | 92 | 9.13 761 | 93 | 0.86 239 | 9.99 595 | 11 | 1 |
| | | 9.13 447 | 92 | 9.13 854 | 94 | 0.86 146 | 9.99 593 | 10 | 1 |
| | | 9.13 539 | 92 91 | 9.13 948 | 93 | 0.86 052 | 9.99 591 | 9 | i |
| | | 9.13 630 | 92 | 9.14 041 | 93 | 0.85 959 | 9.99 589 | 8 | i |
| | | 9.13 772 | 91 | 9.14 134 | 93 | 0.85 866 | 9.99 588 | 7 | i |
| ∟ ° | 54 9 | 9.13 813 | 91 | 9.14 227 | 93 | 0.85 773 | 9.99 586 | 6 | 1 |
| | | 9.13 904 | 90 | 9.14 320 | 92 | 0.85 680 | 9.99 584 | 5 | 1 |
| | | 9.13 994 | 91 | 9.14 412 | 92 | 0.85 588 | 9.99 582 | 4 | i |
| | | 9.14 085 | 90 | 9.14 504 | 93 | 0.85 496 | 9.99 581 | 3 | i |
| | | 9.14 175 | 91 | 9.14 597 | 91 | 0.85 403 | 9.99 579 | 2 | l |
| <u> </u> | | 9.14 266 | 90 | 9.14 688 | 92 | 0.85 312 | 9.99 577 | 1 | 1 |
| 6 | 50 5 | 9.14 356 | | 9.14 780 | | 0.85 220 | 9.99 575 | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | | 352°172° |
| | | | | | | | | | 4 |
| | | L COS | | L COT | | L TAN | L SIN | | 262°82° |

| 8°188° | | L SIN | D | L TAN | CD | L COT | L COS | | |
|---------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|----------|----------|
| 98°278° | | L COS | | L COT | | L TAN | L SIN | | |
| | ٥ | 9.14 356 | | 9.14 780 | | 0.85 220 | 9.99 575 | 60 | |
| | 1 | 9.14 445 | 89 | 9.14 872 | 92 | 0.85 128 | 9.99 574 | 59 | |
| | 2 | 9.14 535 | 90 | 9.14 963 | 91 | 0.85 037 | 9.99 572 | 58 | |
| | 3 | 9.14 624 | 89 | 9.15 054 | 91 | 0.84 946 | 9.99 570 | 57 | |
| | 4 | 9.14 714 | 90 | 9.15 145 | 91 | 0.84 855 | 9.99 568 | 56 | |
| | | 3.14714 | 89 | 3.13 140 | 91 | 0.04 000 | 0.00 000 | | |
| | 5 | 9.14 803 | 88 | 9.15 236 | 91 | 0.84 764 | 9.99 566 | 55 | |
| | 6 | 9.14 891 | 89 | 9.15 327 | 90 | 0.84 673 | 9.99 565 | 54 | |
| | 7 | 9.14 980 | 89 | 9.15 417 | 91 | 0.84 583 | 9.99 563 | 53 | |
| | 8 | 9.15 069 | 88 | 9.15 508 | 90 | 0.84 492 | 9.99 561 | 52 | |
| | 9 | 9.15 157 | 88 | 9.15 598 | 90 | 0.84 402 | 9.99 559 | 51 | |
| | 10 | 9.15 245 | | 9.15 688 | | 0.84 312 | 9.99 557 | 50 | |
| | 11 | 9.15 333 | 88 | 9.15 777 | 89 | 0.84 223 | 9.99 556 | 49 | |
| | 12 | 9.15 421 | 88 | 9.15 867 | 90 | 0.84 133 | 9.99 554 | 48 | |
| | 13 | 9.15 508 | 87 | 9.15 956 | 89 | 0.84 044 | 9.99 552 | 47 | |
| | 14 | 9.15 596 | 88 | 9.16 046 | 90 | 0.83 954 | 9.99 550 | 46 | |
| | 15 | 0.45.000 | 87 | 0.16.105 | 89 | 0.00.005 | 0.00 548 | 45 | |
| | 15 | 9.15 683 | 87 | 9.16 135 9.16 224 | 89 | 0.83 865 0.83 776 | 9.99 548 9.99 546 | 45 | |
| | 16 17 | 9.15 770 9.15 857 | 87 | 9.16 224 | 88 | 0.83 688 | 9.99 545 | 44 43 | |
| | 18 | 9.15 944 | 87 | 9.16 401 | 89 | 0.83 599 | 9.99 543 | 42 | |
| | 19 | 9.16 030 | 86 | 9.16 489 | 88 | 0.83 588 | 9.99 541 | 41 | |
| | ., | 3.10 000 | 86 | 3.10 403 | 88 | 0.00 011 | 3.33 547 | - | |
| | 20 | 9.16 116 | 87 | 9.16 577 | 88 | 0.83 423 | 9.99 539 | 40 | |
| | 21 | 9.16 203 | 86 | 9.16 665 | 88 | 0.83 335 | 9.99 537 | 39 | |
| | 22 | 9.16 289 | 85 | 9.16 753 | 88 | 0.83 247 | 9.99 535 | 38 | |
| | 23 | 9.16 374 | 86 | 9.16 841 | 87 | 0.83 159 | 9.99 533 | 37 | |
| | 24 | 9.16 460 | 85 | 9.16 928 | 88 | 0.83 072 | 9.99 532 | 36 | |
| | 25 | 9.16 545 | •• | 9.17 016 |] `` | 0.82 984 | 9.99 530 | 35 | |
| | 26 | 9.16 631 | 86 | 9.17 103 | 87 | 0.82 897 | 9.99 528 | 34 | |
| | 27 | 9.16 716 | 85 | 9.17 190 | 87 | 0.82 810 | 9.99 526 | 33 | |
| | 28 | 9,16 801 | 85 | 9.17 277 | 87 | 0.82 723 | 9.99 524 | 32 | |
| | 29 | 9.16 886 | 85 | 9.17 363 | 86 | 0.82 637 | 9.99 522 | 31 | |
| | 20 | 0.40.070 | 84 | 0.47.460 | 87 | 0.00.550 | 0.00 500 | 20 | |
| | 30 | 9.16 970 | 85 | 9.17 450 | 86 | 0.82 550 | 9.99 520 | 30 | |
| | 31 32 | 9.17 055 9.17 139 | 84 | 9.17 536 9.17 622 | 86 | 0.82 464 0.82 378 | 9.99 518 9.99 517 | 29 28 | |
| | 33 | 9.17 223 | 84 | 9.17 708 | 86 | 0.82 378 | 9.99 515 | 27 | |
| | 34 | 9.17 307 | 84 | 9.17 794 | 86 | 0.82 292 | 9.99 513 | 26 | |
| | | 5.17 557 | 84 | 0.17 70 7 | 86 | 0.02 200 | | | |
| | 35 | 9.17 391 | 83 | 9.17 880 | 85 | 0.82 120 | 9.99 511 | 25 | |
| | 36 | 9.17 474 | 84 | 9.17 965 | 86 | 0.82 035 | 9.99 509 | 24 | |
| | 37 | 9.17 558 | 83 | 9.18 051 | 85 | 0.81 949 | 9.99 507 | 23 | |
| | 38 | 9.17 641 | 83 | 9.18 136 | 85 | 0.81 864 | 9.99 505 | 22 | |
| | 39 | 9.17 724 | 83 | 9.18 221 | 85 | 0.81 779 | 9.99 503 | 21 | |
| | 40 | 9.17 807 | ا م | 9.18 306 | | 0.81 694 | 9.99 501 | 20 | |
| | 41 | 9.17 890 | 83 | 9.18 391 | 85 | 0.81 609 | 9.99 499 | 19 | |
| | 42 | 9.17 973 | 83 82 | 9.18 475 | 84 85 | 0.81 525 | 9.99 497 | 18 | |
| | 43 | 9.18 055 | 82 82 | 9.18 560 | | 0.81 440 | 9.99 495 | 17 | |
| | 44 | 9.18 137 | 83 | 9.18 644 | 84 84 | 0.81 356 | 9.99 494 | 16 | |
| | 45 | 9.18 220 | | 9.18 728 |] | 0.81 272 | 9.99 492 | 15 | |
| 1 | 46 | 9.18 302 | 82 | 9.18 812 | 84 | 0.81 188 | 9.99 490 | 14 | |
| | 47 | 9.18 383 | 81 | 9.18 896 | 84 | 0.81 104 | 9.99 488 | 13 | |
| | 48 | 9.18 465 | 82 | 9.18 979 | 83 | 0.81 021 | 9.99 486 | 12 | |
| | 49 | 9.18 547 | 82 | 9.19 063 | 84 | 0.80 937 | 9.99 484 | 11 | |
| | 50 | 9.18 628 | 81 | 9,19 146 | 83 | 0.80 854 | 9.99 482 | 10 | |
| 1 | 50 51 | 9.18 628 | 81 | 9.19 146 9.19 229 | 83 | 0.80 854 | 9.99 482 9.99 480 | 9 | |
| | 52 | 9.18 790 | 81 | 9.19 229 | 83 | 0.80 771 | 9.99 480 9.99 478 | 8 | |
| | 53 | 9.18 871 | 81 | 9.19 395 | 83 | 0.80 605 | 9.99 476 | 7 | |
| | 54 | 9.18 952 | 81 | 9.19 478 | 83 | 0.80 522 | 9.99 474 | 6 | |
| i | <u> </u> | | 81 | | 83 | | | | |
| 1 | 55 | 9.19 033 | 80 | 9.19 561 | 82 | 0.80 439 | 9.99 472 | 5 | |
| | 56 | 9.19 113 | 80 | 9.19 643 | 82 | 0.80 357 | 9.99 470 | 4 | |
| | 57 | 9.19 193 | 80 | 9.19 725 | 82 | 0.80 275 | 9.99 468 | 3 | |
| | 58 | 9.19 273 | 80 | 9.19 807 | 82 | 0.80 193 | 9.99 466 | 2 | |
| | 59 | 9.19 353 | 80 | 9.19 889 | 82 | 0.80 111 | 9.99 464 | 1 | |
| | 60 | 9.19 433 | | 9.19 971 | | 0.80 029 | 9.99 462 | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | | 351°171° |
| | | L COS | | L COT | " | L TAN | L SIN | | 261°81° |
| | | | l | l | | | | | l |

| 9°189° | | L SIN | O. | L TAN | CD | L COT | L COS | | |
|---------|----------|----------------------|----|----------------------|----------|----------------------|----------|----|----------|
| 99°279° | | L COS | | L COT | | L TAN | L SIN | | |
| | 0 | 0.10.422 | | 0.10.071 | | 0.90.000 | 0.00.460 | | |
| | | 9.19 433 | 80 | 9.19 971 | 82 | 0.80 029 | 9.99 462 | 60 | |
| | 1 1 | 9.19 513 | 79 | 9.20 053 | 81 | 0.79 947 | 9.99 460 | 59 | |
| | 2 | 9.19 592 | 80 | 9.20 134 | 82 | 0.79 866 | 9.99 458 | 58 | |
| | 3 | 9.19 672 | 79 | 9.20 216 | 81 | 0.79 784 | 9.99 456 | 57 | 1 |
| | 4 | 9.19 751 | | 9.20 297 | | 0.79 703 | 9.99 454 | 56 | |
| | | | 79 | | 81 | | | | 1 |
| | 5 | 9.19 830 | 79 | 9.20 378 | 81 | 0.79 622 | 9.99 452 | 55 | 1 |
| | 6 | 9.19 909 | | 9.20 459 | | 0.79 541 | 9.99 450 | 54 | |
| | 7 | 9.19 988 | 79 | 9.20 540 | 81 | 0.79 460 | 9.99 448 | 53 | |
| | 8 | 9.20 067 | 79 | 9.20 621 | 81 | 0.79 379 | 9.99 446 | 52 | |
| | 9 | 9.20 145 | 78 | 9.20 701 | 80 | 0.79 299 | 9.99 444 | 51 | |
| | <u> </u> | 3.20 140 | 78 | 3.20 701 | 81 | 0.75 200 | 0.00 111 | j | |
| | 10 | 9.20 223 | | 9.20 782 | | 0.79 218 | 9.99 442 | 50 | |
| | 11 | 9.20 302 | 79 | 9.20 862 | 80 | 0.79 138 | 9.99 440 | 49 | |
| | 12 | 9.20 380 | 78 | 9.20 942 | 80 | 0.79 058 | 9.99 438 | 48 | l |
| | 13 | 9.20 458 | 78 | 9.21 022 | 80 | 0.78 978 | | 47 | |
| | | | 77 | | 80 | | 9.99 436 | | |
| | 14 | 9.20 535 | 78 | 9.21 102 | 80 | 0.78 898 | 9.99 434 | 46 | |
| | 15 | 9.20 613 | | 9.21 182 | | 0.78 818 | 9.99 432 | 45 | |
| | 16 | 9.20 691 | 78 | 9.21 261 | 79 | 0.78 739 | 9.99 429 | 44 | |
| | | | 77 | | 80 | | | | I |
| | 17 | 9.20 768 | 77 | 9.21 341 | 79 | 0.78 659 | 9.99 427 | 43 | I |
| | 18 | 9.20 845 | 77 | 9.21 420 | 79 | 0.78 580 | 9.99 425 | 42 | I |
| | 19 | 9.20 922 | 77 | 9.21 499 | 79 | 0.78 501 | 9.99 423 | 41 | ł |
| | 20 | 9.20 999 | | 9,21 578 | } | 0.78 422 | 9.99 421 | 40 | |
| | 21 | 9.21 076 | 77 | 9.21 657 | 79 | 0.78 343 | 9.99 419 | 39 | |
| | 22 | 9.21 153 | 77 | 9.21 736 | 79 | 0.78 264 | 9.99 417 | 38 | |
| | 23 | | 76 | | 78 | | | 38 | Ī |
| | | 9.21 229 | 77 | 9.21 814 | 79 | 0.78 186 | 9.99 415 | | Ĭ |
| | 24 | 9.21 306 | 76 | 9.21 893 | 78 | 0.78 107 | 9.99 413 | 36 | |
| | 25 | 9.21 382 | | 9.21 971 | | 0.78 029 | 9.99 411 | 35 | |
| | 26 | 9.21 458 | 76 | 9.22 049 | 78 | 0.77 951 | 9.99 409 | 34 | I |
| | 27 | 9.21 534 | 76 | 9.22 127 | 78 | 0.77 873 | 9.99 407 | 33 | |
| | 28 | 9.21 610 | 76 | 9.22 205 | 78 | 0.77 795 | 9.99 404 | 32 | Ī |
| | 28 29 | | 75 | 9.22 205 9.22 283 | 78 | | | 31 | Ī |
| | 25 | 9.21 685 | 76 | 9.22 203 | 78 | 0.77 717 | 9.99 402 | 31 | Ī |
| | 30 | 9.21 761 | | 9.22 361 | l | 0.77 639 | 9.99 400 | 30 | Ī |
| | 31 | 9.21 836 | 75 | 9.22 438 | 77 | 0.77 562 | 9.99 398 | 29 | |
| | 32 | 9.21 912 | 76 | 9.22 516 | 78 | 0.77 484 | 9.99 396 | 28 | I |
| | 33 | 9.21 987 | 75 | 9.22 593 | 77 | 0.77 407 | 9.99 394 | 27 | |
| | 33 | 9.22 062 | 75 | 9.22 593 9.22 670 | 77 | 0.77 330 | 9.99 392 | 26 | Ī |
| | 34 | 3.22 UGZ | 75 | 5.22 0/0 | 77 | 0.77 330 | J.33 382 | ده | Ī |
| | 35 | 9.22 137 | ~. | 9.22 747 | | 0.77 253 | 9.99 390 | 25 | Ī |
| | 36 | 9.22 211 | 74 | 9.22 824 | 77 | 0.77 176 | 9.99 388 | 24 | I |
| | 37 | 9.22 286 | 75 | 9.22 901 | 77 | 0.77 099 | 9.99 385 | 23 | |
| | 38 | 9.22 361 | 75 | 9.22 977 | 76 | 0.77 033 | 9.99 383 | 22 | I |
| | | | 74 | | 77 | | | | |
| | 39 | 9.22 435 | 74 | 9.23 054 | 76 | 0.76 945 | 9.99 381 | 21 | |
| | 40 | 9.22 509 | | 9.23 130 | 1 | 0.76 870 | 9.99 379 | 20 | Ī |
| | 41 | 9.22 583 | 74 | 9.23 206 | 76 | 0.76 794 | 9.99 377 | 19 | 1 |
| | 42 | 9.22 657 | 74 | 9.23 283 | 77 | 0.76 717 | 9.99 375 | 18 | |
| | 43 | | 74 | | 76 | | | 17 | I |
| | 43 | 9.22 731 9.22 805 | 74 | 9.23 359 | 76 | 0.76 641 0.76 565 | 9.99 372 | | I |
| | - 44 | J.ZZ 805 | 73 | 9.23 435 | 75 | U./6 565 | 9.99 370 | 16 | |
| | 45 | 9.22 878 | i | 9.23 510 | | 0.76 490 | 9.99 368 | 15 | |
| | 46 | 9.22 952 | 74 | 9.23 586 | 76 | 0.76 414 | 9.99 366 | 14 | 1 |
| | 47 | 9.23 025 | 73 | 9.23 661 | 75 | 0.76 339 | 9.99 364 | 13 | |
| | | | 73 | | 76 | | | | |
| | 48 | 9.23 098 | 73 | 9.23 737 | 75 | 0.76 263 | 9.99 362 | 12 | |
| | 49 | 9.23 171 | 73 | 9.23 812 | 75 | 0.76 188 | 9.99 359 | 11 | |
| | 50 | 9.23 244 | | 9,23 887 | | 0.76 113 | 9.99 357 | 10 | Ī |
| | 51 | 9.23 317 | 73 | 9.23 962 | 75 | 0.76 038 | 9.99 355 | 9 | |
| | 52 | 9.23 390 | 73 | 9.23 902 | 75 | 0.76 038 | 9.99 353 | 8 | I |
| | | | 72 | | 75 | | | | |
| | 53 | 9.23 462 | 73 | 9.24 112 | 74 | 0.75 888 | 9.99 351 | 7 | |
| | 54 | 9.23 535 | 72 | 9.24 186 | 75 | 0.75 814 | 9.99 348 | 6 | |
| | 55 | 9.23 607 | | 9.24 261 | l ' | 0.75 739 | 9.99 346 | 5 | Ī |
| | 56 | 9.23 679 | 72 | 9.24 281 | 74 | 0.75 739 | | 4 | |
| | | 9.23 679 9.23 752 | 73 | | 75 | | 9.99 344 | 1 | I |
| | 57 59 | | 71 | 9.24 410 | 74 | 0.75 590 | 9.99 342 | 3 | |
| | 58 | 9.23 823 | 72 | 9.24 484 | 74 | 0.75 516 | 9.99 340 | 2 | Ī |
| | 59 | 9.23 895 | 72 | 9.24 558 | 74 | 0.75 442 | 9.99 337 | 1 | |
| | 60 | 9.23 967 | | 9.24 632 | ا ا | 0.75 368 | 9.99 335 | 0 | |
| | | L SIN | 2 | L TAN | CD | L COT | L COS | | 350°170° |
| | | | D | | CD | | | | 0 |
| | 1 | L COS | | L COT | | L TAN | L SIN | | 260°80° |
| | 1 | 1 | \ | 1 | 1 | | |) | |
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| | | | | • | | T . | | | 1 |
|----------------------------------|----------|----------------------|----------|----------------------|-------------|----------------------|----------------------|----------|----------|
| 10 ⁰ 190 ⁰ | | L SIN | D | L TAN | CD | L COT | L COS | } | |
| 100°.280° | | L COS | | L COT | ļ | L TAN | L SIN | | |
| | 0 | 9.23 967 | | 9.24 632 | l _ | 0.75 368 | 9.99 335 | 60 | |
| | 1 | 9.24 039 | 72 | 9.24 706 | 74 | 0.75 294 | 9.99 333 | 59 | 1 |
| | 2 | 9.24 110 | 71 | 9.24 779 | 73 | 0.75 221 | 9.99 331 | 58 | |
| | 3 | 9.24 181 | 71 | 9.24 853 | 74 | 0.75 147 | 9.99 328 | 57 | 1 |
| | 4 | 9.24 253 | 72 71 | 9.24 926 | 73 74 | 0.75 074 | 9.99 326 | 56 | |
| | 5 | 9.24 324 | l | 9.25 000 | 1 | 0.75 000 | 9.99 324 | 55 | |
| | 6 | 9.24 395 | 71 | 9.25 073 | 73 | 0.74 927 | 9.99 322 | 54 | |
| | 7 | 9.24 466 | 71 | 9.25 146 | 73 | 0.74 854 | 9.99 319 | 53 | |
| | 8 | 9.24 536 | 70 | 9.25 219 | 73 | 0.74 781 | 9.99 317 | 52 | |
| | 9 | 9.24 607 | 71 70 | 9.25 292 | 73 73 | 0.74 708 | 9.99 315 | 51 | |
| | 10 | 9.24 677 | 1 ~ | 9.25 365 | 1 ′° | 0.74 635 | 9.99 313 | 50 | 1 |
| | 11 | 9.24 748 | 71 | 9.25 437 | 72 | 0.74 563 | 9.99 310 | 49 | 1 |
| | 12 | 9.24 818 | 70 | 9.25 510 | 73 | 0.74 490 | 9.99 308 | 48 | i |
| | 13 | 9.24 888 | 70 | 9.25 582 | 72 | 0.74 418 | 9.99 306 | 47 | |
| | 14 | 9.24 958 | 70 | 9.25 655 | 73 | 0.74 345 | 9.99 304 | 46 | |
| | 4.5 | 0.05.000 | 70 | | 72 | | | | 1 |
| | 15 16 | 9.25 028 | 70 | 9.25 727 | 72 | 0.74 273 | 9.99 301 | 45 | |
| | 16 17 | 9.25 098 9.25 168 | 70 | 9.25 799 | 72 | 0.74 201 | 9.99 299 | 44 | 1 |
| | 17 18 | 9.25 168 | 69 | 9.25 871 | 72 | 0.74 129 | 9.99 297 | 43 | |
| | 19 | 9.25 237 9.25 307 | 70 | 9.25 943 9.26 015 | 72 | 0.74 057 0.73 985 | 9.99 294 9.99 292 | 42 41 | 1 |
| | | | 69 | | 71 | | | | Į. |
| | 20 | 9.25 376 | 69 | 9.26 086 | 72 | 0.73 914 | 9.99 290 | 40 | |
| | 21 | 9.25 445 | 69 | 9.26 158 | 71 | 0.73 842 | 9.99 288 | 39 | |
| | 22 | 9.25 514 | 69 | 9.26 229 | 72 | 0.73 771 | 9.99 285 | 38 | |
| | 23 | 9.25 583 | 69 | 9.26 301 | 71 | 0.73 699 | 9.99 283 | 37 | |
| | 24 | 9.25 652 | 69 | 9.26 372 | 71 | 0.73 628 | 9.99 281 | 36 | I |
| | 25 | 9.25 721 | | 9.26 443 | | 0.73 557 | 9.99 278 | 35 | |
| | 26 | 9.25 790 | 69 68 | 9.26 514 | 71 | 0.73 486 | 9.99 276 | 34 | |
| | 27 | 9.25 858 | 69 | 9.26 585 | 71 70 | 0.73 415 | 9.99 274 | 33 | |
| | 28 | 9.25 927 | 68 | 9.26 665 | 70 | 0.73 345 | 9.99 271 | 32 | 1 |
| | 29 | 9.25 995 | 68 | 9.26 726 | 71 | 0.73 274 | 9.99 269 | 31 | |
| | 30 | 9.26 063 | | 9.26 797 | 1 ′′ | 0.73 203 | 9.99 267 | 30 | 1 |
| | 31 | 9.26 131 | 68 | 9.26 867 | 70 | 0.73 133 | 9.99 264 | 29 | |
| | 32 | 9.26 199 | 68 | 9.26 937 | 70 | 0.73 063 | 9.99 262 | 28 | |
| | 33 | 9.26 267 | 68 | 9.27 008 | 71 | 0.72 992 | 9.99 260 | 27 | |
| | 34 | 9.26 335 | 68 | 9.27 078 | 70 | 0.72 922 | 9.99 257 | 26 | |
| | 35 | 9.26 403 | 68 | 9.27 148 | 70 | 0.72 852 | 9.99 255 | 25 | 1 |
| | 36 | 9.26 470 | 67 | 9.27 218 | 70 | 0.72 782 | 9.99 252 | 25 24 | |
| | 37 | 9.26 538 | 68 | 9.27 288 | 70 | 0.72 712 | 9.99 250 | 23 | |
| | 38 | 9.26 605 | 67 | 9.27 357 | 69 | 0.72 643 | 9.99 248 | 22 | |
| | 39 | 9.26 672 | 67 | 9.27 427 | 70 | 0.72 573 | 9.99 245 | 21 | |
| | 40 | 9.26 739 | 67 | 0.27.406 | 69 | | | | I |
| | 40 | 9.26 739 | 67 | 9.27 496 9.27 566 | 70 | 0.72 504 | 9.99 243 | 20 | l |
| | 42 | 9.26 873 | 67 | 9.27 635 | 69 | 0.72 434 0.72 365 | 9.99 241 9.99 238 | 19 18 | 1 |
| | 43 | 9.26 940 | 67 | 9.27 704 | 69 | 0.72 305 | 9.99 236 9.99 236 | 17 | I |
| | 44 | 9.27 007 | 67 | 9.27 773 | 69 | 0.72 227 | 9.99 233 | 16 | Ī |
| | , | | 66 | | 69 | | | | |
| | 45 46 | 9.27 073 | 67 | 9.27 842 | 69 | 0.72 158 | 9.99 231 | 15 | |
| | 46 47 | 9.27 140 | 66 | 9.27 911 | 69 | 0.72 089 | 9.99 229 | 14 | |
| | 47 48 | 9.27 206 9.27 273 | 67 | 9.27 980 9.28 049 | 69 | 0.72 020 0.71 951 | 9.99 226 | 13 | |
| | 49 | 9.27 339 | 66 | 9.28 049 | 68 | 0.71 951 0.71 883 | 9.99 224 9.99 221 | 12 11 | |
| | \vdash | · | 66 | | 69 | | | | |
| | 50 | 9.27 405 | 66 | 9.28 186 | 68 | 0.71 814 | 9.99 219 | 10 | |
| | 51 50 | 9.27 471 | 66 | 9.28 254 | 69 | 0.71 746 | 9.99 217 | 9 | |
| | 52 53 | 9.27 537 | 65 | 9.28 323 | 68 | 0.71 677 | 9.99 214 | 8 | |
| | 53 54 | 9.27 602 9.27 668 | 66 | 9.28 391 9.28 459 | 68 | 0.71 609 0.71 541 | 9.99 212 9.99 209 | 7 | |
| | - | | 66 | | 68 | V./ (341 | 5.88 ZUB | Lů | |
| | 55 | 9.27 734 | 65 | 9.28 527 | 68 | 0.71 473 | 9.99 207 | 5 | |
| | 56 | 9.27 799 | 65 | 9.28 595 | 67 | 0.71 405 | 9.99 204 | 4 | |
| | 57 | 9.27 864 | 66 | 9.28 662 | 68 | 0.71 338 | 9.99 202 | 3 | |
| | 58 50 | 9.27 930 | 65 | 9.28 730 | 68 | 0.71 270 | 9.99 200 | 2 | |
| | 59 | 9.27 995 | 65 | 9.28 798 | 67 | 0.71 202 | 9.99 197 | 1 | |
| | 60 | 9.28 060 | | 9.28 865 | | 0.71 135 | 9.99 195 | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | | 349°169° |
| | | L COS | | L COT | | L TAN | L SIN | | 259°79° |
| | I (| | | | | | | | |

| 11°191° | | L SIN | Γ - | L TAN | T . | L COT | L COS | |] |
|----------|--------------|----------------------|----------|----------------------|--|----------------------|----------------------|----------|-----------------------------------|
| 101°281° | | L COS | D | L COT | CD | L TAN | L SIN | | |
| | 0 | 9.28 060 | | 9.28 865 | | 0.71 135 | 9.99 195 | | |
| | ı | 9.28 125 | 65 | 9.28 933 | 68 | 0.71 135 | 9.99 193 | 60 59 | |
| | 2 | 9.28 190 | 65 | 9.29 000 | 67 | 0.71 000 | 9.99 190 | 58 | Ĭ |
| | 3 | 9.28 254 | 64 65 | 9.29 067 | 67 | 0.70 933 | 9.99 187 | 57 | |
| | 4 | 9.28 319 | 65 65 | 9.29 134 | 67 67 | 0.70 866 | 9.99 185 | 56 | |
| | 5 | 9.28 384 | 1 | 9.29 201 | 1 | 0.70 799 | 9.99 182 | 55 | |
| | 6 | 9.28 448 | 64 | 9.29 268 | 67 | 0.70 732 | 9.99 180 | 54 | |
| | 7 | 9.28 512 | 6 65 | 9.29 335 | 67 | 0.70 665 | 9.99 177 | 53 | |
| | 8 | 9.28 577 | 64 | 9.29 402 | 67 66 | 0.70 598 | 9.99 175 | 52 | |
| | 9 | 9.28 641 | 64 | 9.29 468 | 67 | 0.70 532 | 9.99 172 | 51 | |
| | 10 | 9.28 705 | | 9.29 535 | | 0.70 465 | 9.99 170 | 50 | 1 |
| | 11 | 9.28 769 | 64 64 | 9.29 601 | 66 | 0.70 399 | 9.99 167 | 49 | |
| | 12 | 9.28 833 | 63 | 9.29 668 | 67 66 | 0.70 332 | 9.99 165 | 48 | |
| | 13 | 9.28 896 | 64 | 9.29 734 | 66 | 0.70 266 | 9.99 162 | 47 | |
| | 14 | 9.28 960 | 64 | 9.29 800 | 66 | 0.70 200 | 9.99 160 | 46 | |
| | 15 | 9.29 02 | 1 : | 9.29 866 | 1 | 0.70 134 | 9.99 157 | 45 | Ī |
| | 16 | 9.29 087 | 63 | 9.29 932 | 66 | 0.70 068 | 9.99 155 | 44 | l |
| | 17 | 9.29 150 | 63 64 | 9.29 998 | 66 66 | 0.70 002 | 9.99 152 | 43 | i |
| | 18 | 9.29 214 | 63 | 9.30 064 | 66 | 0.69 936 | 9.99 150 | 42 | ł |
| | 19 | 9.29 277 | 63 | 9.30 130 | 65 | 0.69 870 | 9.99 147 | 41 | I |
| | 20 | 9.29 340 | 1 | 9.30 195 | 1 | 0.69 805 | 9.99 145 | 40 | 1 |
| | 21 | 9.29 403 | 63 63 | 9.30 261 | 66 65 | 0.69 739 | 9.99 142 | 39 | |
| | 22 | 9.29 466 | 63 63 | 9.30 326 | 65 | 0.69 674 | 9.99 140 | 38 | |
| | 23 | 9.29 529 | 62 | 9.30 391 | 66 | 0.69 609 | 9.99 137 | 37 | I |
| | 24 | 9.29 591 | 63 | 9.30 457 | 65 | 0.69 543 | 9.99 135 | 36 | |
| | 25 | 9.29 654 | | 9.30 522 | ٠,- | 0.69 478 | 9.99 132 | 35 | |
| | 26 | 9.29 716 | 62 63 | 9.30 587 | 65 65 | 0.69 413 | 9.99 130 | 34 | |
| | 27 | 9.29 779 | 62 | 9.30 652 | 65 | 0.69 348 | 9.99 127 | 33 | |
| | 28 | 9.29 841 | 62 | 9.30 717 | 65 | 0.69 283 | 9.99 124 | 32 | |
| | 29 | 9.29 903 | 63 | 9.30 782 | 64 | 0.69 218 | 9.99 122 | 31 | |
| | 30 | 9.29 966 | 60 | 9.30 846 | | 0.69 154 | 9.99 119 | 30 | |
| | 31 | 9.30 028 | 62 62 | 9.30 911 | 65 64 | 0.69 089 | 9.99 117 | 29 | |
| | 32 | 9.30 090 | 61 | 9.30 975 | 65 | 0.69 025 | 9.99 114 | 28 | |
| | 33 | 9.30 151 | 62 | 9.31 040 | 64 | 0.68 960 | 9.99 112 | 27 | |
| | 34 | 9.30 213 | 62 | 9.31 104 | 64 | 0.68 896 | 9.99 109 | 26 | |
| | 35 | 9.30 275 | 61 | 9.31 168 | 65 | 0.68 832 | 9.99 106 | 25 | |
| | 36 | 9.30 336 | 62 | 9.31 233 | 64 | 0.68 767 | 9.99 104 | 24 | |
| | 37 | 9.30 398 | 61 | 9.31 297 | 64 | 0.68 703 | 9.99 101 | 23 | |
| | 38 39 | 9.30 459 9.30 521 | 62 | 9.31 361 | 64 | 0.68 639 | 9.99 099 | 22 | |
| | 3,5 | 9.30 521 | 61 | 9.31 425 | 64 | 0.68 575 | 9.99 096 | 21 | |
| | 40 | 9.30 582 | 61 | 9.31 489 | 63 | 0.68 511 | 9.99 093 | 20 | |
| | 41 | 9.30 643 | 61 | 9.31 552 | 64 | 0.68 448 | 9.99 091 | 19 | |
| | 42 | 9.30 704 | 61 | 9.31 616 | 63 | 0.68 384 | 9.99 088 | 18 | |
| | 43 44 | 9.30 765 9.30 826 | 61 | 9.31 679 | 64 | 0.68 321 | 9.99 086 | 17. | |
| | | 9.30 826 | 61 | 9.31 /43 | 63 | 0.68 257 | 9.99 083 | 16 | |
| | 45 | 9.30 887 | 60 | 9.31 806 | 64 | 0.68 194 | 9.99 080 | 15 | |
| | 46 | 9.30 947 | 61 | 9.31 870 | 63 | 0.68 130 | 9.99 078 | 14 | |
| | 47 48 | 9.31 008 9.31 068 | 60 | 9.31 933 | 63 | 0.68 067 | 9.99 075 | 13 | 1 |
| | 49 | 9.31 129 | 61 | 9.31 996 9.32 059 | 63 | 0.68 004 0.67 941 | 9.99 072 9.99 070 | 12 11 | |
| | | | 60 | | 63 | | | | |
| | 50 | 9.31 189 | 61 | 9.32 122 | 63 | 0.67 878 | 9.99 067 | 10 | |
| | 51 52 | 9.31 250 9.31 310 | 60 | 9.32 185 9.32 248 | 63 | 0.67 815 | 9.99 064 9.99 062 | 9 | |
| | 52 53 | 9.31 370 | 60 | 9.32 246 | 63 | 0.67 752 0.67 689 | 9.99 062 | 8 7 | |
| | 54 | 9.31 430 | 60 | 9.32 373 | 62 | 0.67 627 | 9.99 056 | 6 | |
| | \vdash | | 60 | | 63 | | | | |
| | 55 56 | 9.31 490 | 59 | 9.32 436 | 62 | 0.67 564 | 9.99 054 | 5 | |
| | 56 57 | 9.31 549 9.31 609 | 60 | 9.32 498 | 63 | 0.67 502 | 9.99 051 | 4 | |
| | 57 58 | 9.31 669 | 60 | 9.32 561 9.32 623 | 62 | 0.67 439 0.67 377 | 9.99 048 9.99 046 | 3 2 | |
| | 59 | 9.31 728 | 59 | 9.32 623 | 62 | 0.67 377 | 9.99 046 | 1 | l |
| | | | 60 | | 62 | | | | |
| : | 60 | 9.31 788 | | 9.32 747 | | 0.67 253 | 9.99 040 | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | | 348 ⁰ 168 ⁰ |
| | | L COS | | L COT | | L TAN | LSIN | | 258°78° |
| | !! | | l | | | J { | | | |

| 12°192° | T . | | Γ | | | | | | 1 |
|-----------------------------------|-----------|-----------|---------|----------|----------|----------|----------|----------|----------|
| | ļ | L SIN | D | L TAN | CD | LCOT | L COS | | |
| 102 ⁰ 282 ⁰ | | L COS | | L COT | ļ | L TAN | L SIN | | |
| | 0 | 9.31 788 | | 9.32 747 | | 0.67 253 | 9.99 040 | 60 | |
| | 1 | 9.31 847 | 59 | 9.32 810 | 63 | 0.67 190 | 9.99 038 | 59 | |
| | 2 | 9.31 907 | 60 | 9.32 872 | 62 | 0.67 128 | 9.99 035 | 58 | |
| | 3 | 9.31 966 | 59 | 9.32 933 | 61 | 0.67 067 | 9.99 032 | 57 | |
| | 4 | 9.32 025 | 59 | 9.32 995 | 62 | 0.67 005 | 9.99 030 | 56 | |
| | | 3.02.020 | 59 | 9.32 993 | 62 | 0.67 005 | 9.99 030 | 50 | |
| | 5 | 9.32 084 | l | 9.33 057 | | 0.66 943 | 9.99 027 | 55 | |
| | 6 | 9.32 143 | 59 | 9.33 119 | 62 | 0.66 881 | 9.99 024 | 54 | |
| | 7 | 9.32 202 | 59 | 9.33 180 | 61 | 0.66 820 | 9.99 022 | 53 | |
| | 8 | 9.32 261 | 59 | 9.33 242 | 62 | 0.66 758 | 9.99 019 | 52 | |
| | 9 | 9.32 319 | 58 | 9.33 303 | 61 | 0.66 697 | 9.99 016 | 52 51 | |
| | | 0.02 010 | 59 | 5.55 555 | 62 | 0.00 037 | 8.88 010 | 5 | ı |
| | 10 | 9.32 378 | | 9.33 365 | | 0.66 635 | 9.99 013 | 50 | |
| | 11 | 9.32 437 | 59 | 9.33 426 | 61 | 0.66 574 | 9.99 011 | 49 | |
| | 12 | 9.32 495 | 58 | 9.33 487 | 61 | 0.66 513 | 9.99 008 | 48 | |
| | 13 | 9.32 553 | 58 | 9.33 548 | 61 | 0.66 452 | 9.99 005 | 47 | |
| | 14 | 9.32 612 | 59 | 9.33 609 | 61 | 0.66 391 | 9.99 002 | 46 | |
| | | | 58 | | 61 | | | | 1 |
| | 15 | 9.32 670 | 58 | 9.33 670 | 61 | 0.66 330 | 9.99 000 | 45 | |
| | 16 | 9.32 728 | 58 | 9.33 731 | 61 | 0.66 269 | 9.98 997 | 44 | |
| | 17 | 9.32 786 | 58 | 9.33 792 | 61 | 0.66 208 | 9.98 994 | 43 | |
| | 18 | 9.32 844 | | 9.33 853 | | 0.66 147 | 9.98 991 | 42 | |
| | 19 | 9.32 902 | 58 5 | 9.33 913 | 60 | 0.66 087 | 9.98 989 | 41 | |
| | 22 | 0.00.000 | 9 | 0.00.071 | 61 | 0.00.000 | 0.00 | 4- | |
| | 20 | 9.32 960 | 58 | 9.33 974 | 60 | 0.66 026 | 9.98 986 | 40 | I |
| | 21 | 9.33 018 | 57 | 9.34 034 | 61 | 0.65 966 | 9.98 983 | 39 | |
| | 22 | 9.33 075 | 58 | 9.34 095 | 60 | 0.65 905 | 9.98 980 | 38 | ŀ |
| | 23 | 9.33 133 | 57 | 9.34 155 | 60 | 0.65 845 | 9.98 978 | 37 | |
| | 24 | 9.33 190 | 58 | 9.34 215 | 61 | 0.65 785 | 9.98 975 | 36 | |
| | 25 | 9.33 248 | • | 9.34 276 | 1 " | 0.05.704 | 9.98 972 | | |
| | • | | 57 | | 60 | 0.65 724 | | 35 | |
| | 26 | 9.33 305 | 57 | 9.34 336 | 60 | 0.65 664 | 9.98 969 | 34 | |
| | 27 | 9.33 362 | 58 | 9.34 396 | 60 | 0.65 604 | 9.98 967 | 33 | |
| | 28 | 9.33 420 | 57 | 9.34 456 | 60 | 0.65 544 | 9.98 964 | 32 | |
| | 29 | 9.33 477 | 57 | 9.34 516 | 60 | 0.65 484 | 9.98 961 | 31 | |
| | 30 | 9.33 534 | | 9.34 576 | | 0.65 424 | 9.98 958 | 30 | |
| | 31 | 9.33 591 | 57 | 9.34 635 | 59 | 0.65 365 | 9.98 955 | 29 | |
| | 32 | 9.33 647 | 56 | 9.34 695 | 60 | 0.65 305 | 9.98 953 | 28 | |
| | 33 | 9.33 704 | 57 | 9.34 755 | 60 | 0.65 245 | | 27 | |
| | 34 | 9.33 761 | 57 | 9.34 733 | 59 | 0.65 186 | 9.98 950 | 26 | |
| | 37 | 9.33 761 | 57 | 9.34 614 | 60 | 0.05 100 | 9.98 947 | 20 | |
| | 35 | 9.33 818 | | 9.34 874 | | 0.65 126 | 9.98 944 | 25 | |
| | 36 | 9.33 874 | 56 | 9.34 933 | 59 | 0.65 067 | 9.98 941 | 24 | |
| | 37 | 9.33 931 | 57 | 9.34 992 | 59 | 0.65 008 | 9.98 938 | 23 | |
| | 38 | 9.33 987 | 56 | 9.35 051 | 59 | 0.64 949 | 9.98 936 | 22 | |
| | 39 | 9.34 043 | 56 | 9.35 111 | 60 | 0.64 889 | 9.98 933 | 21 | |
| | —— | | 57 | | 59 | | | | |
| | 40 | 9.34 100 | 56 | 9.35 170 | 59 | 0.64 830 | 9.98 930 | 20 | |
| | 41 | 9.34 156 | 56 | 9.35 229 | 59 | 0.64 771 | 9.98 927 | 19 | |
| | 42 | 9.34 212 | 56 | 9.35 288 | 59 59 | 0.64 712 | 9.98 924 | 18 | |
| | 43 | 9.34 268 | 56 | 9.35 347 | 59 58 | 0.64 653 | 9.98 921 | 17 | |
| | 44 | 9.34 324 | 56 | 9.35 405 | 59 | 0.64 595 | 9.98 919 | 16 | |
| | AF | 0.04.000 | - 30 | 0.05 :0: | 59 | 0.04.500 | | | |
| | 45 | 9.34 380 | 56 | 9.35 464 | 59 | 0.64 536 | 9.98 916 | 15 | |
| | 46 | 9.34 436 | 55 | 9.35 523 | 58 | 0.64 477 | 9.98 913 | 14 | |
| | 47 | 9.34 491 | 56 | 9.35 581 | 59 | 0.64 419 | 9.98 910 | 13 | |
| | 48 | 9.34 547 | 55 | 9.35 640 | 58 | 0.64 360 | 9.98 907 | 12 | |
| | 49 | 9.34 602 | 56 | 9.35 698 | 59 | 0.64 302 | 9.98 904 | 11 | |
| | 50 | 9.34 658 | | 9.35 757 | | 0.64 243 | 9.98 901 | 10 | |
| | 51 | 9.34 713 | 55 | 9.35 815 | 58 | 0.64 185 | 9.98 898 | 9 | |
| | 52 | 9.34 769 | 56 | 9.35 873 | 58 | 0.64 183 | 9.98 896 | 8 | |
| | 53 | 9.34 824 | 55 | 9.35 973 | 58 | 0.64 069 | 9.98 893 | 7 | |
| | 54 | 9.34 879 | 55 | 9.35 989 | 58 | 0.64 011 | 9.98 890 | 6 | |
| | | 5.54 57 5 | 55 | 3.55 565 | 58 | 0.04011 | 3.30 030 | Ů | |
| | 55 | 9.34 934 | | 9.36 047 | | 0.63 953 | 9.98 887 | 5 | |
| | 56 | 9.34 989 | 55 | 9.36 105 | 58 | 0.63 895 | 9.98 884 | 4 | |
| | 57 | 9.35 044 | 55 | 9.36 163 | 58 | 0.63 837 | 9.98 881 | 3 | |
| | 58 | 9.35 099 | 55 | 9.36 221 | 58 | 0.63 779 | 9.98 878 | 2 | |
| | 59 | 9.35 154 | 55 | 9.36 279 | 58 | 0.63 773 | 9.98 875 | 1 | |
| | | | 55 | J.30 2/3 | 57 | 0.00 /Z1 | 3.30 0/3 | | |
| | 60 | 9.35 209 | | 9.36 336 | | 0.63 664 | 9.98 872 | 0 | |
| | | L SIN | ٥ | L TAN | CD | L COT | L COS | | 347°167° |
| | | L COS | | L COT | | L TAN | L SIN | | 257° 77° |
| | | | | | [| | _ 0.11 | | 20,, |
| | • | • | | , | , , | , , | j l | | |

| 13°193° | | L SIN | | L TAN | | L COT | L COS | | ì |
|----------|------------|----------------------|----------|--------------|----------|----------|----------|----|-----------------------------------|
| 103°283° | | L COS | ם | L COT | CD | L TAN | LSIN | | |
| | | | | | | | - | | ł |
| | 0 | 9.35 209 9.35 263 | 54 | 9.36 336 | 58 | 0.63 664 | 9.98 872 | 60 | |
| | 1 | | 55 | 9.36 394 | 58 | 0.63 606 | 9.98 869 | 59 | |
| | 2 | 9.35 318 | 55 | 9.36 452 | 57 | 0.63 548 | 9.98 867 | 58 | |
| | 3 | 9.35 373 | 54 | 9.36 509 | 57 | 0.63 491 | 9.98 864 | 57 | 4 |
| | 4 | 9.35 427 | 54 | 9.36 566 | 58 | 0.63 434 | 9.98 861 | 56 | 1 |
| | - | 0.05.404 | ~ | 0.20.004 | 1 ~ | 0.00.070 | 0.00.050 | | 1 |
| | 5 | 9.35 481 | 55 | 9.36 624 | 57 | 0.63 376 | 9.98 858 | 55 | i |
| | 6 | 9.35 536 | 54 | 9.36 681 | 57 | 0.63 319 | 9.98 855 | 54 | i |
| | 7 | 9.35 590 | 54 | 9.36 738 | 57 | 0.63 262 | 9.98 852 | 53 | 4 |
| | 8 | 9.35 644 | 54 | 9.36 795 | 57 | 0.63 205 | 9.98 849 | 52 | i |
| | 9 | 9.35 698 | 54 | 9.36 852 | 57 | 0.63 148 | 9.98 846 | 51 | i |
| | 10 | 9.35 752 | | 9.36 909 | 1 | 0.63 091 | 9.98 843 | 50 | i e |
| | | | 54 | | 57 | | | | i |
| | 11 | 9.35 806 | 54 | 9.36 966 | 57 | 0.63 034 | 9.98 840 | 49 | l . |
| | 12 | 9.35 860 | 54 | 9.37 023 | 57 | 0.62 977 | 9.98 837 | 48 | i e |
| | 13 | 9.35 914 | 54 | 9.37 080 | 57 | 0.62 920 | 9.98 834 | 47 | i |
| | 14 | 9.35 968 | 54 | 9.37 137 | 56 | 0.62 863 | 9.98 831 | 46 | 1 |
| | 15 | 9.36 022 | | 9.37 193 | | 0.62 807 | 9.98 828 | 45 | f |
| | 16 | 9.36 075 | 53 | 9.37 250 | 57 | 0.62 750 | 9.98 825 | 45 | ŧ |
| | 17 | 9.36 129 | 54 | 9.37 306 | 56 | 0.62 750 | 9.98 822 | 43 | i . |
| | | | 53 | | 57 | | | | i |
| | 18 | 9.36 182 | 54 | 9.37 363 | 56 | 0.62 637 | 9.98 819 | 42 | 1 |
| | 19 | 9.36 236 | 53 | 9.37 419 | 57 | 0.62 581 | 9.98 816 | 41 | í |
| | 20 | 9.36 289 | | 9.37 476 | | 0.62 524 | 9.98 813 | 40 | l |
| | 21 | 9.36 342 | 53 | 9.37 532 | 56 | 0.62 468 | 9.98 810 | 39 | 1 |
| | 22 | 9.36 395 | 53 | 9.37 588 | 56 | 0.62 412 | 9.98 807 | 38 | i |
| | 23 | 9.36 449 | 54 | 9.37 644 | 56 | 0.62 412 | 9.98 804 | 37 | 1 |
| | 24 | 9.36 502 | 53 | 9.37 700 | 56 | 0.62 330 | | 36 | 1 |
| | | a.30 302 | 53 | 9.37 700 | 56 | 0.02 300 | 9.98 801 | 30 | Į. |
| | 25 | 9.36 555 | ا ہے ا | 9.37 756 |] | 0.62 244 | 9.98 798 | 35 | 1 |
| | 26 | 9.36 608 | 53 | 9.37 812 | 56 | 0.62 188 | 9.98 795 | 34 | 1 |
| | 27 | 9.36 660 | 52 | 9.37 868 | 56 | 0.62 132 | 9.98 792 | 33 | f |
| | 28 | 9.36 713 | 53 | 9.37 924 | 56 | 0.62 076 | 9.98 789 | 32 | 1 |
| | 29 | 9.36 766 | 53 | 9.37 980 | 56 | 0.62 020 | 9.98 786 | 31 | l |
| | | | 53 | | 55 | | | | 1 |
| | 30 | 9.36 819 | 52 | 9.38 035 | 56 | 0.61 965 | 9.98 783 | 30 | 1 |
| | 31 | 9.36 871 | | 9.38 091 | | 0.61 909 | 9.98 780 | 29 | f |
| | 32 | 9.36 924 | 53 | 9.38 147 | 56 | 0.61 853 | 9.98 777 | 28 | 1 |
| | 33 | 9.36 976 | 52 | 9.38 202 | 55 | 0.61 798 | 9.98 774 | 27 | ł |
| | 34 | 9.37 028 | 52 52 | 9.38 257 | 55 | 0.61 743 | 9.98 771 | 26 | 1 |
| | | | 53 | | 56 | | | | ł |
| | 35 | 9.37 081 | 52 | 9.38 313 | 55 | 0.61 687 | 9.98 768 | 25 | 1 |
| | 36 | 9.37 133 | 52 | 9.38 368 | 55 | 0.61 632 | 9.98 765 | 24 | 1 |
| | 37 | 9.37 185 | 52 52 | 9.38 423 | 56 | 0.61 577 | 9.98 762 | 23 | Í |
| | 38 | 9.37 237 | | 9.38 479 | 1 | 0.61 521 | 9.98 759 | 22 | 1 |
| | 39 | 9.37 289 | 52 52 | 9.38 534 | 55 55 | 0.61 466 | 9.98 756 | 21 | 1 |
| | | 0.03.044 | 52 | | 55 | | | | 4 |
| | 40 | 9.37 341 | 52 | 9.38 589 | 55 | 0.61 411 | 9.98 753 | 20 | 1 |
| | 41 | 9.37 393 | 52 | 9.38 644 | 55 | 0.61 356 | 9.98 750 | 19 | 1 |
| | 42 | 9.37 445 | 52 | 9.38 699 | 55 | 0.61 301 | 9.98 746 | 18 | i |
| | 43 | 9.37 497 | 52 | 9.38 754 | 54 | 0.61 246 | 9.98 743 | 17 | 1 |
| | 44 | 9.37 549 | 51 | 9.38 808 | 55 | 0.61 192 | 9.98 740 | 16 | 1 |
| | 45 | 9 37 600 | [] | 0.36.063 | 1 ~~ | 0.61.127 | 9.98 737 | 15 | 1 |
| | | 9.37 600 9.37 652 | 52 | 9.38 863 | 55 | 0.61 137 | | 15 | ı |
| | 46 | | 51 | 9.38 918 | 54 | 0.61 082 | 9.98 734 | 14 | 1 |
| | 47 | 9.37 703 | 52 | 9.38 972 | 55 | 0.61 028 | 9.98 731 | 13 | 1 |
| | 48 | 9.37 755 | 51 | 9.39 027 | 55 | 0.60 973 | 9.98 728 | 12 | 4 |
| | 49 | 9.37 806 | 52 | 9.39 082 | 54 | 0.60 918 | 9.98 725 | 11 | 1 |
| | 50 | 9.37 858 | | 9.39 136 | 1 | 0.60 864 | 9.98 722 | 10 | 1 |
| | 51 | 9.37 909 | 51 | 9.39 190 | 54 | | 9.98 719 | | 1 |
| | 52 | | 51 | | 55 | 0.60 810 | | 9 | 1 |
| | | 9.37 960 | 51 | 9.39 245 | 54 | 0.60 755 | 9.98 715 | 8 | į. |
| | 53 54 | 9.38 011 | 51 | 9.39 299 | 54 | 0.60 701 | 9.98 712 | 7 | 1 |
| | 54 | 9.38 062 | 51 | 9.39 353 | 54 | 0.60 647 | 9.98 709 | 6 | 1 |
| | 5 5 | 9.38 113 | | 9.39 407 | 1 | 0.60 593 | 9.98 706 | 5 | Í |
| | 56 | 9.38 164 | 51 | 9.39 461 | 54 | 0.60 539 | 9.98 703 | 4 | i |
| | 56 57 | 9.38 215 | 51 | | 54 | | | | t . |
| | 57 58 | | 51 | 9.39 515 | 54 | 0.60 485 | 9.98 700 | 3 | 1 |
| | | 9.38 266 | 51 | 9.39 569 | 54 | 0.60 431 | 9.98 697 | 2 | 1 |
| | 59 | 9.38 317 | 51 | 9.39 623 | 54 | 0.60 377 | 9.98 694 | 1 | i |
| | 60 | 9.38 368 | | 9.39 677 | <u> </u> | 0.60 323 | 9.98 690 | 0 | <u> </u> |
| | | L SIN | D | L TAN | CD | L COT | L COS | | 346 ⁰ 166 ⁰ |
| | | 1.000 | ا د ا | | | | | | |
| | | L COS | | L COT | | L TAN | L SIN | | 256°76° |
| | | 1 | 1 | | ľ. | | | | 4 |

| 14 ⁰ 194 ⁰ | | L SIN | | L TAN | CD | L COT | LCOS | D | | |
|-----------------------------------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|------------|----------|----------|
| 104 ⁰ 284 ⁰ | | L COS | D | L COT | CD | L TAN | L SIN | | | |
| | | 9.38 368 | | 9.39 677 | | 0.60 323 | 9.98 690 | | 60 | |
| | 0 | 9.38 418 | 50 | 9.39 731 | 54 | 0.60 269 | 9.98 687 | 3 | 59 | |
| | 2 | 9.38 469 | 51 | 9.39 785 | 54 | 0.60 215 | 9.98 684 | 3 | 58 | |
| | 3 | 9.38 519 | 50 | 9.39 838 | 53 | 0.60 162 | 9.98 681 | 3 | 57 | |
| | 4 | 9.38 570 | 51 | 9.39 892 | 54 | 0.60 102 | 9.98 678 | 3 | 56 | |
| | <u> </u> | 9.30 370 | 50 | 3.03 032 | 53 | | | 3 | -1 | |
| | 5 | 9.38 620 | 50 | 9.39 945 | 54 | 0.60 055 | 9.98 675 | 4 | 55 | |
| | 6 | 9.38 670 | 51 | 9.39 999 | 53 | 0.60 001 | 9.98 671 | 3 | 54 | |
| | 7 | 9.38 721 | 50 | 9.40 052 | 54 | 0.59 948 | 9.98 668 | 3 | 53 | |
| | 8 | 9.38 771 | 50 | 9.40 106 | 53 | 0.59 894 | 9.98 665 | 3 | 52 | |
| | 9 | 9.38 821 | 50 | 9.40 159 | 53 | 0.59 841 | 9.98 662 | 3 | 51 | |
| | 10 | 9.38 871 | | 9.40 212 | | 0.59 788 | 9.98 659 | | 50 | |
| | 11 | 9.38 921 | 50 | 9.40 206 | 54 | 0.59 734 | 9.98 656 | 3 | 49 | |
| | 12 | 9.38 971 | 50 | 9.40 319 | 53 | 0.59 681 | 9.98 652 | 3 | 48 | |
| | 13 | 9.39 021 | 50 | 9.40 372 | 53 53 | 0.59 628 | 9.98 649 | 3 | 47 | |
| | 14 | 9.39 071 | 50 50 | 9.40 425 | 53 | 0.59 575 | 9.98 646 | 3 | 46 | |
| | | 0.00.101 | 50 | 0.40.470 | - 3 | 0.50.500 | 9.98 643 | ١ | 45 | |
| | 15 | 9.39 121 9.39 170 | 49 | 9.40 478 9.40 531 | 53 | 0.59 522 0.59 469 | 9.98 643 9.98 640 | 3 | 45 | |
| | 16 17 | 9.39 170 | 50 | 9.40 584 | 53 | 0.59 416 | 9.98 636 | 4 | 43 | |
| | 18 | 9.39 220 | 50 | 9.40 584 | 52 | 0.59 364 | 9.98 633 | 3 | 42 | |
| | 19 | 9.39 319 | 49 | 9.40 689 | 53 | 0.59 311 | 9.98 630 | 3 | 41 | |
| | <u> </u> | | 50 | | 53 | | | 3 | | |
| | 20 | 9.39 369 | 49 | 9.40 742 | 53 | 0.59 258 | 9.98 627 | 4 | 40 | |
| | 21 | 9.39 418 | 49 | 9.40 795 | 52 | 0.59 205 | 9.98 623 | 3 | 39 | |
| | 22 | 9.39 467 | 50 | 9.40 847 | 53 | 0.59 153 | 9.98 620 | 3 | 38 37 | |
| | 23 | 9.39 517 | 49 | 9.40 900 | 52 | 0.59 100 | 9.98 617 | 3 | 37 36 | |
| | 24 | 9.39 566 | 49 | 9.40 952 | 53 | 0.59 048 | 9.98 614 | 4 | 36 | |
| | 25 | 9.39 615 | | 9.41 005 | ا م | 0.58 995 | 9.98 610 | , | 35 | |
| | 26 | 9.39 664 | 49 | 9.41 057 | 52 52 | 0.58 943 | 9.98 607 | 3 | 34 | |
| | 27 | 9.39 713 | 49 40 | 9.41 109 | 52 52 | 0.58 891 | 9.98 604 | 3 | 33 | |
| | 28 | 9.39 762 | 49 49 | 9.41 161 | 52 53 | 0.58 839 | 9.98 601 | 4 | 32 | |
| | 29 | 9.39 811 | 49 49 | 9.41 214 | 53 52 | 0.58 876 | 9.98 597 | 3 | 31 | |
| | 30 | 9.39 860 | | 9.41 266 | 1 | 0.58 734 | 9.98 594 | | 30 | |
| | 30 31 | 9.39 860 | 49 | 9.41 266 | 52 | 0.58 734 | 9.98 594 | 3 | 29 | |
| | 31 | 9.39 909 | 49 | 9.41 370 | 52 | 0.58 630 | 9.98 588 | 3 | 28 | |
| | 33 | 9.40 006 | 48 | 9.41 422 | 52 | 0.58 578 | 9.98 584 | 4 | 27 | |
| | 34 | 9.40 055 | 49 | 9.41 474 | 52 | 0.58 526 | 9.98 581 | 3 | 26 | |
| | | | 48 | | 52 | | | 3 | | |
| | 35 | 9.40 103 | 49 | 9.41 526 | 52 | 0.58 474 | 9.98 578 | 4 | 25 | |
| | 36 | 9.40 152 | 48 | 9.41 578 | 51 | 0.58 422 | 9.98 574 | 3 | 24 | |
| | 37 | 9.40 200 | 49 | 9.41 629 | 52 | 0.58 371 | 9.98 571 | 3 | 23 | |
| | 38 | 9.40 249 | 48 | 9.41 681 | 52 | 0.58 319 | 9.98 568 | 3 | 22 21 | |
| | 39 | 9.40 297 | 49 | 9.41 733 | 51 | 0.58 267 | 9.98 565 | 4 | - 1 | |
| | 40 | 9.40 346 | 48 | 9.41 784 | 52 | 0.58 216 | 9.98 561 | 3 | 20 | |
| | 41 | 9.40 394 | 48 48 | 9.41 836 | 52 51 | 0.58 164 | 9.98 558 | 3 | 19 | |
| | 42 | 9.40 442 | 48 | 9.41 887 | 52 | 0.58 113 | 9.98 555 | 4 | 18 | |
| | 43 | 9.40 490 | 48 | 9.41 939 | 51 | 0.58 061 | 9.98 551 | 3 | 17 | |
| | 44 | 9.40 538 | 48 | 9.41 990 | 51 | 0.58 010 | 9.98 548 | 3 | 16 | |
| | 45 | 9.40 586 | 1 | 9.42 041 | 1 | 0.57 959 | 9.98 545 | . | 15 | |
| | 46 | 9.40 634 | 48 | 9.42 093 | 52 51 | 0.57 907 | 9.98 541 | 4 3 | 14 | |
| | 47 | 9.40 682 | 48 | 9.42 144 | 51 51 | 0.57 856 | 9.98 538 | 3 | 13 | |
| | 48 | 9.40 730 | 48 48 | 9.42 195 | 51 51 | 0.57 805 | 9.98 535 | 4 | 12 | |
| | 49 | 9.40 778 | 48 47 | 9.42 246 | 51 51 | 0.57 754 | 9.98 531 | 3 | 11 | |
| | 50 | 9.40 825 | 1 ~ | 9.42 297 | 1 ~ | 0.57 703 | 9.98 528 | | 10 | l |
| | 50 51 | 9.40 825 | 48 | 9.42 297 | 51 | 0.57 652 | 9.98 525 | 3 | 9 | |
| | 52 | 9.40 873 | 48 | 9.42 346 | 51 | 0.57 601 | 9.98 521 | 4 | 8 | |
| | 52 53 | 9.40 921 | 47 | 9.42 399 | 51 | 0.57 550 | 9.98 518 | 3 | 7 | |
| | 53 54 | 9.41 016 | 48 | 9.42 501 | 51 | 0.57 499 | 9.98 515 | 3 | 6 | |
| | | | 47 | | 51 | | | ∤ ⁴ | \vdash | |
| | 55 | 9.41 063 | 48 | 9.42 552 | 51 | 0.57 448 | 9.98 511 | 3 | 5 | |
| | 56 | 9.41 111 | 47 | 9.42 603 | 50 | 0.57 397 | 9.98 508 | 3 | 4 | |
| | 57 | 9.41 158 | 47 | 9.42 653 | 51 | 0.57 347 | 9.98 505 | 4 | 3 | |
| | 58 | 9.41 205 | 47 | 9.42 704 | 51 | 0.57 296 | 9.98 501 | 3 | 2 | |
| | 59 | 9.41 252 | 48 | 9.42 755 | 50 | 0.57 245 | 9.98 498 | 4 | 1 | |
| | 60 | 9.41 300 | | 9.42 805 | | 0.57 195 | 9.98 494 | | 0 | |
| | | L SIN | | L TAN | CC | L COT | L COS | D | | 345°165° |
| | | L COS | D | L COT | CD | L TAN | L SIN | 1 | | 255° 75° |
| | 1 | i | l | I | I | I | 1 | | | J |

| 15°195° | 1 | L SIN | D | L TAN | CD | LCOT | LCOS | D | |
|----------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|-----|----------|
| 105°285° | | L COS | | L COT | CD | L TAN | L SIN | | |
| | 0 | 9.41 300 | | 9.42 805 | | 0.57 195 | 9.98 494 | | 60 |
| | Ĭ | 9.41 347 | 47 | 9.42 856 | 51 | 0.57 144 | 9.98 491 | 3 | 59 |
| | 2 | 9.41 394 | 47 | 9.42 906 | 50 | 0.57 094 | 9.98 488 | 3 | 58 |
| | 3 | 9.41 441 | 47 | 9.42 957 | 51 | 0.57 043 | 9.98 484 | 4 | 57 |
| | 4 | 9.41 488 | 47 47 | 9.43 007 | 50 50 | 0.56 993 | 9.98 481 | 3 4 | 56 |
| | 5 | 9.41 535 | | 9.43 057 | 1 | 0.56 943 | 9.98 477 | | 55 |
| | 6 | 9.41 582 | 47 46 | 9.43 108 | 51 | 0.56 892 | 9.98 474 | 3 | 54 |
| | 7 | 9.41 628 | 46 47 | 9.43 158 | 50 50 | 0.56 842 | 9.98 471 | 3 | 53 |
| | 8 | 9.41 675 | 47 | 9.43 208 | 50 | 0.56 792 | 9.98 467 | 3 | 52 |
| | 9 | 9.41 722 | 46 | 9.43 258 | 50 | 0.56 742 | 9.98 464 | 4 | 51 |
| | 10 | 9.41 768 | 47 | 9.43 308 | 50 | 0.56 692 | 9.98 460 | 3 | 50 |
| | 11 | 9.41 815 | 46 | 9.43 358 | 50 | 0.56 642 | 9.98 457 | 4 | 49 |
| | 12 | 9.41 861 | 47 | 9.43 408 | 50 | 0.56 592 | 9.98 453 | 3 | 48 |
| | 13 | 9.41 908 | 46 | 9.43 458 | 50 | 0.56 542 | 9.98 450 | 3 | 47 |
| | 14 | 9.41 954 | 47 | 9.43 508 | 50 | 0.56 492 | 9.98 447 | 4 | 46 |
| | 15 | 9.42 001 | 46 | 9.43 558 | 49 | 0.56 442 | 9.98 443 | 3 | 45 |
| | 16 | 9.42 047 | 46 | 9.43 607 | 50 | 0.56 393 | 9.98 440 | 4 | 44 |
| | 17 | 9.42 093 | 47 | 9.43 657 | 50 | 0.56 343 | 9.98 436 | 3 | 43 |
| | 18 | 9.42 140 | 46 | 9.43 707 | 49 | 0.56 293 | 9.98 433 | 4 | 42 |
| | 19 | 9.42 186 | 46 | 9.43 756 | 50 | 0.56 244 | 9.98 429 | 3 | 41 |
| | 20 | 9.42 232 | 46 | 9.43 806 | 49 | 0.56 194 | 9.98 426 | 4 | 40 |
| | 21 | 9.42 278 | 46 | 9.43 855 | 50 | 0.56 145 | 9.98 422 | 3 | 39 |
| | 22 23 | 9.42 324 9.42 370 | 46 | 9.43 905 9.43 954 | 49 | 0.56 095 | 9.98 419 | 4 | 38 37 |
| | 23 | 9.42 370 9.42 416 | 46 | 9.43 954 9.44 004 | 50 | 0.56 046 0.55 996 | 9.98 415 9.98 412 | 3 | 36 |
| | | | 45 | | 49 | | | 3 | Ь— |
| | 25 26 | 9.42 461 9.42 507 | 46 | 9.44 053 9.44 102 | 49 | 0.55 947 | 9.98 409 | 4 | 35 |
| | 27 | 9.42 507 | 46 | 9.44 102 | 49 | 0.55 898 0.55 849 | 9.98 405 9.98 402 | 3 | 34 33 |
| | 28 | 9.42 599 | 46 | 9.44 201 | 50 | 0.55 799 | 9.98 398 | 4 | 32 |
| | 29 | 9.42 644 | 45 46 | 9.44 250 | 49 49 | 0.55 750 | 9.98 395 | 3 | 31 |
| | 30 | 9.42 690 | | 9,44 299 | 1 | 0.55 701 | 9.98 391 | 1 | 30 |
| | 31 | 9.42 735 | 45 | 9.44 348 | 49 | 0.55 652 | 9.98 388 | 3 | 29 |
| | 32 | 9.42 781 | 46 | 9.44 397 | 49 | 0.55 603 | 9.98 384 | 4 | 28 |
| | 33 | 9.42 826 | 45 46 | 9.44 446 | 49 49 | 0.55 554 | 9.98 381 | 3 4 | 27 |
| | 34 | 9.42 872 | 45 | 9.44 495 | 49 | 0.55 505 | 9.98 377 | 4 | 26 |
| | 35 | 9.42 917 | 45 | 9.44 544 | 48 | 0.55 456 | 9.98 373 | 3 | 25 |
| | 36 | 9.42 962 | 46 | 9.44 592 | 49 | 0.55 408 | 9.98 370 | 4 | 24 |
| | 37 | 9.43 008 | 45 | 9.44 641 | 49 | 0.55 359 | 9.98 366 | 3 | 23 |
| | 38 39 | 9.43 053 9.43 098 | 45 | 9.44 690 9.44 738 | 48 | 0.55 310 0.55 262 | 9.98 363 9.98 359 | 4 | 22 21 |
| | | | 45 | | 49 | | | 3 | |
| | 40 | 9.43 143 | 45 | 9.44 787 | 49 | 0.55 213 | 9.98 356 | 4 | 20 |
| | 41 42 | 9.43 188 9.43 233 | 45 | 9.44 836 9.44 884 | 48 | 0.55 164 0.55 116 | 9.98 352 9.98 349 | 3 | 19 18 |
| | 43 | 9.43 278 | 45 | 9.44 933 | 49 | 0.55 116 | 9.98 349 9.98 345 | 4 | 17 |
| | 44 | 9.43 323 | 45 44 | 9.44 981 | 48 48 | 0.55 019 | 9.98 342 | 3 4 | 16 |
| | 45 | 9.43 367 | | 9.45 029 | 1 | 0.54 971 | 9.98 338 | 1 ' | 15 |
| | 46 | 9.43 412 | 45 | 9.45 078 | 49 | 0.54 971 | 9.98 334 | 4 | 14 |
| | 47 | 9.43 457 | 45 45 | 9.45 126 | 48 | 0.54 874 | 9.98 331 | 3 | 13 |
| | 48 | 9.43 502 | 45 44 | 9.45 174 | 48 48 | 0.54 826 | 9.98 327 | 3 | 12 |
| | 49 | 9.43 546 | 45 | 9.45 222 | 49 | 0.54 778 | 9.98 324 | 4 | - 11 |
| | 50 | 9.43 591 | } | 9.45 271 | 1 | 0.54 729 | 9.98 320 | 1 . | 10 |
| | 51 | 9.43 635 | 44 45 | 9.45 319 | 48 | 0.54 681 | 9.98 317 | 3 | 9 |
| | 52 | 9.43 680 | 45 44 | 9.45 367 | 48 48 | 0.54 633 | 9.98 313 | 4 | 8 |
| | 53 | 9.43 724 | 45 | 9.45 415 | 48 | 0.54 585 | 9.98 309 | 3 | 7 |
| | 54 | 9.43 769 | 44 | 9.45 463 | 48 | 0.54 537 | 9.98 306 | 4 | 6 |
| | 55 | 9.43 813 | 44 | 9.45 511 | 48 | 0.54 489 | 9.98 302 | 3 | 5 |
| | 56 | 9.43 857 | 44 | 9.45 559 | 47 | 0.54 441 | 9.98 299 | 4 | 4 |
| | 57 59 | 9.43 901 | 45 | 9.45 606 | 48 | 0.54 394 | 9.98 295 | 4 | 3 |
| | 58 59 | 9.43 946 9.43 990 | 44 | 9.45 654 9.45 702 | 48 | 0.54 346 0.54 298 | 9.98 291 9.98 288 | 3 | 2 1 |
| | \vdash | | 44 | | 48 | | | 4 | |
| | 60 | 9.44 034 | | 9.45 750 | <u> </u> | 0.54 250 | 9.98 284 | | ٥ |
| | | L SIN | D | L TAN | CD | L COT | LCOS | D | |
| | | LCOS | | L COT | \ | L TAN | L SIN | | |
| | I I | J i | j l | | j | ! |] | | |

| 16°196° | | L SIN | D | L TAN | CD | L COT | L COS | D | | |
|----------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|--------|----------|----------|
| 106°286° | | L COS | | L COT | | L TAN | L SIN | | | |
| | 0 | 9.44 034 | | 9.45 750 | | 0.54 250 | 9.98 284 | | 60 | |
| | 1 | 9.44 078 | 44 | 9.45 797 | 47 | 0.54 203 | 9.98 281 | 3 | 59 | |
| | 2 | 9.44 122 | 44 | 9.45 845 | 48 | 0.54 155 | 9.98 277 | 4 | 58 | |
| | 3 | 9.44 166 | 44 | 9.45 892 | 47 | 0.54 108 | 9.98 273 | 3 | 57 | |
| | 4 | 9.44 210 | 44 43 | 9.45 940 | 48 47 | 0.54 060 | 9.98 270 | 4 | 56 | |
| | 5 | 9.44 253 | 40 | 9.45 987 | ٠, | 0.54 013 | 9.98 266 | | 55 | |
| | 6 | 9.44 297 | 44 | 9.46 035 | 48 | 0.53 965 | 9.98 262 | 4 | 54 | |
| | 7 | 9.44 341 | 44 | 9.46 082 | 47 | 0.53 918 | 9.98 259 | 3 | 53 | |
| | 8 | 9.44 385 | 44 | 9.46 130 | 48 47 | 0.53 870 | 9.98 255 | 4 | 52 | |
| | 9 | 9.44 428 | 43 44 | 9.46 177 | 47 | 0.53 823 | 9.98 251 | 3 | 51 | |
| | 10 | 9.44 472 | | 9.46 224 | | 0.53 776 | 9.98 248 | | 50 | |
| | 11 | 9.44 516 | 44 | 9.46 271 | 47 | 0.53 729 | 9.98 244 | 4 | 49 | |
| | 12 | 9.44 559 | 43 | 9.46 319 | 48 | 0.53 681 | 9.98 240 | 4 3 | 48 | |
| | 13 | 9.44 602 | 43 44 | 9.46 366 | 47 47 | 0.53 634 | 9.98 237 | 4 | 47 | |
| | 14 | 9.44 646 | 43 | 9.46 413 | 47 | 0.53 587 | 9.98 233 | 4 | 46 | |
| | 15 | 9.44 689 | | 9.46 460 | | 0.53 540 | 9.98 229 | | 45 | |
| | 16 | 9.44 733 | 44 | 9.46 507 | 47 | 0.53 493 | 9.98 226 | 3 4 | 44 | |
| | 17 | 9.44 776 | 43 43 | 9.46 554 | 47 47 | 0.53 446 | 9.98 222 | 4 | 43 | |
| | 18 | 9.44 819 | 43 | 9.46 601 | 47 | 0.53 399 | 9.98 218 | 3 | 42 | |
| | 19 | 9.44 862 | 43 | 9.46 648 | 46 | 0.53 352 | 9.98 215 | 4 | 41 | |
| | 20 | 9.44 905 | 40 | 9.46 694 | 47 | 0.53 306 | 9.98 211 | 4 | 40 | |
| | 21 | 9.44 948 | 43 44 | 9.46 711 | 47 | 0.53 259 | 9.98 207 | 3 | 39 | |
| | 22 | 9.44 992 | 43 | 9.46 788 | 47 | 0.53 212 | 9.98 204 | 4 | 38 | |
| | 23 | 9.45 035 | 42 | 9.46 835 | 46 | 0.53 165 | 9.98 200 9.98 196 | 4 | 37 36 | |
| | 24 | 9.45 077 | 43 | 9.46 861 | 47 | 0.53 119 | 9.90 190 | 4 | -30 | |
| | 25 | 9.45 120 | 43 | 9.46 928 | 47 | 0.53 072 | 9.98 192 | 3 | 35 | |
| | 26 | 9.45 163 | 43 | 9.46 975 | 46 | 0.53 025 | 9.98 189 | 4 | 34 | |
| | 27 | 9.45 206 | 43 | 9.47 021 | 47 | 0.52 979 | 9.98 185 | 4 | 33 | |
| | 28 20 | 9.45 249 | 43 | 9.47 068 9.47 114 | 46 | 0.52 932 0.52 886 | 9.98 181 9.98 177 | 4 | 32 31 | |
| | 29 | 9.45 292 | 42 | 9.47 114 | 46 | 0.52 000 | 9.90 177 | 3 | 31 | |
| | 30 | 9.45 334 | 43 | 9.47 160 | 47 | 0.52 840 | 9.98 174 | 4 | 30 | |
| | 31 | 9.45 377 | 42 | 9.47 207 | 46 | 0.52 793 | 9.98 170 | 4 | 29 | ! |
| | 32 | 9.45 419 | 43 | 9.47 253 | 46 | 0.52 747 | 9.98 166 | 4 | 28 27 | |
| | 33 34 | 9.45 462 9.45 504 | 42 | 9.47 299 9.47 346 | 47 | 0.52 701 0.52 654 | 9.98 162 9.98 159 | 3 | 26 | |
| | | | 43 | | 46 | | | 4 | 25 | |
| | 35 36 | 9.45 547 9.45 589 | 42 | 9.47 392 9.47 438 | 46 | 0.52 608 0.52 562 | 9.98 155 9.98 151 | 4 | 25 | |
| | 37 | 9.45 632 | 43 | 9.47 484 | 46 | 0.52 516 | 9.98 147 | 4 | 23 | |
| | 38 | 9.45 674 | 42 | 9.47 530 | 46 | 0.52 470 | 9.98 144 | 3 | 22 | |
| | 39 | 9.45 716 | 42 42 | 9.47 576 | 46 46 | 0.52 424 | 9.98 140 | 4 | 21 | |
| | 40 | 9.45 758 | 42 | 9.47 622 | 1 ~ | 0.52 378 | 9.98 136 | | 20 | |
| | 41 | 9.45 801 | 43 | 9.47 668 | 46 | 0.52 332 | 9.98 132 | 4 | 19 | |
| | 42 | 9.45 843 | 42 | 9.47 714 | 46 | 0.52 286 | 9.98 129 | 3 4 | 18 | |
| | 43 | 9.45 885 | 42 42 | 9.47 760 | 46 46 | 0.52 240 | 9.98 125 | 4 | 17 | |
| | 44 | 9.45 927 | 42 | 9.47 806 | 46 | 0.52 194 | 9.98 121 | 4 | 16 | |
| | 45 | 9.45 969 | | 9.47 852 | | 0.52 148 | 9.98 117 | 4 | 15 | |
| | 46 | 9.46 011 | 42 42 | 9.47 897 | 45 46 | 0.52 103 | 9.98 113 | 3 | 14 | |
| | 47 | 9.46 053 | 42 | 9.47 943 | 46 | 0.52 057 | 9.98 110 | 4 | 13 | |
| | 48 49 | 9.46 095 9.46 136 | 41 | 9.47 989 9.48 035 | 46 | 0.52 011 0.51 965 | 9.98 106 9.98 102 | 4 | 12 11 | |
| | | | 42 | | 45 | | | 4 | | |
| | 50 | 9.46 178 | 42 | 9.48 080 | 46 | 0.51 920 | 9.98 098 | 4 | 10 | |
| | 51 | 9.46 220 | 42 | 9.48 126 | 45 | 0.51 874 0.51 829 | 9.98 094 | 4 | 9 8 | |
| | 52 53 | 9.46 262 9.46 303 | 41 | 9.48 171 9.48 217 | 46 | 0.51 783 | 9.98 090 9.98 087 | 3 | 7 | |
| | 54 | 9.46 345 | 42 | 9.48 262 | 45 | 0.51 738 | 9.98 083 | 4 | 6 | |
| | | | 41 | | 45 | | | 4 | | |
| | 55 56 | 9.46 386 9.46 428 | 42 | 9.48 307 9.48 353 | 46 | 0.51 693 0.51 647 | 9.98 079 9.98 075 | 4 | 5 4 | |
| | 56 57 | 9.46 428 9.46 469 | 41 | 9.48 353 | 45 | 0.51 647 | 9.98 075 | 4 | 3 | |
| | 58 | 9.46 511 | 42 | 9.48 443 | 45 | 0.51 557 | 9.98 067 | 4 | 2 | |
| | 59 | 9.46 552 | 41 | 9.48 489 | 46 | 0.51 511 | 9.98 063 | 4 | 1 | |
| | 60 | 9.46 594 | 42 | 9.48 534 | 45 | 0.51 466 | 9.98 060 | 3 | 0 | |
| | | L SIN | | L TAN | | L COT | L COS | | Ť | 343°163° |
| | | | D | | CD | | | D | | |
| | | L COS | | L COT | | L TAN | L SIN | | | 253° 73° |

| 17 ⁰ 197 ⁰ | | | | | T | | | | | 1 |
|----------------------------------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|----------|----------|-----------------------------------|
| | | L SIN | D | L TAN | , CD | L COT | L COS | | | ļ |
| 107°287° | | L COS | | L COT | - 00 | L TAN | L SIN | <u> </u> | | |
| | 0 | 9.46 594 | | 9.48 534 | | 0.51 466 | 9.98 060 | | 60 | |
| | Ĭ | 9.46 635 | 41 | 9.48 579 | 45 | 0.51 421 | 9.98 056 | 4 | 59 | į. |
| | 2 | 9.46 676 | 41 | 9.48 624 | 45 | 0.51 376 | 9.98 052 | 4 | 58 | i |
| | 3 | 9.46 717 | 41 | 9.48 669 | 45 | 0.51 331 | 9.98 048 | 4 | 57 | 1 |
| | 4 | 9.46 758 | 41 | 9.48 714 | 45 | 0.51 286 | 9.98 044 | 4 | 56 | i |
| | 5 | 9.46 800 | 42 | 9.48 759 | 45 | 0.51 241 | 0.00.040 | 4 | | 1 |
| | 6 | 9.46 841 | 41 | 9.48 804 | 45 | 0.51 241 | 9.98 040 9.98 036 | 4 | 55 54 | 1 |
| | 7 | 9.46 882 | 41 | 9.48 849 | 45 | 0.51 151 | 9.98 032 | 4 | 53 | 1 |
| | 8 | 9.46 923 | 41 | 9.48 894 | 45 | 0.51 106 | 9.98 029 | 3 | 52 | 1 |
| | 9 | 9.46 964 | 41 | 9.48 939 | 45 | 0.51 061 | 9.98 025 | 4 | 51 | 1 |
| | 10 | 9.47 005 | 41 | 9.48 984 | 45 | 0.51.010 | | 4 | | 1 |
| | 11 | 9.47 045 | 40 | 9.49 029 | 45 | 0.51 016 0.50 971 | 9.98 021 9.98 017 | 4 | 50 | i |
| | 12 | 9.47 086 | 41 | 9.49 073 | 44 | 0.50 971 | 9.98 013 | 4 | 49 48 | i |
| | 13 | 9.47 127 | 41 | 9.49 118 | 45 | 0.50 882 | 9.98 009 | 4 | 47 | ĺ |
| | 14 | 9.47 168 | 41 | 9.49 163 | 45 | 0.50 837 | 9.98 005 | 4 | 46 | 1 |
| | 1,5 | | 41 | | 44 | | | 4 | | i |
| | 15 16 | 9.47 209 | 40 | 9.49 207 | 45 | 0.50 793 | 9.98 001 | 4 | 45 | i |
| | 16 | 9.47 249 9.47 290 | 41 | 9.49 252 9.49 296 | 44 | 0.50 748 0.50 704 | 9.97 997 | 4 | 44 | i |
| | 17 | 9.47 290 | 40 | 9.49 296 9.49 341 | 45 | 0.50 704 0.50 659 | 9.97 993 9.97 989 | 4 | 43 | i |
| | 19 | 9.47 371 | 41 | 9.49 385 | 44 | 0.50 659 | 9.97 986 | 3 | 42 41 | 1 |
| | - | | 40 | | 45 | | | 4 | | 1 |
| | 20 | 9.47 411 | 41 | 9.49 430 | 44 | 0.50 570 | 9.97 982 | 4 | 40 | 1 |
| | 21 | 9.47 452 | 40 | 9.49 474 | 45 | 0.50 526 | 9.97 978 | 4 | 39 | 1 |
| | 22 23 | 9.47 492 9.47 533 | 41 | 9.49 519 9.49 563 | 44 | 0.50 481 | 9.97 974 | 4 | 38 | i |
| | 24 | 9.47 573 | 40 | 9.49 607 | 44 | 0.50 437 0.50 393 | 9.97 970 9.97 966 | 4 | 37 36 | i |
| | | | 40 | 3.43 007 | 45 | 0.50 555 | 3.37 300 | 4 | 30 | j |
| | 25 | 9.47 613 | 41 | 9.49 652 | 44 | 0.50 348 | 9.97 962 | 4 | 35 | İ |
| | 26 | 9.47 654 | 40 | 9.49 696 | 44 | 0.50 304 | 9.97 958 | 4 | 34 | i |
| | 27 | 9.47 694 | 40 | 9.49 740 | 44 | 0.50 260 | 9.97 954 | 4 | 33 | i |
| | 28 29 | 9.47 734 | 40 | 9.49 784 | 44 | 0.50 216 | 9.97 950 | 4 | 32 | i |
| | -29 | 9.47 774 | 40 | 9.49 828 | 44 | 0.50 172 | 9.97 946 | 4 | 31 | i |
| | 30 | 9.47 814 | 40 | 9.49 872 | 44 | 0.50 128 | 9.97 942 | | 30 | i |
| | 31 | 9.47 854 | 40 | 9.49 916 | 44 44 | 0.50 084 | 9.97 938 | 4 | 29 | i |
| | 32 | 9.47 894 | 40 | 9.49 960 | 44 | 0.50 040 | 9.97 934 | 4 | 28 | i |
| | 33 | 9.47 934 | 40 | 9.50 004 | 44 | 0.49 996 | 9.97 930 | 4 | 27 | i |
| | 34 | 9.47 974 | 40 | 9.50 048 | 44 | 0.49 952 | 9.97 926 | 4 | 26 | i |
| | 35 | 9.48 014 | 40 | 9.50 092 | 44 | 0.49 908 | 9.97 922 | | 25 | i |
| | 36 | 9.48 054 | 40 40 | 9.50 136 | 44 44 | 0.49 864 | 9.97 918 | 4 | 24 | i |
| | 37 | 9.48 094 | 39 | 9.50 180 | 43 | 0.49 820 | 9.97 914 | 4 | 23 | i |
| | 38 | 9.48 133 | 40 | 9.50 223 | 44 | 0.49 777 | 9.97 910 | 4 | 22 | i |
| | 39 | 9.48 173 | 40 | 9.50 267 | 44 | 0.49 733 | 9.97 906 | 4 | 21 | i |
| | 40 | 9.48 213 | | 9.50 311 | | 0.49 689 | 9.97 902 | | 20 | İ |
| | 41 | 9.48 252 | 39 | 9.50 355 | 44 | 0.49 645 | 9.97 898 | 4 | 19 | 1 |
| | 42 | 9.48 292 | 40 40 | 9.50 398 | 43 | 0.49 602 | 9.97 894 | 4 | 18 | 1 |
| | 43 | 9.48 332 | 39 | 9.50 442 | 44 43 | 0.49 558 | 9.97 890 | 4 | 17 | 1 |
| | 44 | 9.48 371 | 40 | 9.50 485 | 44 | 0.49 515 | 9.97 886 | 4 | 16 | 1 |
| | 45 | 9.48 411 | | 9.50 529 | | 0.49 471 | 9.97 882 | | 15 | 1 |
| | 46 | 9.48 450 | 39 | 9.50 572 | 43 | 0.49 428 | 9.97 878 | 4 | 14 | i |
| | 47 | 9.48 490 | 40 | 9.50 616 | 44 | 0.49 384 | 9.97 874 | 4 | 13 | 1 |
| | 48 | 9.48 529 | 39 39 | 9.50 659 | 43 | 0.49 341 | 9.97 870 | 4 | 12 | 1 |
| | 49 | 9.48 568 | 39 | 9.50 703 | 44 43 | 0.49 297 | 9.97 866 | 4 5 | 11 | |
| | 50 | 9.48 607 | | 9.50 746 | | 0.49 254 | 9.97 861 | | 10 | ĺ |
| į | 51 | 9.48 647 | 40 | 9.50 789 | 43 | 0.49 211 | 9.97 857 | 4 | 9 | ĺ |
| | 52 | 9.48 686 | 39 | 9.50 833 | 44 | 0.49 167 | 9.97 853 | 4 | 8 | |
| | 53 | 9.48 725 | 39 | 9.50 876 | 43 | 0.49 124 | 9.97 849 | 4 | 7 | |
| | 54 | 9.48 764 | 39 39 | 9.50 919 | 43 43 | 0.49 081 | 9.97 845 | 4 | 6 | 1 |
| | 55 | 9.48 803 | Ja | 9.50 962 | 73 | 0.49 038 | 9.97 841 | 4 | 5 | İ |
| | 56 | 9.48 842 | 39 | 9.51 005 | 43 | 0.49 038 | 9.97 837 | 4 | 4 | |
| | 57 | 9.48 881 | 39 | 9.51 048 | 43 | 0.48 952 | 9.97 833 | 4 | 3 | |
| | 58 | 9.48 920 | 39 | 9.51 092 | 44 | 0.48 908 | 9.97 829 | 4 | 2 | |
| | 59 | 9.48 959 | 39 | 9.51 135 | 43 | 0.48 865 | 9.97 825 | 4 | 1 | |
| | 60 | 9.48 998 | 39 | 9.51 178 | 43 | 0.48 822 | 9.97 821 | 4 | 0 | |
| | | | | | | L COT | L COS | | | 342 ⁰ 162 ⁰ |
| Ì | | L SIN | | L TAN | | | | | | |
| | | L COS | D | L COT | CD | L TAN | L SIN | D | | 252° 72° |

| | | | | _ | | | | , | | |
|----------------------------------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|---------|----------|----------|
| 18 ⁰ 198 ⁰ | | L SIN | D | L TAN | CD | L COT | LCOS | D | 1 | |
| 108°288° | | L COS |] | L COT | | L TAN | L SIN | <u></u> | | |
| | 0 | 9.48 098 | | 9.51 178 | | 0.48 822 | 9.97 821 | | 60 | |
| | 1 | 9.49 037 | 39 | 9.51 221 | 43 | 0.48 779 | 9.97 817 | 4 | 59 | |
| | 2 | 9.49 076 | 39 | 9.51 264 | 43 | 0.48 736 | 9.97 812 | 5 | 58 | |
| | 3 | 9.49 115 | 39 | 9.51 306 | 42 | 0.48 694 | 9.97 808 | 4 | 57 | |
| | 4 | 9.49 153 | 38 39 | 9.51 349 | 43 43 | 0.48 651 | 9.97 804 | 4 | 56 | |
| | 5 | 9,49 192 | 1 3 | 9.51 392 | 1 ~~ | 0.48 608 | 9.97 800 | 1 | 55 | 1 |
| | 6 | 9.49 231 | 39 | 9.51 435 | 43 | 0.48 565 | 9.97 796 | 4 | 54 | 1 |
| | 7 | 9.49 269 | 38 | 9.51 478 | 43 | 0.48 522 | 9.97 792 | 4 | 53 | |
| | 8 | 9.49 308 | 39 | 9.51 520 | 42 | 0.48 480 | 9.97 788 | 4 | 52 | |
| | 9 | 9.49 347 | 39 | 9.51 563 | 43 | 0.48 437 | 9.97 784 | 4 | 51 | |
| | 10 | 9.49 385 | 38 | 9.51 606 | 43 | 0.48 394 | 0.07.770 | 5 | 50 | |
| | 11 | 9.49 424 | 39 | 9.51 648 | 42 | 0.48 352 | 9.97 779 9.97 775 | 4 | 49 | |
| | 12 | 9.49 462 | 38 | 9.51 691 | 43 | 0.48 309 | 9.97 771 | 4 | 48 | |
| | 13 | 9.49 500 | 38 | 9.51 734 | 43 | 0.48 266 | 9.97 767 | 4 | 47 | |
| | 14 | 9.49 539 | 39 | 9.51 776 | 42 | 0.48 224 | 9.97 763 | 4 | 46 | |
| | 15 | 0.40.533 | 38 | | 43 | | | 4 | _ | |
| | 15 16 | 9.49 577 | 38 | 9.51 819 | 42 | 0.48 181 | 9.97 759 | 5 | 45 | |
| | 16 17 | 9.49 615 9.49 654 | 39 | 9.51 861 9.51 903 | 42 | 0.48 139 0.48 097 | 9.97 754 | 4 | 44 | |
| | 18 | 9.49 654 | 38 | 9.51 903 9.51 946 | 43 | 0.48 097 | 9.97 750 9.97 746 | 4 | 43 | |
| | 19 | 9.49 730 | 38 | 9.51 946 | 42 | 0.48 054 | 9.97 746 | 4 | 42 41 | |
| | | | 38 | | 43 | | | 4 | | |
| | 20 | 9.49 768 | 38 | 9.52 031 | 42 | 0.47 969 | 9.97 738 | 4 | 40 | |
| | 21 | 9.49 806 | 38 | 9.52 073 | 42 | 0.47 927 | 9.97 734 | 5 | 39 | |
| | 22 | 9.49 844 | 38 | 9.52 115 | 42 | 0.47 885 | 9.97 729 | 4 | 38 | |
| | 23 24 | 9.49 822 9.49 920 | 38 | 9.52 157 9.52 200 | 43 | 0.47 843 0.47 800 | 9.97 725 | 4 | 37 | |
| | | 3.43 320 | 38 | 9.52 200 | 42 | 0.47 800 | 9.97 721 | 4 | 36 | |
| | 25 | 9.49 958 | 38 | 9.52 242 | 42 | 0.47 758 | 9.97 717 | I₄ | 35 | |
| | 26 | 9.49 996 | 38 | 9.52 284 | 42 | 0.47 716 | 9.97 713 | 5 | 34 | |
| | 27 | 9.50 034 | 38 | 9.52 326 | 42 | 0.47 674 | 9.97 708 | 4 | 33 | |
| | 28 29 | 9.50 072 | 38 | 9.52 368 | 42 | 0.47 632 | 9.97 704 | 4 | 32 | |
| | 29 | 9.50 110 | 38 | 9.52 410 | 42 | 0.47 590 | 9.97 700 | 4 | 31 | |
| | 30 | 9.50 148 | 37 | 9.52 452 | ۱ ភ | 0.47 548 | 9.97 699 | ا ۔ ا | 30 | |
| | 31 | 9.50 185 | 38 | 9.52 494 | 42 | 0.47 506 | 9.97 691 | 5 | 29 | |
| | 32 | 9.50 223 | 38 | 9.52 536 | 42 42 | 0.47 464 | 9.97 687 | 4 | 28 | |
| | 33 | 9.50 281 | 37 | 9.52 578 | 42 | 0.47 422 | 9.97 683 | 4 | 27 | |
| | 34 | 9.50 298 | 38 | 9.52 620 | 41 | 0.47 380 | 9.97 679 | 5 | 26 | |
| | 35 | 9.50 336 | 20 | 9.52 661 | 40 | 0.47 339 | 9.97 674 | | 25 | |
| | 36 | 9.50 374 | 38 37 | 9.52 703 | 42 42 | 0.47 297 | 9.97 670 | 4 | 24 | |
| | 37 | 9.50 411 | 38 | 9.52 745 | 42 | 0.47 255 | 9.97 666 | 4 | 23 | |
| | 38 | 9.50 449 | 37 | 9.52 787 | 42 | 0.47 213 | 9.97 662 | 5 | 22 | |
| | 39 | 9.50 486 | 37 | 9.52 829 | 41 | 0.47 171 | 9.97 657 | 4 | 21 | |
| | 40 | 9.50 523 | 20 | 9.52 870 | 40 | 0.47 130 | 9.97 653 | | 20 | |
| | 41 | 9.50 561 | 38 37 | 9.52 912 | 42 | 0.47 088 | 9.97 649 | 4 | 19 | |
| | 42 | 9.50 598 | 37 | 9.52 953 | 41 42 | 0.47 047 | 9.97 645 | 5 | 18 | |
| | 43 | 9.50 635 | 38 | 9.52 995 | 42 | 0.47 005 | 9.97 640 | 4 | 17 | |
| | 44 | 9.50 673 | 37 | 9.53 037 | 41 | 0.46 963 | 9.97 636 | 4 | 16 | |
| | 45 | 9.50 710 | | 9.53 078 | | 0.46 922 | 9.97 632 | | 15 | |
| | 46 | 9.50 747 | 37 | 9.53 120 | 42 | 0.46 880 | 9.97 628 | 4 | 14 | Ì |
| | 47 | 9.50 784 | 37 37 | 9.53 161 | 41 41 | 0.46 839 | 9.97 623 | 5 4 | 13 | |
| | 48 | 9.50 821 | 37 | 9.53 202 | 42 | 0.46 798 | 9.97 619 | 4 | 12 | |
| | 49 | 9.50 858 | 38 | 9.53 244 | 41 | 0.46 756 | 9.97 615 | 5 | 11 | |
| | 50 | 9.50 896 | | 9.53 285 | | 0.46 715 | 9.97 610 | | 10 | |
| | 51 | 9.50 933 | 37 | 9.53 327 | 42 | 0.46 673 | 9.97 606 | 4 | 9 | |
| | 52 | 9.50 970 | 37 37 | 9.53 368 | 41 | 0.46 632 | 9.97 602 | 4 | 8 | |
| | 53 | 9.51 007 | 37 36 | 9.53 409 | 41 41 | 0.46 591 | 9.97 597 | 5 4 | 7 | |
| | 54 | 9.51 043 | 37 | 9.53 450 | 42 | 0.46 550 | 9.97 593 | 4 | 6 | |
| | 55 | 9.51 080 | | 9.53 492 | | 0.46 508 | 9.97 589 | | 5 | |
| | 56 | 9.51 117 | 37 | 9.53 533 | 41 | 0.46 467 | 9.97 584 | 5 | 4 | l |
| | 57 | 9.51 154 | 37 37 | 9.53 574 | 41 | 0.46 426 | 9.97 580 | 4 | 3 | |
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| 57 9.53 301 35 9.55 989 39 0.44 011 9.97 312 4 3 2 556 028 39 9.56 028 39 9.56 067 40 0.43 972 9.97 308 5 1 1 60 9.53 405 9.56 107 0.43 893 9.97 299 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | | | | | 9.55 949 | | | | | | |
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| 9.53 370 35 9.56 067 40 0.43 933 9.97 303 4 1 0 0.43 893 9.97 299 0 0 0 0.43 893 9.97 299 0 0 0 0.43 893 9.97 299 0 0 0 0 0.43 893 9.97 299 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | | | | | | 0.43 972 | 9.97 308 | | 2 | |
| 60 9.53 405 9.56 107 0.43 893 9.97 299 0 L SIN D L TAN CD L COT L COS D 340°160° | | 59 | 9.53 370 | | 9.56 067 | | 0.43 933 | 9.97 303 | | 1 | |
| D CD CD D 3-0100 | | 60 | 9.53 405 | | 9.56 107 | | 0.43 893 | 9.97 299 | | 0 | |
| | | | L SIN | _ | L TAN | C | L COT | L COS | _ | | 340°160° |
| 250°70° | | | 1.009 | J | 1,007 | CD | I TAN | 1.000 | ט | | 05-0 |
| , , , , , , , , , , , , , , , , , , , | | | 2000 | | 1 2001 | | LIAN | LSIN | | | 250 70 |

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|----------|-------------|----------------------|----------|----------------------|----------|----------------------|----------------------|--------|----------|----------|
| 20°200° | ļ | L SIN | D | L TAN | CD | L COT | L COS | | | |
| 110°290° | | L COS | | L COT | | L TAN | L SIN | Ĺ | | |
| | ٥ | 9.53 405 | | 9.56 107 | | 0.43 893 | 9.97 299 | i | 60 | |
| | 1 | 9.53 440 | 35 | 9.56 146 | 39 | 0.43 854 | 9.97 294 | 5 | 59 | |
| | 2 | 9.53 475 | 35 | 9.56 185 | 39 | 0.43 815 | 9.97 289 | 5 | 58 | |
| | 3 | 9.53 509 | 34 | 9.56 224 | 39 | 0.43 776 | 9.97 285 | 4 | 57 | Į. |
| | 4 | 9.53 544 | 35 | 9.56 264 | 40 | 0.43 736 | 9.97 280 | 5 | 56 | |
| | | 0.50.570 | 34 | | 39 | | | 4 | | ł |
| | 5 6 | 9.53 578 9.53 613 | 35 | 9.56 303 9.56 342 | 39 | 0.43 697 | 9.97 276 | 5 | 55 | |
| | 7 | 9.53 647 | 34 | 9.56 381 | 39 | 0.43 658 | 9.97 271 | 5 | 54 | |
| | 8 | 9.53 682 | 35 | 9.56 420 | 39 | 0.43 619 0.43 580 | 9.97 266 9.97 262 | 4 | 53 | |
| | 9 | 9.53 716 | 34 | 9.56 459 | 39 | 0.43 541 | 9.97 257 | 5 | 52 51 | |
| | \vdash | | 35 | 0.00 100 | 39 | 0.40 041 | 0.07 207 | 5 | <u> </u> | 4 |
| | 10 | 9.53 751 | | 9.56 498 | | 0.43 502 | 9.97 252 | Ι. | 50 | |
| | 11 | 9.53 785 | 34 34 | 9.56 537 | 39 | 0.43 463 | 9.97 248 | 4 | 49 | |
| | 12 | 9.53 819 | 35 | 9.56 576 | 39 39 | 0.43 424 | 9.97 243 | 5 5 | 48 | |
| | 13 | 9.53 854 | 34 | 9.56 615 | 39 | 0.43 385 | 9.97 238 | 4 | 47 | |
| | 14 | 9.53 888 | 34 | 9.56 654 | 39 | 0.43 346 | 9.97 234 | 5 | 46 | |
| | 15 | 9.53 922 | | 9.56 693 | | 0.43 307 | 9.97 229 | | 45 | |
| | 16 | 9.53 957 | 35 | 9.56 732 | 39 | 0.43 268 | 9.97 224 | 5 | 44 | |
| | 17 | 9.53 991 | 34 | 9.56 771 | 39 | 0.43 229 | 9.97 220 | 4 | 43 | |
| | 18 | 9.54 025 | 34 | 9.56 810 | 39 | 0.43 190 | 9.97 215 | 5 | 42 | |
| | 19 | 9.54 059 | 34 | 9.56 849 | 39 | 0.43 151 | 9.97 210 | 5 | 41 | |
| | 20 | 9.54 093 | 34 | 9.56 887 | 38 | 0.43 113 | 9.97 206 | 4 | 40 | 1 |
| | 21 | 9.54 127 | 34 | 9.56 926 | 39 | 0.43 113 | 9.97 201 | 5 | 39 | |
| | 22 | 9.54 161 | 34 | 9.56 965 | 39 | 0.43 074 | 9.97 196 | 5 | 38 | |
| | 23 | 9.54 195 | 34 | 9.57 004 | 39 | 0.42 996 | 9.97 192 | 4 | 37 | |
| | 24 | 9.54 229 | 34 | 9.57 042 | 38 | 0.42 958 | 9.97 187 | 5 | 36 | |
| | | | 34 | | 39 | | | 5 | | |
| | 25 | 9.54 263 | 34 | 9.57 081 | 39 | 0.42 919 | 9.97 182 | 4 | 35 | |
| | 26 | 9.54 297 | 34 | 9.57 120 | 38 | 0.42 880 | 9.97 178 | 5 | 34 | |
| | 27 | 9.54 331 | 34 | 9.57 158 | 39 | 0.42 842 | 9.97 173 | 5 | 33 | |
| | 28 29 | 9.54 365 | 34 | 9.57 197 | 38 | 0.42 803 | 9.97 168 | 5 | 32 | |
| | 29 | 9.54 399 | 34 | 9.57 235 | 39 | 0.42 765 | 9.97 163 | 4 | 31 | |
| | 30 | 9.54 433 | | 9.57 274 | | 0.42 726 | 9.97 159 | l | 30 | |
| | 31 | 9.54 466 | 33 | 9.57 312 | 38 | 0.42 688 | 9.97 154 | 5 | 29 | |
| | 32 | 9.54 500 | 34 34 | 9.57 351 | 39 38 | 0.42 649 | 9.97 149 | 5 | 28 | |
| | 33 | 9.54 534 | 33 | 9.57 389 | 39 | 0.42 611 | 9.97 145 | 5 | 27 | |
| | 34 | 9.54 567 | 34 | 9.57 428 | 38 | 0.42 572 | 9.97 140 | 5 | 26 | |
| | 35 | 9.54 601 | | 9.57 466 | 1 | 0.42 534 | 9.97 135 | | 25 | |
| | 36 | 9.54 635 | 34 | 9.57 504 | 38 | 0.42 496 | 9.97 130 | 5 | 24 | |
| | 37 | 9.54 668 | 33 | 9.57 543 | 39 | 0.42 457 | 9.97 126 | 4 | 23 | |
| | 38 | 9.54 702 | 34 | 9.57 581 | 38 | 0.42 419 | 9.57 121 | 5 | 22 | |
| | 39 | 9.54 735 | 33 34 | 9.57 619 | 38 39 | 0.42 381 | 9.57 116 | 5 5 | 21 | |
| | 40 | 9.54 769 | ٠, | 9.57 658 | 1 " | 0.42 342 | 9.97 111 | l " | 20 | 1 |
| | 41 | 9.54 802 | 33 | 9.57 696 | 38 | 0.42 304 | 9.97 107 | 4 | 19 | |
| | 42 | 9.54 836 | 34 | 9.57 734 | 38 | 0.42 266 | 9.97 102 | 5 | 18 | Ì |
| | 43 | 9.54 869 | 33 | 9.57 772 | 38 | 0.42 228 | 9.97 097 | 5 | 17 | I |
| | 44 | 9.54 903 | 34 | 9.57 810 | 38 | 0.42 190 | 9.97 092 | 5 | 16 | I |
| | 45 | 9.54 936 | 33 | 9.57 849 | 39 | 0.42 151 | 9.97 087 | 5 | 15 | I |
| | 46 | 9.54 969 | 33 | 9.57 887 | 38 | 0.42 151 | 9.97 087 | 4 | 15 14 | |
| | 47 | 9.55 003 | 34 | 9.57 925 | 38 | 0.42 113 | 9.97 078 | 5 | 13 | |
| | 48 | 9.55 036 | 33 | 9.57 963 | 38 | 0.42 037 | 9.97 073 | 5 | 12 | |
| | 49 | 9.55 069 | 33 | 9.58 001 | 38 | 0.41 999 | 9.97 068 | 5 | 11 | |
| | = | 0 EE 100 | 33 | 0.50.000 | 38 | 0.44.004 | | 5 | | |
| | 50 51 | 9.55 102 9.55 136 | 34 | 9.58 039 9.58 077 | 38 | 0.41 961 0.41 923 | 9.97 063 | 4 | 10 | |
| | 52 | 9.55 169 | 33 | 9.58 077 | 38 | 0.41 923 | 9.97 059 | 5 | 9 | |
| | 53 | 9.55 202 | 33 | 9.58 153 | 38 | 0.41 847 | 9.97 054 9.97 049 | 5 | 8 7 | |
| | 54 | 9.55 235 | 33 | 9.58 191 | 38 | 0.41 809 | 9.97 049 | 5 | 6 | |
| | | | 33 | | 38 | | | 5 | | |
| | 55 | 9.55 268 | 33 | 9.58 229 | 90 | 0.41 771 | 9.97 039 | , | 5 | |
| | 56 | 9.55 301 | 33 | 9.58 267 | 38 37 | 0.41 733 | 9.97 035 | 4 | 4 | |
| | 57 | 9.55 334 | 33 | 9.58 304 | 37 38 | 0.41 696 | 9.97 030 | 5 5 | 3 | |
| | 58 59 | 9.55 367 | 33 | 9.58 342 | 38 | 0.41 658 | 9.97 025 | 5 | 2 | |
| | 59 | 9.55 400 | 33 | 9.58 380 | 38 | 0.41 620 | 9.97 020 | 5 | 1 | |
| | 60 | 9.55 433 | | 9.58 418 | | 0.41 582 | 9.97 015 | | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | D | | 339°159° |
| | | LCOS | | L COT | | L TAN | L SIN | | | 249° 69° |
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| 21°201° | T | | | | | | | | | 1 |
|-------------|-------------|-------------------------------|----------|----------------------|----------|----------------------|----------------------|--------|-----------|-------|
| | | L SIN | D | L TAN | CD | L COT | LCOS | D | | i |
| 111°291° | | L COS | | L COT | | L TAN | L SIN | | | i |
| | 0 | 9.55 433 | 22 | 9.58 418 | 27 | 0.41 582 | 9.97 015 | ا ۔ | 60 | i |
| | 1 | 9.55 466 | 33 33 | 9.58 455 | 37 38 | 0.41 545 | 9.97 010 | 5 5 | 59 | ŧ |
| | 2 | 9.55 499 | 33 | 9.58 493 | 38 | 0.41 507 | 9.97 005 | 4 | 58 | i |
| | 3 | 9.55 532 | 32 | 9.58 531 | 38 | 0.41 469 | 9.97 001 | 5 | 57 | |
| | 4 | 9.55 564 | 33 | 9.58 569 | 37 | 0.41 431 | 9.96 996 | 5 | 56 | 1 |
| | 5 | 9.55 597 | | 9.58 606 | l | 0.41 394 | 9.96 991 | l I | 55 | 1 |
| | 6 | 9.55 630 | 33 | 9.58 644 | 38 | 0.41 356 | 9.96 986 | 5 | 54 | |
| | 7 | 9.55 663 | 33 32 | 9.58 681 | 37 | 0.41 319 | 9.96 981 | 5 | 53 | |
| | 8 | 9.55 695 | 33 | 9.58 719 | 38 38 | 0.41 281 | 9.96 976 | 5 5 | 52 | 1 |
| | 9 | 9.55 728 | 33 | 9.58 757 | 37 | 0.41 243 | 9.96 971 | 5 | 51 | |
| | 10 | 9.55 761 | | 9.58 794 | 1 | 0.41 206 | 9.96 966 | ľ | 50 | i |
| | 11 | 9.55 793 | 32 | 9.58 832 | 38 | 0.41 168 | 9.96 962 | 4 | 49 | 1 |
| | 12 | 9.55 826 | 33 | 9.58 869 | 37 | 0.41 131 | 9.96 957 | 5 | 48 | |
| | 13 | 9.55 858 | 32 | 9.58 907 | 38 | 0.41 093 | 9.96 952 | 5 | 47 | l |
| | 14 | 9.55 891 | 33 32 | 9.58 944 | 37 37 | 0.41 056 | 9.96 947 | 5 5 | 46 | Î |
| | 15 | 9.55 923 | | 9.58 981 |] " | 0.41 019 | 9.96 942 | | 45 | 1 |
| | 16 | 9.55 923 9.55 9 5 6 | 33 | 9.50 901 | 38 | 0.41 019 | 9.96 942 | 5 | 45 | 1 |
| | 17 | 9.55 988 | 32 | 9.59 056 | 37 | 0.40 944 | 9.96 932 | 5 | 43 | 1 |
| | 18 | 9.56 021 | 33 | 9.59 094 | 38 | 0.40 906 | 9.96 927 | 5 | 42 | 1 |
| | 19 | 9.56 053 | 32 32 | 9.59 131 | 37 | 0.40 869 | 9.96 922 | 5 | 41 | 1 |
| | <u> </u> | | 32 | | 37 | | | 5 | | 1 |
| | 20 21 | 9.56 085 9.56 118 | 33 | 9.59 168 9.59 205 | 37 | 0.40 832 | 9.96 917 | 5 | 40 | 1 |
| | 22 | 9.56 150 | 32 | 9.59 205 | 38 | 0.40 795 0.40 757 | 9.96 912 9.96 907 | 5 | 39 38 | l . |
| | 23 | 9.56 182 | 32 | 9.59 280 | 37 | 0.40 720 | 9.96 903 | 4 | 37 | f |
| | 24 | 9.56 215 | 33 | 9.59 317 | 37 | 0.40 683 | 9.96 898 | 5 | 36 | i |
| | | | 32 | | 37 | | | 5 | | 1 |
| | 25 | 9.56 247 | 32 | 9.59 354 | 37 | 0.40 646 | 9.96 893 | 5 | 35 | 1 |
| | 26 27 | 9.56 279 | 32 | 9.59 391 | 38 | 0.40 609 | 9.96 888 | 5 | 34 | 1 |
| | 28 | 9.56 311 9.56 343 | 32 | 9.59 429 9.59 466 | 37 | 0.40 571 0.40 534 | 9.96 883 9.96 878 | 5 | 33 32 | 1 |
| | 29 | 9.56 375 | 32 | 9.59 503 | 37 | 0.40 497 | 9.96 873 | 5 | 31 | i i |
| | | | 33 | | 37 | | | 5 | | i |
| | 30 | 9.56 408 | 32 | 9.59 540 | 37 | 0.40 460 | 9.96 868 | 5 | 30 | 1 |
| | 31 32 | 9.56 440 9.56 472 | 32 | 9.59 577 9.59 614 | 37 | 0.40 423 0.40 386 | 9.96 863 9.96 858 | 5 | 29 | 1 |
| | 33 | 9.56 504 | 32 | 9.59 651 | 37 | 0.40 349 | 9.96 853 | 5 | 28 27 | 1 |
| | 34 | 9.56 536 | 32 | 9.59 688 | 37 | 0.40 312 | 9.96 848 | 5 | 26 | i |
| | | | 32 | | 37 | | | 5 | | 1 |
| | 35 | 9.56 568 | 31 | 9.59 725 | 37 | 0.40 275 | 9.96 843 | 5 | 25 | 1 |
| | 36 | 9.56 599 | 32 | 9.59 762 | 37 | 0.40 238 | 9.96 838 | 5 | 24 | i |
| | 37 38 | 9.96 631 9.56 663 | 32 | 9.59 799 9.59 835 | 36 | 0.40 201 0.40 165 | 9.96 833 9.96 828 | 5 | 23 | 1 |
| | 39 | 9.56 695 | 32 | 9.59 872 | 37 | 0.40 183 | 9.96 823 | 5 | 22 21 | 1 |
| | | | 32 | | 37 | | | 5 | | 1 |
| | 40 | 9.56 727 | 32 | 9.59 909 | 37 | 0.40 091 | 9.96 818 | 5 | 20 | ı |
| | 41 | 9.56 759 | 31 | 9.59 946 | 37 | 0.40 054 | 9.96 813 | 5 | 19 | 1 |
| | 42 43 | 9.56 790 9.56 822 | 32 | 9.59 983 | 36 | 0.40 017 | 9.96 808 | 5 | 18 | 1 |
| | 44 | 9.56 822 9.56 854 | 32 | 9.60 019 9.60 056 | 37 | 0.39 981 0.39 944 | 9.96 803 9.96 798 | 5 | 17 16 | 1 |
| | | | 32 | | 37 | 0.00 077 | | 5 | <u>.,</u> | 4 |
| | 45 | 9.56 886 | 31 | 9.60 093 | 37 | 0.39 907 | 9.96 793 | 5 | 15 | 1 |
| | 46 | 9.56 917 | 32 | 9.60 130 | 36 | 0.39 870 | 9.96 788 | 5 | 14 | 4 |
| | 47 | 9.56 949 | 31 | 9.60 166 | 37 | 0.39 834 | 9.96 783 | 5 | 13 | 1 |
| | 48 49 | 9.56 980 9.57 012 | 32 | 9.60 203 9.60 240 | 37 | 0.39 797 0.39 760 | 9.96 778 | 5 | 12 | 1 |
| | | | 32 | 5.00 240 | 36 | 0.39 /00 | 9.96 772 | 5 | 11 | 1 |
| | 50 | 9.57 044 | 31 | 9.60 276 | 37 | 0.39 724 | 9.96 767 | 5 | 10 | 1 |
| | 51 | 9.57 075 | 32 | 9.60 313 | 36 | 0.39 687 | 9.96 762 | 5 | 9 | 1 |
| | 52 50 | 9.57 107 | 31 | 9.60 349 | 37 | 0.39 651 | 9.96 757 | 5 | 8 | 1 |
| | 53 54 | 9.57 133 | 31 | 9.60 386 | 36 | 0.39 614 | 9.96 752 | 5 | 7 | 1 |
| | 54 | 9.57 169 | 32 | 9.60 422 | 37 | 0.39 578 | 9.96 747 | 5 | 6 | i |
| | 55 | 9.57 201 | 31 | 9.60 459 | 36 | 0.39 541 | 9.96 742 | ایا | 5 | £ . |
| | 56 | 9.57 232 | 32 | 9.60 495 | 36 37 | 0.39 505 | 9.96 737 | 5 | 4 | 1 |
| | 57 | 9.57 264 | 31 | 9.60 532 | 36 | 0.39 468 | 9.96 732 | 5 | 3 | 1 |
| | 58 | 9.57 295 | 31 | 9.60 568 | 37 | 0.39 432 | 9.96 727 | 5 | 2 | 1 |
| | 59 | 9.57 326 | 32 | 9.60 605 | 36 | 0.39 395 | 9.96 722 | 5 | 1 | i |
| | 60 | 9.57 358 | | 9.60 641 | | 0.39 359 | 9.96 717 | | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | D | | 338°1 |
| | | L COS | | L COT | " | L TAN | L SIN | ا ۱ | | 248° |
| | |] | |] | | - ''' | 2 3114 | | j i | 240 6 |
| | | | | | | | | , | | |

| | | | | | | | - | | | |
|-----------------------------------|-------------|----------------------|-----------|----------------------|----------|----------------------|----------------------|--------|----------|----------------------------------|
| 22°202° | | L SIN | D | L TAN | CD | L COT | L COS | D | | |
| 112 ⁰ 292 ⁰ | | L COS | | L COT | | L TAN | L SIN | | | 1 |
| | 0 | 9.57 358 | | 9.60 641 | | 0.39 359 | 9.96 717 | | 60 | |
| | ľ | 9.57 389 | 31 | 9.60 677 | 36 | 0.39 323 | 9.96 711 | 6 | 59 | |
| | 2 | 9.57 420 | 31 | 9.60 714 | 37 | 0.39 286 | 9.96 706 | 5 | 58 | |
| | 3 | 9.57 451 | 31 | 9.60 750 | 36 | 0.39 250 | 9.96 701 | 5 | 57 | |
| | 4 | 9.57 482 | 31 32 | 9.60 786 | 36 37 | 0.39 214 | 9.96 696 | 5 5 | 56 | |
| | 5 | 9.57 514 | 31 | 9.60 823 | 36 | 0.39 177 | 9.96 691 | 5 | 55 | |
| | 6 | 9.57 545 | 31 | 9.60 859 | 36 | 0.39 141 | 9.96 686 | 5 | 54 | |
| | 7 | 9.57 576 | 31 | 9.60 895 | 36 | 0.39 105 | 9.96 681 | 5 | 53 | |
| | 8 | 9.57 607 | 31 | 9.60 931 | 36 | 0.39 069 | 9.96 676 | 6 | 52 | |
| | 9 | 9.57 638 | 31 | 9.60 967 | 37 | 0.39 033 | 9.96 670 | 5 | 51 | |
| | 10 | 9.57 669 | | 9.61 004 | 20 | 0.38 996 | 9.96 665 | _ | 50 | |
| | 11 | 9.57 700 | 31 | 9.61 040 | 36 36 | 0.38 960 | 9.96 660 | 5 5 | 49 | |
| | 12 | 9.57 731 | 31 31 | 9.61 076 | 36 | 0.38 924 | 9.96 655 | 5 | 48 | |
| | 13 | 9.57 762 | 31 | 9.61 112 | 36 | 0.38 888 | 9.96 650 | 5 | 47 | |
| | 14 | 9.57 793 | 31 | 9.61 148 | 36 | 0.38 852 | 9.96 645 | 5 | 46 | |
| | 15 | 9.57 824 | 04 | 9.61 184 | 0.0 | 0.38 816 | 9.96 640 | | 45 | |
| | 16 | 9.57 855 | 31 | 9.61 220 | 36 36 | 0.38 780 | 9.96 634 | 6 5 | 44 | |
| | 17 | 9.57 885 | 30 | 9.61 256 | 36 | 0.38 744 | 9.96 629 | 5 | 43 | |
| | 18 | 9.57 916 | 31 31 | 9.61 292 | 36 | 0.38 708 | 9.96 624 | 5 | 42 | |
| | 19 | 9.57 947 | 31 | 9.61 328 | 36 | 0.38 672 | 9.96 619 | 5 | 41 | |
| | 20 | 9.57 978 | | 9.61 364 | | 0.38 636 | 9.96 614 | | 40 | |
| | 21 | 9.58 008 | 30 | 9.61 400 | 36 | 0.38 600 | 9.96 608 | 6 | 39 | |
| | 22 | 9.58 039 | 31 | 9.61 436 | 36 | 0.38 564 | 9.96 603 | 5 | 38 | |
| | 23 | 9.58 070 | 31 | 9.61 472 | 36 | 0.38 528 | 9.96 598 | 5 | 37 | |
| | 24 | 9.58 101 | 31 30 | 9.61 508 | 36 36 | 0.38 492 | 9.96 593 | 5 5 | 36 | |
| | 25 | 9.58 131 | 1 | 9.61 544 | 1 | 0.38 456 | 9.96 588 | 1 | 35 | |
| | 26 | 9.58 162 | 31 | 9.61 579 | 35 | 0.38 421 | 9.96 582 | 6 | 34 | |
| | 27 | 9.58 192 | 30 | 9.61 615 | 36 | 0.38 385 | 9.96 577 | 5 | 33 | |
| | 28 | 9.58 223 | 31 | 9.61 651 | 36 | 0.38 349 | 9.96 572 | 5 | 32 | |
| | 29 | 9.58 253 | 30 31 | 9.61 687 | 36 35 | 0.38 313 | 9.96 567 | 5 5 | 31 | |
| | 30 | 9.58 284 | i I | 9.61 722 | 36 | 0.38 278 | 9.96 562 | 6 | 30 | |
| | 31 | 9.58 314 | 30 | 9.61 758 | 36 | 0.38 242 | 9.96 556 | 5 | 29 | |
| | 32 | 9.58 345 | 31 30 | 9.61 794 | 36 | 0.38 206 | 9.96 551 | 5 | 28 | |
| | 33 | 9.58 375 | 31 | 9.61 830 | 35 | 0.38 170 | 9.96 546 | 5 | 27 | |
| | 34 | 9.58 406 | 30 | 9.61 865 | 36 | 0.38 135 | 9.96 541 | 6 | 26 | |
| | 35 | 9.58 436 | 31 | 9.61 901 | 35 | 0.38 099 | 9.96 535 | 5 | 25 | |
| | 36 | 9.58 467 | 30 | 9.61 936 | 36 | 0.38 064 | 9.96 530 | 5 | 24 | |
| | 37 | 9.58 497 | 30 | 9.61 972 | 36 | 0.38 028 | 9.96 525 | 5 | 23 | |
| | 38 | 9.58 527 | 30 | 9.62 008 | 35 | 0.37 992 | 9.96 520 | 6 | 22 | |
| | 39 | 9.58 557 | 31 | 9.62 043 | 36 | 0.37 957 | 9.96 514 | 5 | 21 | |
| | 40 | 9.58 588 | 30 | 9.62 079 | 35 | 0.37 921 | 9.96 509 | 5 | 20 | |
| | 41 | 9.58 618 | 30 | 9.62 114 | 36 | 0.37 886 | 9.96 504 | 6 | 19 | ľ |
| | 42 | 9.58 648 | 30 | 9.62 150 | 35 | 0.37 850 | 9.96 498 | 5 | 18 | Ī |
| | 43 44 | 9.58 678 9.58 709 | 31 | 9.62 185 9.62 221 | 36 | 0.37 815 0.37 779 | 9.96 493 9.96 488 | 5 | 17 16 | |
| | | | 30 | | 35 | | | 5 | | |
| | 45 | 9.58 739 | 30 | 9.62 256 | 36 | 0.37 744 | 9.96 483 | 6 | 15 | Ī |
| | 46 | 9.58 769 | 30 | 9.62 292 | 35 | 0.37 708 | 9.96 477 | 5 | 14 | |
| | 47 | 9.58 799 | 30 | 9.62 327 | 35 | 0.37 673 | 9.96 472 | 5 | 13 | |
| | 48 49 | 9.58 829 9.58 859 | 30 | 9.62 362 9.62 398 | 36 | 0.37 638 0.37 602 | 9.96 467 9.96 461 | 6 | 12 11 | |
| | | | 30 | | 35 | | | 5 | | |
| | 50 51 | 9.58 889 | 30 | 9.62 433 | 35 | 0.37 567 | 9.96 456 | 5 | 10 | |
| | 51 | 9.58 919 | 30 | 9.62 468 | 36 | 0.37 532 | 9.96 451 | 6 | 9 | |
| | 52 53 | 9.58 949 | 30 | 9.62 504 | 35 | 0.37 496 | 9.96 445 | 5 | 8 7 | |
| | 53 54 | 9.58 979 9.59 009 | 30 | 9.62 539 9.62 574 | 35 | 0.37 461 0.37 426 | 9.96 440 9.96 435 | 5 | 6 | |
| | <u> </u> | | 30 | | 35 | | | 6 | | |
| | 55 56 | 9.59 039 9.59 069 | 30 | 9.62 609 | 36 | 0.37 391 | 9.96 429 | 5 | 5 | |
| | 56 57 | | 29 | 9.62 645 | 35 | 0.37 355 | 9.96 424 | 5 | 4 | |
| | 57 59 | 9.59 098 | 30 | 9.62 680 | 35 | 0.37 320 | 9.96 419 | 6 | 3 | |
| | 58 59 | 9.59 128 9.59 158 | 30 | 9.62 715 9.62 750 | 35 | 0.37 285 0.37 250 | 9.96 413 9.96 408 | 5 | 2 | I |
| | | | 30 | | 35 | | | 5 | | |
| | 60 | 9.59 188 | | 9.62 785 | | 0.37 215 | 9.96 403 | | 0 | |
| | | L SIN | D | L TAN | CD | L COT | LCOS | D | | 337°157° |
| | | L COS | | L COT | | L TAN | L SIN | | | 247 [°] 67 [°] |
| | - | - | • | - | • | - | - | • | , ' | • |

| 23°203° | | L SIN | | L TAN | | L COT | L COS | | | Ì |
|----------|-----|----------|----------|----------|----------|----------|----------|--------|----------|---------------------|
| | | | D | | CD | | | D | | |
| 113°293° | | L COS . | | L COT | | L TAN | L SIN | | | |
| | 0 | 9.59 188 | 30 | 9.62 785 | 25 | 0.37 215 | 9.96 403 | | 60 | |
| | 1 | 9.59 218 | 30 29 | 9.62 820 | 35 35 | 0.37 180 | 9.96 397 | 6 5 | 59 | |
| | 2 | 9.59 247 | 30 | 9.62 855 | 35 | 0.37 145 | 9.96 392 | 5 | 58 | |
| | 3 4 | 9.59 277 | 30 | 9.62 890 | 36 | 0.37 110 | 9.96 387 | 6 | 57 56 | |
| | | 9.59 307 | 29 | 9.62 926 | 35 | 0.37 074 | 9.96 381 | 5 | 56 | j |
| | 5 | 9.59 336 | 30 | 9.62 961 | 35 | 0.37 039 | 9.96 376 | 6 | 55 | |
| | 6 | 9.59 366 | 30 | 9.62 996 | 35 | 0.37 004 | 9.96 370 | 5 | 54 | |
| | 7 | 9.59 396 | 29 | 9.63 031 | 35 | 0.36 969 | 9.96 365 | 5 | 53 | |
| | 8 | 9.59 425 | 30 | 9.63 066 | 35 | 0.36 934 | 9.96 360 | 6 | 52 | i |
| | 9 | 9.59 455 | 29 | 9.63 101 | 34 | 0.36 899 | 9.96 354 | 5 | 51 | i |
| | 10 | 9.59 484 | | 9.63 135 | ا م | 0.36 865 | 9.96 349 | ا ا | 50 | |
| | 11 | 9.59 514 | 30 29 | 9.63 170 | 35 35 | 0.36 830 | 9.96 343 | 6 5 | 49 | İ |
| | 12 | 9.59 543 | 30 | 9.63 205 | 35 | 0.36 795 | 9.96 338 | 5 | 48 | i |
| | 13 | 9.59 573 | 29 | 9.63 240 | 35 | 0.36 760 | 9.96 333 | 6 | 47 | i |
| | 14 | 9.59 602 | 30 | 9.63 275 | 35 | 0.36 725 | 9.96 327 | 5 | 46 | i |
| | 15 | 9.59 632 | | 9.63 310 | 1 | 0.36 690 | 9.96 322 | i I | 45 | i |
| | 16 | 9.59 661 | 29 | 9.63 345 | 35 | 0.36 655 | 9.96 316 | 6 | 44 | i |
| | 17 | 9.59 690 | 29 30 | 9.63 379 | 34 | 0.36 621 | 9.96 311 | 5 | 43 | i |
| | 18 | 9.59 720 | 29 | 9.63 414 | 35 35 | 0.36 586 | 9.96 305 | 6 5 | 42 | i |
| | 19 | 9.59 749 | 29 29 | 9.63 449 | 35 35 | 0.36 551 | 9.96 300 | 6 | 41 | i |
| | 20 | 9.59 778 | | 9.63 484 | 1 | 0.36 516 | 9.96 294 | 1 | 40 | i |
| | 21 | 9.59 808 | 30 | 9.63 519 | 35 | 0.36 481 | 9.96 289 | 5 | 39 | į |
| | 22 | 9.59 837 | 29 | 9.63 553 | 34 | 0.36 447 | 9.96 284 | 5 | 38 | i |
| | 23 | 9.59 866 | 29 29 | 9.63 588 | 35 35 | 0.36 412 | 9.96 278 | 6 5 | 37 | i |
| | 24 | 9.59 895 | 29 29 | 9.63 623 | 35 | 0.36 377 | 9.96 273 | 6 | 36 | i |
| | 25 | 9.59 924 | | 9.63 657 | | 0.36 343 | 9.96 267 | | 35 | i |
| | 26 | 9.59 954 | 30 | 9.63 692 | 35 | 0.36 308 | 9.96 262 | 5 | 34 | İ |
| | 27 | 9.59 983 | 29 | 9.63 726 | 34 | 0.36 274 | 9.96 256 | 6 | 33 | |
| | 28 | 9.60 012 | 29 29 | 9.63 761 | 35 35 | 0.36 239 | 9.96 251 | 5 6 | 32 | |
| | 29 | 9.60 041 | 29 | 9.63 796 | 34 | 0.36 204 | 9.96 245 | 5 | 31 | |
| | 30 | 9.60 070 | | 9.63 830 | | 0.36 170 | 9.96 240 | 1 | 30 | |
| | 31 | 9.60 099 | 29 | 9.63 865 | 35 | 0.36 135 | 9.96 234 | 6 | 29 | |
| | 32 | 9.60 128 | 29 | 9.63 899 | 34 | 0.36 101 | 9.96 229 | 5 | 28 | Ì |
| | 33 | 9.60 157 | 29 29 | 9.63 934 | 35 34 | 0.36 066 | 9.96 223 | 6 | 27 | |
| | 34 | 9.60 186 | 29 | 9.63 968 | 35 | 0.36 032 | 9.96 218 | 5 6 | 26 | |
| | 35 | 9.60 215 | | 9.64 003 | | 0.35 997 | 9.96 212 | ľ | 25 | |
| | 36 | 9.60 244 | 29 | 9.64 037 | 34 | 0.35 963 | 9.96 207 | 5 | 24 | İ |
| | 37 | 9.60 273 | 29 | 9.64 072 | 35 | 0.35 928 | 9.96 201 | 6 | 23 | |
| | 38 | 9.60 302 | 29 29 | 9.64 106 | 34 34 | 0.35 894 | 9.96 196 | 5 6 | 22 | |
| | 39 | 9.60 331 | 28 | 9.64 140 | 35 | 0.35 860 | 9.96 190 | 5 | 21 | |
| | 40 | 9.60 359 | | 9.64 175 | | 0.35 825 | 9.96 185 | | 20 | i |
| | 41 | 9.60 388 | 29 | 9.64 209 | 34 | 0.35 791 | 9.96 179 | 6 | 19 | İ |
| | 42 | 9.60 417 | 29 | 9.64 243 | 34 | 0.35 757 | 9.96 174 | 5 | 18 | İ |
| | 43 | 9.60 446 | 29 28 | 9.64 278 | 35 34 | 0.35 722 | 9.96 168 | 6 | 17 | i |
| | 44 | 9.60 474 | 29 | 9.64 312 | 34 | 0.35 688 | 9.96 162 | 5 | 16 | i |
| | 45 | 9.60 503 | | 9.64 346 | | 0.35 654 | 9.96 157 | 1 | 15 | ĺ |
| | 46 | 9.60 532 | 29 | 9.64 381 | 35 | 0.35 619 | 9.96 151 | 6 | 14 | ĺ |
| | 47 | 9.60 561 | 29 | 9.64 415 | 34 | 0.35 585 | 9.96 146 | 5 | 13 | i |
| | 48 | 9.60 589 | 28 29 | 9.64 449 | 34 34 | 0.35 551 | 9.96 140 | 6 | 12 | i |
| | 49 | 9.60 618 | 29 28 | 9.64 483 | 34 34 | 0.35 517 | 9.96 135 | 5 6 | 11 | i |
| | 50 | 9.60 646 | | 9.64 517 | | 0.35 483 | 9.96 129 | 1 | 10 | ĺ |
| | 51 | 9.60 675 | 29 | 9.64 552 | 35 | 0.35 448 | 9.96 123 | 6 | 9 | |
| | 52 | 9.60 704 | 29 | 9.64 586 | 34 | 0.35 414 | 9.96 118 | 5 | 8 | i |
| | 53 | 9.60 732 | 28 | 9.64 620 | 34 | 0.35 380 | 9.96 112 | 6 | 7 | i |
| | 54 | 9.60 761 | 29 28 | 9.64 654 | 34 34 | 0.35 346 | 9.96 107 | 5 6 | 6 | 1 |
| | 55 | 9.60 789 | - | 9.64 688 | ~ | 0.35 312 | 9.96 101 | " | 5 | l |
| | 56 | 9.60 818 | 29 | 9.64 722 | 34 | 0.35 278 | 9.96 095 | 6 | 4 | İ |
| | 57 | 9.60 846 | 28 | 9.64 756 | 34 | 0.35 244 | 9.96 090 | 5 | 3 | İ |
| | 58 | 9.60 875 | 29 | 9.64 790 | 34 | 0.35 210 | 9.96 084 | 6 | 2 | i |
| | 59 | 9.60 903 | 28 | 9.64 824 | 34 | 0.35 176 | 9.96 079 | 5 | 1 | |
| | 60 | 9.60 931 | 28 | 9.64 858 | 34 | 0.35 142 | 9.96 073 | 6 | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | D | | 336 ⁰ 18 |
| | | L COS | ا ۲ | L COT | | L TAN | L SIN | | | 246 ⁰ 6 |
| | | | | | | | | | | ∡ -∠+0 b |

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|----------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|--------|--------------|----------------------------------|
| 24°204° | | L SIN | D | L TAN | CD | L COT | L COS | D | | |
| 114°294° | | L COS | | L COT | | L TAN | L SIN | | | |
| | 0 | 9.60 931 | | 9.64 858 | | 0.35 142 | 9.96 073 | | 60 | |
| | ĭ | 9.60 960 | 29 | 9.64 892 | 34 | 0.35 108 | 9.96 067 | 6 | 59 | |
| | 2 | 9.60 988 | 28 | 9.64 926 | 34 | 0.35 074 | 9.96 062 | 5 | 58 | |
| | 3 | 9.61 016 | 28 | 9.64 960 | 34 | 0.35 040 | 9.96 056 | 6 | 57 | |
| | 4 | 9.61 045 | 29 | 9.64 994 | 34 | 0.35 006 | 9.95 050 | 6 | 56 | |
| | | | 28 | | 34 | | | 5 | - | |
| | 5 | 9.61 073 | 28 | 9.65 028 | 34 | 0.34 972 | 9.96 045 | 6 | 55 | |
| | 6 | 9.61 101 | 28 | 9.65 062 | 34 | 0.34 938 | 9.96 039 | 5 | 54 | |
| | 7 | 9.61 129 | 29 | 9.65 096 | 34 | 0.34 904 | 9.96 034 | 6 | 53 | |
| | 8 9 | 9.61 158 | 28 | 9.65 130 | 34 | 0.34 870 | 9.96 028 | 6 | 52 51 | |
| | - | 9.61 186 | 28 | 9.65 164 | 33 | 0.34 836 | 9.96 022 | 5 | | |
| | 10 | 9.61 214 | 28 | 9.65 197 | 34 | 0.34 803 | 9.96 017 | 6 | 50 | |
| | 11 | 9.61 242 | 26 28 | 9.65 231 | 34 34 | 0.34 769 | 9.96 011 | 6 | 49 | |
| | 12 | 9.61 270 | 28 | 9.65 265 | 34 | 0.34 735 | 9.96 005 | 5 | 48 | |
| | 13 | 9.61 298 | 28 | 9.65 299 | 34 | 0.34 701 | 9.96 000 | 6 | 47 | |
| | 14 | 9.61 326 | 28 | 9.65 333 | 33 | 0.34 667 | 9.95 994 | 6 | 46 | |
| | 15 | 9.61 354 | 1 | 9.65 366 | 1 | 0.34 634 | 9.95 988 | | 45 | |
| | 16 | 9.61 382 | 28 | 9.65 400 | 34 | 0.34 600 | 9.95 982 | 6 | 44 | |
| | 17 | 9.61 411 | 29 | 9.65 434 | 34 | 0.34 566 | 9.95 977 | 5 | 43 | |
| | 18 | 9.61 438 | 27 | 9.65 467 | 33 | 0.34 533 | 9.95 971 | 6 | 42 | |
| | 19 | 9.61 466 | 28 | 9.65 501 | 34 | 0.34 499 | 9.95 965 | 6 | 41 | |
| | | | 28 | | 34 | | | 5 | | |
| | 20 | 9.61 494 | 28 | 9.65 535 | 33 | 0.34 465 | 9.95 960 | 6 | 40 | |
| | 21 | 9.61 522 | 28 | 9.65 568 | 34 | 0.34 432 | 9.95 954 | 6 | 39 | |
| ' | 22 | 9.61 550 | 28 | 9.65 602 | 34 | 0.34 398 | 9.95 948 | 6 | 38 | |
| | 23 24 | 9.61 578 | 28 | 9.65 636 | 33 | 0.34 364 | 9.95 942 | 5 | 37 | |
| | 24 | 9.61 606 | 28 | 9.65 669 | 34 | 0.34 331 | 9.95 937 | 6 | 36 | |
| | 25 | 9.61 634 | ا 🚓 ا | 9.65 703 | ا مما | 0.34 297 | 9.95 931 | | 35 | |
| | 26 | 9.61 662 | 28 | 9.65 736 | 33 | 0.34 264 | 9.95 925 | 6 | 34 | |
| | 27 | 9.61 689 | 27 | 9.65 770 | 34 | 0.34 230 | 9.95 920 | 5 6 | 33 | |
| | 28 | 9.61 717 | 28 28 | 9.65 803 | 33 34 | 0.34 197 | 9.95 914 | 6 | 32 | |
| İ | 29 | 9.61 745 | 28 | 9.65 837 | 33 | 0.34 163 | 9.95 908 | 6 | 31 | |
| | 30 | 9.61 773 | | 9.65 870 | Į į | 0.34 130 | 9.95 902 | | 30 | |
| | 31 | 9.61 800 | 27 | 9.65 904 | 34 | 0.34 096 | 9.95 897 | 5 | 29 | |
| | 32 | 9.61 828 | 28 | 9.65 937 | 33 | 0.34 063 | 9.95 891 | 6 | 28 | |
| | 33 | 9.61 856 | 28 | 9.65 971 | 34 | 0.34 029 | 9.95 885 | 6 | 27 | |
| | 34 | 9.61 883 | 27 | 9.66 004 | 33 | 0.33 996 | 9.95 879 | 6 | 26 | |
| | 35 | 9.61 911 | 28 | 9.66 038 | 34 | 0.33 962 | 9.95 873 | 6 | 25 | |
| | 36 | 9.61 939 | 28 | 9.66 071 | 33 | 0.33 962 | 9.95 868 | 5 | 24 | |
| | 37 | 9.61 966 | 27 | 9.66 104 | 33 | 0.33 896 | 9.95 862 | 6 | 23 | |
| | 38 | 9.61 994 | 28 | 9.66 138 | 34 | 0.33 862 | 9.95 856 | 6 | 22 | |
| | 39 | 9.62 021 | 27 | 9.66 171 | 33 | 0.33 829 | 9.95 850 | 6 | 21 | |
| | | | 28 | | 33 | | | 6 | _ | |
| | 40 | 9.62 049 | 27 | 9.66 204 | 34 | 0.33 796 | 9.95 844 | 5 | 20 | |
| | 41 | 9.62 076 | 28 | 9.66 238 | 33 | 0.33 762 | 9.95 839 | 6 | 19 | |
| | 42 | 9.62 104 | 27 | 9.66 271 | 33 | 0.33 729 | 9.95 833 | 6 | 18 | |
| | 43 | 9.62 131 | 28 | 9.66 304 | 33 | 0.33 696 | 9.95 827 | 6 | 17 | |
| | 44 | 9.62 159 | 27 | 9.66 337 | 34 | 0.33 663 | 9.95 821 | 6 | 16 | |
| | 45 | 9.62 186 | ,, | 9.66 371 | 20 | 0.33 629 | 9.95 815 | , | 15 | |
| | 46 | 9.62 214 | 28 27 | 9.66 404 | 33 | 0.33 596 | 9.95 810 | 5 6 | 14 | |
| | 47 | 9.62 241 | 27 | 9.66 437 | 33 33 | 0.33 563 | 9.95 804 | 6 | 13 | |
| | 48 | 9.62 268 | 28 | 9.66 470 | 33 | 0.33 530 | 9.95 798 | 6 | 12 | |
| | 49 | 9.62 296 | 27 | 9.66 503 | 34 | 0.33 497 | 9.95 792 | 6 | 11 | |
| | 50 | 9.62 323 | | 9.66 527 | | 0.33 463 | 9.95 786 | | 10 | |
| | 51 | 9.62 350 | 27 | 9.66 570 | 33 | 0.33 430 | 9.95 780 | 6 | 9 | |
| | 52 | 9.62 377 | 27 | 9.66 603 | 33 | 0.33 397 | 9.95 775 | 5 | 8 | |
| | 53 | 9.62 405 | 28 | 9.66 636 | 33 | 0.33 364 | 9.95 769 | 6 | 7 | |
| | 54 | 9.62 432 | 27 | 9.66 669 | 33 | 0.33 331 | 9.95 763 | 6 | 6 | |
| | | 0.60.450 | 27 | | 33 | | | 6 | - | |
| | 55 56 | 9.62 459 | 27 | 9.66 702 | 33 | 0.33 298 | 9.95 757 | 6 | 5 | Ī |
| | 56 57 | 9.62 486 9.62 513 | 27 | 9.66 735 | 33 | 0.33 265 | 9.95 751 | 6 | 4 | |
| | 57 50 | | 28 | 9.66 768 | 33 | 0.33 232 | 9.95 745 | 6 | 3 | |
| | 58 59 | 9.62 541 9.62 568 | 27 | 9.66 801 9.66 834 | 33 | 0.33 199 0.33 166 | 9.95 739 9.95 733 | 6 | 2 | |
| | | | 27 | | 33 | | | 5 | | |
| | 60 | 9.62 595 | | 9.66 867 | | 0.33 133 | 9.95 728 | | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | D | | 335°155° |
| | | L COS | | L COT | | L TAN | L SIN | | | 245 [°] 65 [°] |
| | ı | 5 | ı | | I i | | I | i l | | |

| 25°205° | | L SIN | | L TAN | | L COT | LCOS | _ | į | |
|-----------------------------------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|---|--------------|---------------------|
| 115 ⁰ 295 ⁰ | | L COS | D | L COT | ÇD | L TAN | L SIN | D | | |
| | 0 | 9.62 595 | | 9.66 867 | | 0.33 133 | 9.95 728 | | 60 | |
| | 1 | 9.62 622 | 27 | 9.66 900 | 33 | 0.33 133 | 9.95 728 | 6 | 59 | |
| | 2 | 9.62 649 | 27 | 9.66 933 | 33 | 0.33 100 | 9.95 716 | 6 | 58 | |
| į | 3 | 9.62 676 | 27 | 9.66 966 | 33 | 0.33 034 | 9.95 710 | 6 | 57 | |
| | 4 | 9.62 703 | 27 | 9.66 999 | 33 | 0.33 001 | 9.95 704 | 6 | 56 | |
| | | | 27 | | 33 | | | 6 | | |
| | 5 | 9.62 730 | 27 | 9.67 032 | 33 | 0.32 968 | 9.95 698 | 6 | 55 | |
| | 6 | 9.62 757 | 27 | 9.67 065 | 33 | 0.32 935 | 9.95 692 | 6 | 54 | |
| | 7 | 9.62 784 | 27 | 9.67 098 | 33 | 0.32 902 | 9.95 686 | 6 | 53 | |
| | 8 9 | 9.62 811 9.62 838 | 27 | 9.67 131 9.67 163 | 32 | 0.32 869 | 9.95 680 | 6 | 52 =+ | |
| | 9 | 9.02 036 | 27 | 9.67 163 | 33 | 0.32 837 | 9.95 674 | 6 | 51 | |
| | 10 | 9.62 865 | 27 | 9.67 196 | 20 | 0.32 804 | 9.95 668 | _ | 50 | |
| İ | 11 | 9.62 892 | 27 26 | 9.67 229 | 33 | 0.32 771 | 9.95 663 | 5 | 49 | |
| | 12 | 9.62 918 | 26 27 | 9.67 262 | 33 33 | 0.32 738 | 9.95 657 | 6 | 48 | |
| | 13 | 9.62 945 | 27 | 9.67 295 | 33 32 | 0.32 705 | 9.95 651 | 6 | 47 | |
| 1 | 14 | 9.62 972 | 27 | 9.67 327 | 33 | 0.32 673 | 9.95 645 | 6 | 46 | |
| | 15 | 9.62 999 | | 9.67 360 | 33 | 0.32 640 | 9.95 639 | | 45 | |
| | 16 | 9.63 026 | 27 | 9.67 393 | 33 | 0.32 640 | 9.95 633 | 6 | 45 44 | |
| | 17 | 9.63 052 | 26 | 9.67 426 | 33 | 0.32 507 | 9.95 627 | 6 | 43 | |
| | 18 | 9.63 079 | 27 | 9.67 458 | 32 | 0.32 542 | 9.95 621 | 6 | 43 42 | |
| | 19 | 9.63 106 | 27 | 9.67 491 | 33 | 0.32 509 | 9.95 615 | 6 | 41 | |
| | | | 27 | | 33 | | | 6 | _ | |
| | 20 | 9.63 133 | 26 | 9.67 524 | 32 | 0.32 476 | 9.95 609 | 6 | 40 | |
| | 21 | 9.63 159 | 27 | 9.67 556 | 33 | 0.32 444 | 9.95 603 | 6 | 39 | |
| İ | 22 | 9.63 186 | 27 | 9.67 589 | 33 | 0.32 411 | 9.95 597 | 6 | 38 | |
| | 23 | 9.63 213 | 26 | 9.67 622 | 32 | 0.32 378 | 9.95 591 | 6 | 37 | |
| | 24 | 9.63 239 | 27 | 9.67 654 | 33 | 0.32 346 | 9.95 585 | 6 | 36 | |
| | 25 | 9.63 266 | | 9.67 687 | | 0.32 313 | 9.95 579 | | 35 | |
| | 26 | 9.63 292 | 26 | 9.67 719 | 32 | 0.32 281 | 9.95 573 | 8 | 34 | |
| | 27 | 9.63 319 | 27 | 9.67 752 | 33 | 0.32 248 | 9.95 567 | 6 | 33 | |
| | 28 | 9.63 345 | 26 27 | 9.67 785 | 33 | 0.32 215 | 9.95 561 | 6 | 32 | |
| | 29 | 9.63 372 | 27 26 | 9.67 817 | 32 | 0.32 183 | 9.95 555 | 6 | 31 | |
| | 30 | 9.63 398 | 20 | 9.67 850 | 33 | 0.33.150 | 0 0F 540 | 6 | 20 | |
| | 30 | 9.63 398 9.63 425 | 27 | 9.67 850 9.67 882 | 32 | 0.32 150 0.32 118 | 9.95 549 | 6 | 30 | |
| | 32 | 9.63 425 | 26 | 9.67 882 | 33 | 0.32 118 | 9.95 543 | 6 | 29 28 | ľ |
| | 33 | 9.63 478 | 27 | 9.67 947 | 32 | 0.32 063 | 9.95 537 9.95 531 | 6 | 28 27 | |
| | 34 | 9.63 504 | 26 | 9.67 980 | 33 | 0.32 033 | 9.95 525 | 6 | 26 | |
| | | | 27 | | 32 | | J.03 020 | 6 | — <u>—</u> — | |
| | 35 | 9.63 531 | 26 | 9.68 012 | 32 | 0.31 988 | 9.95 519 | 6 | 25 | |
| | 36 | 9.63 557 | 26 | 9.68 044 | 33 | 0.31 956 | 9.95 513 | 6 | 24 | |
| | 37 | 9.63 583 | 27 | 9.68 077 | 32 | 0.31 923 | 9.95 507 | 7 | 23 | |
| ļ | 38 | 9.63 610 | 26 | 9.68 109 | 33 | 0.31 891 | 9.95 500 | 6 | 22 | |
| | 39 | 9.63 636 | 26 | 9.68 142 | 32 | 0.31 858 | 9.95 494 | 6 | 21 | |
| | 40 | 9.63 662 | | 9.68 174 | | 0.31 826 | 9.95 488 | i | 20 | |
| | 41 | 9.63 689 | 27 | 9.68 206 | 32 | 0.31 794 | 9.95 482 | 6 | 19 | 1 |
| | 42 | 9.63 715 | 26 | 9.68 239 | 33 | 0.31 761 | 9.95 476 | 6 | 18 | |
| | 43 | 9.63 741 | 26 26 | 9.68 271 | 32 | 0.31 729 | 9.95 470 | 6 | 17 | ĺ |
| | 44 | 9.63 767 | 26 27 | 9.68 303 | 32 33 | 0.31 697 | 9.95 464 | 6 | 16 | ĺ |
| | 45 | 9.63 794 | ٤′ | 0.69.336 | 33 | 0.21.004 | 0.0E.450 | 6 | 4.5 | l |
| | 45 46 | 9.63 /94 | 26 | 9.68 336 9.68 368 | 32 | 0.31 664 | 9.95 458 | 6 | 15 | |
| | 47 | 9.63 846 | 26 | 9.68 400 | 32 | 0.31 632 0.31 600 | 9.95 452 9.95 446 | 6 | 14 13 | |
| 1 | 48 | 9.63 872 | 26 | 9.68 432 | 32 | 0.31 568 | 9.95 446 | 6 | 12 | ĺ |
| | 49 | 9.63 898 | 26 | 9.68 465 | 33 | 0.31 535 | 9.95 434 | 6 | 11 | 1 |
| | | | 26 | | 32 | | | 7 | | |
| | 50 | 9.63 924 | 26 | 9.68 497 | 32 | 0.31 503 | 9.95 427 | 6 | 10 | |
| | 51 | 9.63 950 | 26 | 9.68 529 | 32 | 0.31 471 | 9.95 421 | 6 | 9 | |
| | 52 | 9.63 976 | 26 | 9.68 561 | 32 | 0.31 439 | 9.95 415 | 6 | 8 | |
| | 53 | 9.64 002 | 26 | 9.68 593 | 33 | 0.31 407 | 9.95 409 | 6 | 7 | 1 |
| | 54 | 9.64 028 | 26 | 9.68 626 | 32 | 0.31 374 | 9.95 403 | 6 | 6 | |
| | 55 | 9.64 054 | | 9.68 658 | | 0.31 342 | 9.95 397 | | 5 | |
| | 56 | 9.64 080 | 26 | 9.68 690 | 32 | 0.31 310 | 9.95 391 | 6 | 4 | |
| | 57 | 9.64 106 | 26 | 9.68 722 | 32 | 0.31 278 | 9.95 384 | 7 | 3 | |
| | 58 | 9.64 132 | 26 | 9.68 754 | 32 | 0.31 246 | 9.95 378 | 6 | 2 | |
| | 59 | 9.64 158 | 26 26 | 9.68 786 | 32 | 0.31 214 | 9.95 372 | 6 | 1 | |
| 1 | 60 | 9.64 184 | 26 | 9.68 818 | 32 | 0.31 182 | 9.95 366 | 6 | 0 | |
| | | L SIN | | L TAN | | L COT | L COS | | | 334°154 |
| • | | L COS | D | | CD | | | D | ┝┈┤ | 244 ⁰ 64 |
| | | | | L COT | | L TAN | L SIN | | | |

| | | | | | | | | | | - |
|----------|-------------|----------------------|----------|----------------------|----------|----------------------|----------------------|--------|----------|----------|
| 26°206° | | L SIN | D | L TAN | CD | L COT | L COS | Ь | | |
| 116°296° | | L COS | | L COT | | L TAN | LSIN | Ĺ | | <u> </u> |
| | 0 | 9.64 184 | | 9.68 818 | | 0.31 182 | 9.95 366 | | 60 | |
| | 1 | 9.64 210 | 26 | 9.68 850 | 32 | 0.31 150 | 9.95 360 | 6 | 59 | |
| | 2 | 9.64 236 | 26 | 9.68 882 | 32 | 0.31 118 | 9.95 354 | 6 | 58 | |
| | 3 | 9.64 262 | 26 | 9.68 914 | 32 | 0.31 086 | 9.95 348 | 6 | 57 | |
| | 4 | 9.64 288 | 26 25 | 9.68 946 | 32 32 | 0.31 054 | 9.95 341 | 7 6 | 56 | |
| | 5 | 9.64 313 | | 9.68 978 | 1 | 0.31 022 | 9.95 335 | 1 ° | 55 | 1 |
| | 6 | 9.64 339 | 26 | 9.69 010 | 32 | 0.30 990 | 9.95 329 | 6 | 54 | |
| | 7 | 9.64 365 | 26 | 9.69 042 | 32 | 0.30 958 | 9.95 323 | 6 | 53 | |
| | 8 | 9.64 391 | 26 | 9.69 074 | 32 | 0.30 926 | 9.95 317 | 6 | 52 | |
| | 9 | 9.64 417 | 26 25 | 9.69 106 | 32 32 | 0.30 894 | 9.95 310 | 7 6 | 51 | |
| | 10 | 9.64 442 | 1 | 9.69 138 | | 0.30 862 | 9.95 304 | 1 | 50 | 1 |
| | 11 | 9.64 468 | 26 | 9.69 170 | 32 | 0.30 830 | 9.95 298 | 6 | 49 | |
| | 12 | 9.64 494 | 26 | 9.69 202 | 32 | 0.30 798 | 9.95 292 | 6 | 48 | |
| | 13 | 9.64 519 | 25 | 9.69 234 | 32 | 0.30 766 | 9.95 286 | 6 | 47 | |
| | 14 | 9.64 545 | 26 26 | 9.69 266 | 32 32 | 0.30 734 | 9.95 279 | 7 | 46 | |
| | 15 | 9.64 571 | 1 | 9.69 298 | 1 | 0.30 702 | 9.95 273 | 1 ້ | 45 | 1 |
| | 16 | 9.64 596 | 25 | 9.69 329 | 31 | 0.30 671 | 9.95 267 | 6 | 45 | |
| | 17 | 9.64 622 | 26 | 9.69 361 | 32 | 0.30 639 | 9.95 261 | 6 | 43 | |
| | 18 | 9.64 647 | 25 | 9.69 393 | 32 | 0.30 607 | 9.95 254 | 7 | 42 | 1 |
| | 19 | 9.64 673 | 26 25 | 9.69 425 | 32 32 | 0.30 575 | 9.95 248 | 6 | 41 | |
| | 20 | 9.64 698 | | 9.69 457 | 1 | 0.30 543 | 9.95 242 | 1 ້ | 40 | 1 |
| | 21 | 9.64 724 | 26 | 9.69 488 | 31 | 0.30 512 | 9.95 236 | 6 | 39 | |
| | 22 | 9.64 749 | 25 | 9.69 520 | 32 | 0.30 480 | 9.95 229 | 7 | 38 | |
| | 23 | 9.64 775 | 26 25 | 9.69 552 | 32 32 | 0.30 448 | 9.95 223 | 6 | 37 | |
| | 24 | 9.64 800 | 26 | 9.69 584 | 31 | 0.30 416 | 9.95 217 | 6 | 36 | |
| | 25 | 9.64 826 | | 9.69 615 | 1 | 0.30 385 | 9.95 211 | 1 | 35 | 1 |
| | 26 | 9.64 851 | 25 | 9.69 647 | 32 | 0.30 353 | 9.95 204 | 7 | 34 | |
| | 27 | 9.64 877 | 26 25 | 9.69 679 | 32 | 0.30 321 | 9.95 198 | 6 | 33 | |
| | 28 | 9.64 902 | 25 25 | 9.69 710 | 31 32 | 0.30 290 | 9.95 192 | 6 7 | 32 | |
| | 29 | 9.64 927 | 26 | 9.69 742 | 32 | 0.30 258 | 9.95 185 | l é | 31 | |
| | 30 | 9.64 953 | 25 | 9.69 774 | | 0.30 226 | 9.95 179 | 1 | 30 | 1 |
| | 31 | 9.64 978 | 25 25 | 9.69 805 | 31 | 0.30 195 | 9.95 173 | 6 | 29 | |
| | 32 | 9.65 003 | 25 26 | 9.69 837 | 32 31 | 0.30 163 | 9.95 167 | 6 7 | 28 | |
| | 33 | 9.65 029 | 25 | 9.69 868 | 32 | 0.30 132 | 9.95 160 | 6 | 27 | |
| | 34 | 9.65 054 | 25 | 9.69 900 | 32 | 0.30 100 | 9.95 154 | 6 | 26 | |
| | 35 | 9.65 079 | 25 | 9.69 932 | 31 | 0.30 068 | 9.95 148 | 7 | 25 | |
| | 36 | 9.65 104 | 26 | 9.69 963 | 32 | 0.30 037 | 9.95 141 | 6 | 24 | |
| | 37 | 9.65 130 | 25 | 9.69 995 | 31 | 0.30 005 | 9.95 135 | 6 | 23 | |
| | 38 | 9.65 155 | 25 | 9.70 026 | 32 | 0.29 974 | 9.95 129 | 7 | 22 | |
| | 39 | 9.65 180 | 25 | 9.70 058 | 31 | 0.29 942 | 9.95 122 | 6 | 21 | |
| | 40 | 9.65 205 | 25 | 9.70 089 | 32 | 0.29 911 | 9.95 116 | 6 | 20 | |
| | 41 | 9.65 230 | 25 | 9.70 121 | 31 | 0.29 879 | 9.95 110 | 7 | 19 | |
| | 42 | 9.65 255 | 26 | 9.70 152 | 32 | 0.29 848 | 9.95 103 | 6 | 18 | |
| | 43 44 | 9.65 281 9.65 306 | 25 | 9.70 184 9.70 215 | 31 | 0.29 816 | 9.95 097 | 7 | 17 | |
| | | 9.65 306 | 25 | 9.70 215 | 32 | 0.29 785 | 9.95 090 | 6 | 16 | Ī |
| | 45 | 9.65 331 | 25 | 9.70 247 | 31 | 0.29 753 | 9.95 084 | 6 | 15 | |
| | 46 | 9.65 356 | 25 | 9.70 278 | 31 | 0.29 722 | 9.95 078 | 7 | 14 | I |
| | 47 48 | 9.65 381 9.65 406 | 25 | 9.70 309 | 32 | 0.29 691 | 9.95 071 | 6 | 13 | I |
| | 49 | 9.65 431 | 25 | 9.70 341 9.70 372 | 31 | 0.29 659 0.29 628 | 9.95 065 9.95 059 | 6 | 12 11 | |
| | | | 25 | | 32 | | | 7 | | |
| | 50 | 9.65 456 | 25 | 9.70 404 | 31 | 0.29 596 | 9.95 052 | 6 | 10 | |
| | 51 52 | 9.65 481 9.65 506 | 25 | 9.70 435 | 31 | 0.29 565 | 9.95 046 | 7 | 9 | |
| | 53 | 9.65 531 | 25 | 9.70 466 9.70 498 | 32 | 0.29 534 0.29 502 | 9.95 039 | 6 | 8 | |
| | 54 | 9.65 556 | 25 | 9.70 498 | 31 | 0.29 502 | 9.95 033 9.95 027 | 6 | 7 6 | İ |
| | | | 24 | | 31 | | | 7 | | |
| | 55 56 | 9.65 580 9.65 605 | 25 | 9.70 560 9.70 592 | 32 | 0.29 440 0.29 408 | 9.95 020 9.95 014 | 6 | 5 | |
| | 57 | 9.65 630 | 25 | 9.70 592 | 31 | 0.29 408 | 9.95 014 9.95 007 | 7 | 4 | Ī |
| | 58 | 9,65 655 | 25 | 9.70 654 | 31 | 0.29 346 | 9.95 007 | 6 | 2 | |
| | 59 | 9.65 680 | 25 25 | 9.70 685 | 31 | 0.29 315 | 9.94 995 | 6 | 1 | |
| | 60 | 9.65 705 | 20 | 9.70 717 | 32 | 0.29 283 | 9.94 988 | 7 | 0 | |
| | | L SIN | | L TAN | | L COT | L COS | | | 333°153° |
| | | L COS | D | L COT | CD | L TAN | L SIN | D | | 243° 63° |
| | | | | | | | | | |] |

| 27°207° | | L SIN | | L TAN | | L COT | L COS | | | |
|-----------------------------------|--|----------------------|----------|----------------------|----------|----------------------|----------------------|--------|----------|----------|
| 117 [°] 297 [°] | | L COS | D | L COT | CD | | | D | | |
| 117297 | | | | 1001 | ļ | L TAN | L SIN | | <u> </u> | |
| | 0 | 9.65 705 | 24 | 9.70 717 | 31 | 0.29 283 | 9.94 988 | 6 | 60 | |
| | 1 2 | 9.65 729 9.65 754 | 25 | 9.70 748 9.70 779 | 31 | 0.29 252 | 9.94 982 | 7 | 59 50 | |
| | 3 | 9.65 779 | 25 | 9.70 779 | 31 | 0.29 221 0.29 190 | 9.94 975 9.94 969 | 6 | 58 57 | |
| | 4 | 9.65 804 | 25 | 9.70 841 | 31 | 0.29 159 | 9.94 962 | 7 | 56 | |
| | | | 24 | | 32 | | | 6 | | |
| | 5 6 | 9.65 828 9.65 853 | 25 | 9.70 873 | 31 | 0.29 127 | 9.94 956 | 7 | 55 | |
| | 7 | 9.65 878 | 25 | 9.70 904 9.70 935 | 31 | 0.29 096 0.29 065 | 9.94 949 9.94 943 | 6 | 54 53 | |
| | 8 | 9.65 902 | 24 | 9.70 966 | 31 | 0.29 034 | 9.94 936 | 7 | 52 | ì |
| | 9 | 9.65 927 | 25 | 9.70 997 | 31 | 0.29 003 | 9.94 930 | 6 | 51 | |
| | 10 | 9.65 962 | 25 | 9.71 028 | 31 | 0.28 972 | 9.94 923 | 7 | 50 | |
| | 11 | 9.65 976 | 24 | 9.71 059 | 31 | 0.28 941 | 9.94 917 | 6 | 49 | |
| | 12 | 9.66 001 | 25 | 9.71 090 | 31 | 0.28 910 | 9.94 911 | 6 | 48 | |
| | 13 | 9.66 025 | 24 25 | 9.71 121 | 31 | 0.28 879 | 9.94 904 | 7 | 47 | |
| | 14 | 9.66 050 | 25 25 | 9.71 153 | 32 31 | 0.28 847 | 9.94 898 | 6 7 | 46 | |
| | 15 | 9.66 075 | | 9.71 184 | | 0.28 816 | 9.94 891 | | 45 | I |
| | 16 | 9.66 099 | 24 | 9.71 215 | 31 | 0.28 785 | 9.94 885 | 6 | 44 | |
| | 17 | 9.66 124 | 25 | 9.71 246 | 31 | 0.28 754 | 9.94 878 | 7 | 43 | 1 |
| | 18 | 9.66 148 | 24 25 | 9.71 277 | 31 31 | 0.28 723 | 9.94 871 | 7 6 | 42 | |
| | 19 | 9.66 173 | 24 | 9.71 308 | 31 | 0.28 692 | 9.94 865 | 7 | 41 | |
| | 20 | 9.66 197 | 1 | 9.71 339 | 1 | 0.28 661 | 9.94 858 | 1 | 40 | |
| | 21 | 9.66 221 | 24 25 | 9.71 370 | 31 31 | 0.28 630 | 9.94 852 | 6 7 | 39 | l |
| | 22 | 9.66 246 | 25 | 9.71 401 | 30 | 0.28 599 | 9.94 845 | 6 | 38 | |
| | 23 24 | 9.66 270 | 25 | 9.71 431 | 31 | 0.28 569 | 9.94 839 | 7 | 37 | |
| | 24 | 9.66 295 | 24 | 9.71 462 | 31 | 0.28 538 | 9.94 832 | 6 | 36 | l |
| | 25 | 9.66 319 | 24 | 9.71 493 | 31 | 0.28 507 | 9.94 826 | 7 | 35 | |
| | 26 | 9.66 343 | 25 | 9.71 524 | 31 | 0.28 476 | 9.94 819 | 6 | 34 | |
| | 27 28 | 9.66 368 9.66 392 | 24 | 9.71 555 9.71 586 | 31 | 0.28 445 0.28 414 | 9.94 813 9.94 806 | 7 | 33 32 | |
| | 29 | 9.66 416 | 24 | 9.71 617 | 31 | 0.28 383 | 9.94 799 | 7 | 31 | |
| | | | 25 | | 31 | | | 6 | _ | |
| | 30 31 | 9.66 441 9.66 465 | 24 | 9.71 648 9.71 679 | 31 | 0.28 352 | 9.94 793 | 7 | 30 | |
| | 32 | 9.66 489 | 24 | 9.71 709 | 30 | 0.28 321 0.28 291 | 9.94 786 9.94 780 | 6 | 29 28 | |
| | 33 | 9.66 513 | 24 | 9.71 740 | 31 | 0.28 260 | 9.94 773 | 7 | 27 | |
| | 34 | 9.66 537 | 24 25 | 9.71 771 | 31 31 | 0.28 229 | 9.94 767 | 6 7 | 26 | |
| | 35 | 9.66 562 | | 9.71 802 | 1 | 0.28 198 | 9.94 760 | 1 | 25 | |
| | 36 | 9.66 586 | 24 | 9.71 833 | 31 | 0.28 167 | 9.94 753 | 7 | 24 | |
| | 37 | 9.66 610 | 24 24 | 9.71 863 | 30 31 | 0.28 137 | 9.94 747 | 6 7 | 23 | |
| | 38 | 9.66 634 | 24 | 9.71 894 | 31 | 0.28 106 | 9.94 740 | 6 | 22 | |
| | 39 | 9.66 658 | 24 | 9.71 925 | 30 | 0.28 075 | 9.94 734 | 7 | 21 | |
| | 40 | 9.66 682 | 24 | 9.71 955 | 1 | 0.28 045 | 9.94 727 | 7 | 20 | l |
| | 41 | 9.66 706 | 25 | 9.71 986 | 31 31 | 0.28 014 | 9.94 720 | 6 | 19 | |
| | 42 | 9.66 731 | 24 | 9.72 017 | 31 | 0.27 983 | 9.94 714 | 7 | 18 | |
| | 43 44 | 9.66 755 9.66 779 | 24 | 9.72 048 9.72 078 | 30 | 0.27 952 0.27 922 | 9.94 707 9.94 700 | 7 | 17 16 | |
| | | | 24 | | 31 | | | 6 | | |
| | 45 | 9.66 803 | 24 | 9.72 109 | 31 | 0.27 891 | 9.94 694 | 7 | 15 | |
| | 46 47 | 9.66 827 9.66 851 | 24 | 9.72 140 9.72 170 | 30 | 0.27 860 0.27 830 | 9.94 687 | 7 | 14 | |
| | 48 | 9.66 875 | 24 | 9.72 170 | 31 | 0.27 830 | 9.94 680 9.94 674 | 6 | 13 12 | l |
| | 49 | 9.66 899 | 24 | 9.72 231 | 30 | 0.27 769 | 9.94 667 | 7 | 11 | Ī |
| | 50 | 9.66 922 | 23 | 9.72 262 | 31 | | | 7 | | l |
| | 50 51 | 9.66 922 | 24 | 9.72 262 9.72 293 | 31 | 0.27 738 0.27 707 | 9.94 660 9.94 654 | 6 | 10 9 | Ī |
| | 52 | 9.66 970 | 24 | 9.72 323 | 30 | 0.27 677 | 9.94 647 | 7 | 8 | |
| | 53 | 9.66 994 | 24 | 9.72 354 | 31 | 0.27 646 | 9.94 640 | 7 | 7 | |
| | 54 | 9.67 018 | 24 24 | 9.72 384 | 30 31 | 0.27 616 | 9.94 634 | 6 7 | 6 | Ī |
| | 55 | 9.67 042 | l i | 9.72 415 | | 0.27 585 | 9.94 627 | 1 | 5 | |
| | 56 | 9.67 066 | 24 | 9.72 445 | 30 | 0.27 555 | 9.94 620 | 7 | 4 | |
| | 57 | 9.67 090 | 24 | 9.72 476 | 31 | 0.27 524 | 9.94 614 | 6 | 3 | ł |
| | 58 | 9.67 113 | 23 24 | 9.72 506 | 30 31 | 0.27 494 | 9.94 607 | 7 | 2 | |
| | 59 | 9.67 137 | 24 | 9.72 537 | 30 | 0.27 463 | 9.94 600 | 7 | 1 | |
| | 60 | 9.67 161 | | 9.72 567 | | 0.27 433 | 9.94 593 | | ٥ | |
| | | L SIN | D | L TAN | CD | L COT | L COS | ٥ | | 332°152° |
| | | L COS | | L COT | | L TAN | L SIN | | | 242° 62° |
| | | | | | | | | | | |

| | T | | | | | | | | 1 | 1 |
|-----------------------------------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|--------|----------|----------|
| 28°208° | | L SIN | D | L TAN | CD | L COT | LCOS | Ь | ļ | |
| 118 ⁰ 298 ⁰ | | L COS | | L COT | | L TAN | L SIN | | |] |
| | 0 | 9.67 161 | 24 | 9.72 567 | 31 | 0.27 433 | 9.94 593 | 6 | 60 | |
| | 1 | 9.67 185 | 23 | 9.72 598 | 30 | 0.27 402 | 9.94 587 | 7 | 59 | |
| | 2 | 9.67 208 | 24 | 9.72 628 | 31 | 0.27 372 | 9.94 580 | 7 | 58 | |
| | 3 | 9.67 232 | 24 | 9.72 659 | 30 | 0.27 341 | 9.94 573 | 6 | 57 | |
| | 4 | 9.67 256 | 24 | 9.72 689 | 31 | 0.27 311 | 9.94 567 | 7 | 56 | 1 |
| | 5 | 9.67 280 | 23 | 9.72 720 | 30 | 0.27 280 | 9.94 560 | 7 | 55 | |
| | 6 | 9.67 303 | 23 | 9.72 750 | 30 30 | 0.27 250 | 9.94 553 | 7 | 54 | |
| | 7 | 9.67 327 | 23 | 9.72 780 | 31 | 0.27 220 | 9.94 546 | 6 | 53 | |
| | 8 | 9.67 350 | 24 | 9.72 811 | 30 | 0.27 189 | 9.94 540 | 7 | 52 | |
| | 9 | 9.67 374 | 24 | 9.72 841 | 31 | 0.27 159 | 9.94 533 | 7 | 51 | Į. |
| | 10 | 9.67 398 | 23 | 9.72 872 | 30 | 0.27 128 | 9.94 526 | 7 | 50 | 1 |
| | 11 | 9.67 421 | 24 | 9.72 902 | 30 | 0.27 098 | 9.94 519 | 6 | 49 | |
| | 12 | 9.67 445 | 23 | 9.72 932 | 31 | 0.27 068 | 9.94 513 | 7 | 48 | |
| | 13 14 | 9.67 468 | 24 | 9.72 963 | 30 | 0.27 037 | 9.94 506 | 7 | 47 | |
| | | 9.67 492 | 23 | 9.72 993 | 30 | 0.27 007 | 9.94 499 | 7 | 46 | |
| | 15 | 9.67 515 | 24 | 9.73 023 | 31 | 0.26 977 | 9.94 492 | 7 | 45 | |
| | 16 | 9.67 539 | 23 | 9.73 054 | 30 | 0.26 946 | 9.94 485 | 6 | 44 | |
| | 17 | 9.67 562 | 24 | 9.73 084 | 30 | 0.26 916 | 9.94 479 | 7 | 43 | |
| | 18 | 9.67 586 | 23 | 9.73 114 | 30 | 0.26 886 | 9.94 472 | 7 | 42 | Ī |
| | 19 | 9.67 609 | 24 | 9.73 144 | 31 | 0.26 856 | 9.94 465 | 7 | 41 | I |
| | 20 | 9.67 633 | 22 | 9.73 175 |] " | 0.26 825 | 9.94 458 |], | 40 | |
| | 21 | 9.67 656 | 23 24 | 9.73 205 | 30 30 | 0.26 795 | 9.94 451 | 7 6 | 39 | |
| | 22 | 9.67 680 | 23 | 9.73 235 | 30 | 0.26 765 | 9.94 445 | 7 | 38 | |
| | 23 | 9.67 703 | 23 | 9.73 265 | 30 | 0.26 735 | 9.94 438 | 7 | 37 | |
| | 24 | 9.67 726 | 24 | 9.73 295 | 31 | 0.26 705 | 9.94 431 | 7 | 36 | |
| | 25 | 9.67 750 | 23 | 9.73 326 | 30 | 0.26 674 | 9.94 424 | 7 | 35 | |
| | 26 | 9.67 773 | 23 | 9.73 356 | 30 | 0.26 644 | 9.94 417 | 7 | 34 | |
| | 27 | 9.67 796 | 24 | 9.73 386 | 30 | 0.26 614 | 9.94 410 | 6 | 33 | |
| | 28 29 | 9.67 820 | 23 | 9.73 416 | 30 | 0.26 584 | 9.94 404 | 7 | 32 | |
| | 29 | 9.67 843 | 23 | 9.73 446 | 30 | 0.26 554 | 9.94 397 | 7 | 31 | |
| | 30 | 9.67 866 | 24 | 9.73 476 | 91 | 0.26 524 | 9.94 390 | 7 | 30 | |
| | 31 | 9.67 890 | 23 | 9.73 507 | 31 30 | 0.26 493 | 9.94 383 | 7 | 29 | |
| | 32 | 9.76 913 | 23 | 9.73 537 | 30 | 0.26 463 | 9.94 376 | 7 | 28 | |
| | 33 34 | 9.67 936 9.67 959 | 23 | 9.73 567 9.73 597 | 30 | 0.26 433 0.26 403 | 9.94 369 9.94 362 | 7 | 27 26 | |
| | | 3.07 333 | 23 | 9.73 097 | 30 | 0.26 403 | 9.94 302 | 7 | 20 | |
| | 35 | 9.67 982 | 24 | 9.73 627 | 30 | 0.26 373 | 9.94 355 | 6 | 25 | |
| | 36 37 | 9.68 006 | 23 | 9.73 657 | 30 | 0.26 343 | 9.94 349 | 7 | 24 | |
| | 38 | 9.68 029 9.68 052 | 23 | 9.73 687 9.73 717 | 30 | 0.26 313 0.26 283 | 9.94 342 9.94 335 | 7 | 23 22 | |
| | 39 | 9.68 075 | 23 | 9.73 747 | 30 | 0.26 253 | 9.94 328 | 7 | 21 | |
| | | | 23 | | 30 | | | 7 | | l |
| | 40 | 9.68 098 | 23 | 9.73 777 | 30 | 0.26 223 | 9.94 321 | 7 | 20 | |
| | 41 42 | 9.68 121 9.68 144 | 23 | 9.73 807 | 30 | 0.26 193 | 9.94 314 | 7 | 19 | |
| | 43 | 9.68 167 | 23 | 9.73 837 9.73 867 | 30 | 0.26 163 0.26 133 | 9.94 307 9.94 300 | 7 | 18 17 | ĺ |
| | 44 | 9.68 190 | 23 | 9.73 897 | 30 | 0.26 103 | 9.94 293 | 7 | 16 | i |
| | | | 23 | | 30 | | | 7 | | |
| | 45 46 | 9.68 213 9.68 237 | 24 | 9.73 927 9.73 957 | 30 | 0.26 073 0.26 043 | 9.94 286 9.94 279 | 7 | 15 | I |
| | 47 | 9.68 260 | 23 | 9.73 987 | 30 | 0.26 043 | 9.94 279 | 6 | 14 13 | |
| | 48 | 9.68 283 | 23 | 9.74 017 | 30 | 0.25 983 | 9.94 266 | 7 | 12 | |
| | 49 | 9.68 305 | 22 | 9.74 047 | 30 | 0.25 953 | 9.94 259 | 7 | 11 | |
| | 50 | 9.68 328 | 23 | 9.74 077 | 30 | 0.25 923 | 9.94 252 | 7 | 10 | |
| | 51 | 9.68 351 | 23 | 9.74 077 | 30 | 0.25 923 | 9.94 252 | 7 | 9 | |
| | 52 | 9.68 374 | 23 | 9.74 137 | 30 | 0.25 863 | 9.94 238 | 7 | 8 | |
| | 53 | 9.68 397 | 23 | 9.74 166 | 29 | 0.25 834 | 9.94 231 | 7 | 7 | |
| | 54 | 9.68 420 | 23 23 | 9.74 196 | 30 30 | 0.25 804 | 9.94 224 | 7 | 6 | |
| | 55 | 9.68 443 | | 9.74 226 | 1 | 0.25 774 | 9.94 217 | 1 | 5 | |
| | 56 | 9.68 466 | 23 | 9.74 256 | 30 | 0.25 744 | 9.94 210 | 7 | 4 | |
| | 57 | 9.68 489 | 23 | 9.74 286 | 30 | 0.25 714 | 9.94 203 | 7 | 3 | |
| | 58 | 9.68 512 | 23 | 9.74 316 | 30 | 0.25 684 | 9.94 196 | 7 | 2 | |
| | 59 | 9.68 534 | 22 23 | 9.74 345 | 29 30 | 0.25 655 | 9.94 189 | 7 | 1 | |
| | 60 | 9.68 557 | | 9.74 375 | | 0.25 625 | 9.94 182 | | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | D | | 331°151° |
| | | L COS | | L COT | | L TAN | L SIN | " | \vdash | 241° 61° |
| | | 2 300 | | | | LIM | r SIM | | | 241 01 |

| 29°209° 119°299° | | L SIN | D | L TAN | CD | LCOT | L COS | l _ | | 1 |
|-----------------------------------|---------------|----------------------|----------|----------------------|----------|----------------------|----------------------|--------|----------|----------|
| 119 ⁰ 299 ⁰ | 1 | | | • | ן טט | | | D | | i |
| | | L COS | | L COT | | L TAN | L SIN | | | |
| | 0 | 9.68 557 | | 9.74 375 | | 0.25 625 | 9.94 182 | | 60 | İ |
| | 1 | 9.68 580 | 23 | 9.74 405 | 30 | 0.25 595 | 9.94 175 | 7 | 59 | i |
| | 2 | 9.68 603 | 23 | 9.74 435 | 30 | 0.25 565 | 9.94 168 | 7 | 58 | i |
| | 3 | 9.68 625 | 22 | 9.74 465 | 30 | 0.25 535 | 9.94 161 | 7 | 57 | i |
| | 4 | 9.68 648 | 23 23 | 9.74 494 | 29 30 | 0.25 506 | 9.94 154 | 7 | 56 | i |
| | 5 | 9.68 671 | | 9.74 524 | | 0.25 476 | 9.94 147 | 1 | 55 | i |
| | 6 | 9.68 694 | 23 | 9.74 554 | 30 | 0.25 446 | 9.94 140 | 7 | 54 | i |
| | 7 | 9.68 716 | 22 | 9.74 583 | 29 | 0.25 417 | 9.94 133 | 7 | 53 | İ |
| | 8 | 9.68 739 | 23 | 9.74 613 | 30 | 0.25 387 | 9.94 126 | 7 | 52 | 1 |
| | 9 | 9.68 762 | 23 22 | 9.74 643 | 30 30 | 0.25 357 | 9.94 119 | 7 | 51 | i |
| | 10 | 9.68 784 | | 9.74 673 | ~ ' | 0.25 327 | 9.94 112 | | 50 | i |
| | 11 | 9.68 807 | 23 | 9.74 702 | 29 | 0.25 298 | 9.94 105 | 7 | 49 | 1 |
| | 12 | 9.68 829 | 22 | 9.74 732 | 30 | 0.25 268 | 9.94 098 | 7 | 48 | Ė |
| | 13 | 9.68 852 | 23 | 9.74 762 | 30 | 0.25 238 | 9.94 090 | 8 | 47 | 1 |
| | 14 | 9.68 875 | 23 | 9.74 791 | 29 | 0.25 209 | 9.94 083 | 7 | 46 | i |
| | 1. | 0.00.00 | 22 | | 30 | | | 7 | | <u> </u> |
| | 15 | 9.68 897 | 23 | 9.74 821 9.74 851 | 30 | 0.25 179 | 9.94 076 | 7 | 45 | i |
| ŀ | 16 17 | 9.68 920 9.68 942 | 22 | 9.74 851 9.74 880 | 29 | 0.25 149 | 9.94 069 | 7 | 44 | i |
| | 18 | 9.68 965 | 23 | 9.74 880 | 30 | 0.25 120 0.25 090 | 9.94 062 9.94 055 | 7 | 43 | i |
| | 19 | 9.68 987 | 22 | 9.74 910 | 29 | 0.25 090 | 9.94 055 9.94 048 | 7 | 42 41 | 1 |
| | | | 23 | | 30 | | | 7 | | İ |
| | 20 | 9.69 010 | 22 | 9.74 969 | 29 | 0.25 031 | 9.94 041 | 7 | 40 | i |
| | 21 | 9.69 032 | 23 | 9.74 998 | 30 | 0.25 002 | 9.94 034 | 7 | 39 | i |
| | 22 | 9.69 055 | 22 | 9.75 028 | 30 | 0.24 972 | 9.94 027 | 7 | 38 | i |
| | 23 24 | 9.69 077 9.69 100 | 23 | 9.75 058 | 29 | 0.24 942 | 9.94 020 | 8 | 37 | i |
| | | 9.09 100 | 22 | 9.75 087 | 30 | 0.24 913 | 9.94 012 | 7 | 36 | i |
| | 25 | 9.69 122 | 22 | 9.75 117 | | 0.24 883 | 9.94 005 | | 35 | Ĺ |
| İ | 26 | 9.69 144 | 22 23 | 9.75 146 | 29 30 | 0.24 854 | 9.93 998 | 7 7 | 34 | i |
| | 27 | 9.69 167 | 22 | 9.75 176 | 29 | 0.24 824 | 9.93 991 | 7 | 33 | i |
| | 28 | 9.69 189 | 23 | 9.75 205 | 30 | 0.24 795 | 9.93 984 | 7 | 32 | |
| | 29 | 9.69 212 | 22 | 9.75 235 | 29 | 0.24 765 | 9.93 977 | 7 | 31 | i |
| | 30 | 9.69 234 | | 9.75 264 | | 0.24 736 | 9.93 970 | _ | 30 | |
| | 31 | 9.69 256 | 22 | 9.75 294 | 30 | 0.24 706 | 9.93 963 | 7 | 29 | i |
| | 32 | 9.69 279 | 23 22 | 9.75 323 | 29 30 | 0.24 677 | 9.93 955 | 8 7 | 28 | i |
| | 33 | 9.69 301 | 22 | 9.75 353 | 29 | 0.24 647 | 9.93 948 | 7 | 27 | Ĺ |
| | 34 | 9.69 323 | 22 | 9.75 382 | 29 | 0.24 618 | 9.93 941 | 7 | 26 | |
| | 35 | 9.69 345 | | 9.75 411 | | 0.24 589 | 9.93 934 | _ | 25 | i |
| | 36 | 9.69 368 | 23 | 9.75 441 | 30 | 0.24 559 | 9.93 927 | 7 | 24 | į. |
| | 37 | 9.69 390 | 22 22 | 9.75 470 | 29 30 | 0.24 530 | 9.93 920 | 7 | 23 | |
| | 38 | 9.69 412 | 22 | 9.75 500 | 29 | 0.24 500 | 9.93 912 | 7 | 22 | l |
| | 39 | 9.69 434 | 22 | 9.75 529 | 29 | 0.24 471 | 9.93 905 | 7 | 21 | İ |
| | 40 | 9.69 456 | | 9.75 558 | | 0.24 442 | 9.93 898 | | 20 | l |
| | 41 | 9.69 479 | 23 | 9.75 588 | 30 | 0.24 412 | 9.93 891 | 7 | 19 | i |
| | 42 | 9.69 501 | 22 | 9.75 617 | 29 | 0.24 383 | 9.93 884 | 7 | 18 | i |
| ļ | 43 | 9.69 523 | 22 22 | 9.75 647 | 30 29 | 0.24 353 | 9.93 876 | 8 7 | 17 | i |
| , | 44 | 9.69 545 | 22 | 9.75 676 | 29 | 0.24 324 | 9.93 869 | 7 | 16 | i |
| ļ | 45 | 9.69 567 | | 9.75 705 | | 0.24 295 | 9.93 862 | | 15 | l |
| ļ | 46 | 9.69 589 | 22 | 9.75 735 | 30 | 0.24 265 | 9.93 855 | 7 | 14 | i |
| | 47 | 9.69 611 | 22 | 9.75 764 | 29 | 0.24 236 | 9.93 847 | 8 | 13 | i |
| ļ | 48 | 9.69 633 | 22 | 9.75 793 | 29 | 0.24 207 | 9.93 840 | 7 | 12 | 1 |
| | 49 | 9.69 655 | 22 22 | 9.75 822 | 29 30 | 0.24 178 | 9.93 833 | 7 | 11 | l |
| ļ | 50 | 9.69 677 | | 9.75 852 | " | 0.24 148 | 9.93 826 | ' | 10 | i |
| ľ | 50 51 | 9.69 699 | 22 | 9.75 881 | 29 | 0.24 148 | 9.93 826 9.93 819 | 7 | 10 9 | 1 |
| | 52 | 9.69 721 | 22 | 9.75 910 | 29 | 0.24 090 | 9.93 811 | 8 | 8 | i |
| ł | 53 | 9.69 743 | 22 | 9.75 939 | 29 | 0.24 061 | 9.93 804 | 7 | 7 | l |
| | 54 | 9.69 765 | 22 | 9.75 969 | 30 | 0.24 031 | 9.93 797 | 7 | 6 | |
| ļ | _ | | 22 | | 29 | | | 8 | _ | i |
| 1 | 55 56 | 9.69 787 9.69 809 | 22 | 9.75 998 | 29 | 0.24 002 | 9.93 789 | 7 | 5 | [|
| | 56 57 | 9.69 831 | 22 | 9.76 027 9.76 056 | 29 | 0.23 973 0.23 944 | 9.93 782 9.93 775 | 7 | 3 | i |
| | 58 | 9.69 853 | 22 | 9.76 086 | 30 | 0.23 944 | 9.93 7/5 9.93 768 | 7 | 2 | ĺ |
| | 59 | 9.69 875 | 22 | 9.76 115 | 29 | 0.23 885 | 9.93 760 | 8 | 1 | |
| | 60 | 9.69 897 | 22 | 9.76 144 | 29 | 0.23 856 | 9.93 753 | 7 | 0 | |
| , | | L SIN | | L TAN | | L COT | L COS | _ | _ | 330°150° |
| | | | | | | | | | | |
| | | L COS | D | L COT | CD | L TAN | L SIN | D | | 240° 60° |

| 00 | 1 | | | | | | | | | |
|----------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|------------------|----------|----------|
| 30°210° | | L SIN | D | L TAN | CD | L COT | L COS | D | | |
| 120°300° | | L COS | | L COT | | L TAN | L SIN | | | |
| | 0 | 9.69 897 | - 22 | 9.76 144 | 29 | 0.23 856 | 9.93 753 | 7 | 60 | |
| | 1 | 9.69 919 | 22 22 | 9.76 173 | 29 | 0.23 827 | 9.93 746 | 8 | 59 | |
| | 2 | 9.69 941 | 22 | 9.76 202 | 29 | 0.23 798 | 9.93 738 | 7 | 58 | |
| | 3 | 9.69 963 | 21 | 9.76 231 | 30 | 0.23 769 | 9.93 731 | 7 | 57 | |
| | 4 | 9.69 984 | 22 | 9.76 261 | 29 | 0.23 739 | 9.93 724 | 7 | 56 | |
| | 5 | 9.70 006 | | 9.76 290 | | 0.23 710 | 9.93 717 | | 55 | |
| | 6 | 9.70 028 | 22 | 9.76 319 | 29 | 0.23 681 | 9.93 709 | 8 7 | 54 | |
| | 7 | 9.70 050 | 22 22 | 9.76 348 | 29 29 | 0.23 652 | 9.93 702 | 7 | 53 | |
| | 8 | 9.70 072 | 21 | 9.76 377 | 29 | 0.23 623 | 9.93 695 | 8 | 52 | |
| | 9 | 9.70 093 | 22 | 9.76 406 | 29 | 0.23 594 | 9.93 687 | 7 | 51 | |
| | 10 | 9.70 115 | | 9.76 435 | | 0.23 565 | 9.93 680 | _ | 50 | |
| | 11 | 9.70 137 | 22 | 9.76 464 | 29 | 0.23 536 | 9.93 673 | 7 | 49 | |
| | 12 | 9.70 159 | 22 21 | 9.76 493 | 29 29 | 0.23 507 | 9.93 665 | 7 | 48 | |
| | 13 | 9.70 180 | 22 | 9.76 522 | 29 | 0.23 478 | 9.93 658 | 8 | 47 | |
| | 14 | 9.70 202 | 22 | 9.76 551 | 29 | 0.23 449 | 9.93 650 | 7 | 46 | |
| | 15 | 9.70 224 | | 9.76 580 | | 0.23 420 | 9.93 643 | ١ , ا | 45 | |
| | 16 | 9.70 245 | 21 | 9.76 609 | 29 30 | 0.23 391 | 9.93 636 | 7 8 | 44 | |
| | 17 | 9.70 267 | 22 21 | 9.76 639 | 30 29 | 0.23 361 | 9.93 628 | 7 | 43 | |
| | 18 | 9.70 288 | 22 | 9.76 668 | 29 | 0.23 332 | 9.93 621 | 7 | 42 | |
| | 19 | 9.70 310 | 22 | 9.76 697 | 28 | 0.23 303 | 9.93 614 | 8 | 41 | |
| | 20 | 9.70 332 | | 9.76 725 | | 0.23 275 | 9.93 606 | | 40 | |
| | 21 | 9.70 353 | 21 | 9.76 754 | 29 29 | 0.23 246 | 9.93 599 | 7 8 | 39 | |
| | 22 | 9.70 375 | 22 21 | 9.76 783 | 29 | 0.23 217 | 9.93 591 | 7 | 38 | |
| | 23 | 9.70 396 | 22 | 9.76 812 | 29 | 0.23 188 | 9.93 584 | 7 | 37 | |
| | 24 | 9.70 418 | 21 | 9.76 841 | 29 | 0.23 159 | 9.93 577 | 8 | 36 | |
| | 25 | 9.70 439 | | 9.76 870 | 1 | 0.23 130 | 9.93 569 | ١., | 35 | |
| | 26 | 9.70 461 | 22 | 9.76 899 | 29 29 | 0.23 101 | 9.93 562 | 7 8 | 34 | |
| | 27 | 9.70 482 | 21 22 | 9.76 928 | 29 29 | 0.23 072 | 9.93 554 | 7 | 33 | |
| | 28 | 9.70 504 | 21 | 9.76 957 | 29 | 0.23 043 | 9.93 547 | 8 | 32 | |
| | 29 | 9.70 525 | 22 | 9.76 986 | 29 | 0.23 014 | 9.93 539 | 7 | 31 | |
| | 30 | 9.70 547 | | 9.77 015 | | 0.22 985 | 9.93 532 | , | 30 | |
| | 31 | 9.70 568 | 21 22 | 9.77 044 | 29 29 | 0.22 956 | 9.93 525 | 7 8 | 29 | |
| | 32 | 9.70 590 | 21 | 9.77 073 | 28 | 0.22 927 | 9.93 517 | 7 | 28 | |
| | 33 | 9.70 611 | 22 | 9.77 101 | 29 | 0.22 899 0.22 870 | 9.93 510 9.93 502 | 8 | 27 26 | |
| | 34 | 9.70 633 | 21 | 9.77 130 | 29 | 0.22 6/0 | 9.93 502 | 7 | 20 | |
| | 35 | 9.70 654 | 21 | 9.77 159 | 29 | 0.22 841 | 9.93 495 | 8 | 25 | |
| | 36 | 9.70 675 | 22 | 9.77 188 | 29 | 0.22 812 | 9.93 487 | 7 | 24 | |
| | 37 | 9.70 697 | 21 | 9.77 217 | 29 | 0.22 783 | 9.93 480 | 8 | 23 | |
| | 38 | 9.70 718 | 21 | 9.77 246 | 28 | 0.22 754 0.22 726 | 9.93 472 9.93 465 | 7 | 22 21 | |
| | 39 | 9.70 739 | 22 | 9.77 274 | 29 | 0.22 720 | 9.93 403 | 8 | | |
| | 40 | 9.70 761 | 21 | 9.77 303 | 29 | 0.22 697 | 9.93 457 | 7 | 20 | |
| | 41 | 9.70 782 | 21 | 9.77 332 | 29 | 0.22 668 | 9.93 450 | 8 | 19 | |
| | 42 | 9.70 803 | 21 | 9.77 361 | 29 | 0.22 639 | 9.93 442 | 7 | 18 17 | i |
| | 43 | 9.70 824 9.70 846 | 22 | 9.77 390 9.77 418 | 28 | 0.22 610 0.22 582 | 9.93 435 9.93 427 | 8 | 16 | |
| | 44 | | 21 | | 29 | | *** | 7 | | |
| | 45 | 9.70 867 | 21 | 9.77 447 | 29 | 0.22 553 | 9.93 420 | ₈ | 15 | |
| | 46 | 9.70 888 | 21 | 9.77 476 | 29 | 0.22 524 | 9.93 412 | 7 | 14 | |
| | 47 48 | 9.70 909 9.70 931 | 22 | 9.77 505 9.77 533 | 28 | 0.22 495 0.22 467 | 9.93 405 9.93 397 | 8 | 13 12 | |
| | 48 49 | 9.70 931 9.70 952 | 21 | 9.77 562 | 29 | 0.22 438 | 9.93 397 | 7 | 11 | |
| | \vdash | | 21 | | 29 | | | 8 | | |
| | 50 | 9.70 973 | 21 | 9.77 591 | 28 | 0.22 409 | 9.93 382 | 7 | 10 | |
| | 51 | 9.70 994 | 21 | 9.77 619 | 29 | 0.22 381 | 9.93 375 9.93 367 | 8 | 9 | |
| | 52 53 | 9.71 015 9.71 036 | 21 | 9.77 648 9.77 677 | 29 | 0.22 352 0.22 323 | 9.93 367 | 7 | 8 7 | |
| | 53 54 | 9.71 036 | 22 | 9.77 706 | 29 | 0.22 323 | 9.93 352 | 8 | 6 | |
| | | | 21 | | 28 | | | 8 | | |
| | 55 | 9.71 079 | 21 | 9.77 734 | 29 | 0.22 266 | 9.93 344 | 7 | 5 | |
| | 56 57 | 9.71 100 | 21 | 9.77 763 | 28 | 0.22 237 | 9.93 337 | 8 | 4 2 | |
| | 57 58 | 9.71 121 9.71 142 | 21 | 9.77 791 9.77 820 | 29 | 0.22 209 0.22 180 | 9.93 329 9.93 322 | 7 | 3 2 | |
| | 58 59 | 9.71 142 9.71 163 | 21 | 9.77 820 9.77 849 | 29 | 0.22 150 | 9.93 322 | 8 | 1 | |
| | 60 | 9.71 184 | 21 | 9.77 877 | 28 | 0.22 123 | 9.93 307 | 7 | 0 | |
| | | ļ | ļ | | | L COT | L COS | - - | _ | 329°149° |
| | | I SIN | | E I IAN | | | | | | |
| | | L SIN | D | L TAN | CD | L TAN | L SIN | P | | 239° 59° |

| 31°211° LSIN D LTAN CD LCOT LCOS | | | |
|---|--------------|----------|-----------------------------------|
| 121°301° LCOS LCOT LTAN LSIN | | | |
| 0 9.71 184 9.77 877 0.22 123 9.93 307 | | 60 | |
| 1 9.71 205 21 9.77 906 29 0.22 094 9.93 299 | 8 | 59 | ! |
| 2 9.71 226 ²¹ 9.77 935 ²⁹ 0.22 085 9.93 291 | 8 | 58 | |
| 3 9.71 247 ²¹ 9.77 963 ²⁸ 0.22 037 9.93 284 | 7 | 57 | |
| 4 9.71 268 ²¹ 9.77 992 ²⁹ 0.22 008 9.93 276 | 8 | 56 | |
| 21 28 | 7 | | |
| 5 9.71 289 9.78 020 0.21 980 9.93 269 | 8 | 55 | |
| 6 9.71 310 21 9.78 049 28 0.21 951 9.93 261 7 9.71 331 21 9.78 077 28 0.21 923 9.93 253 | 8 | 54 50 | |
| 21 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20 | 7 | 53 | ļ |
| 8 9.71 352 21 9.78 106 29 0.21 894 9.93 246 9 9.71 373 21 9.78 135 29 0.21 865 9.93 238 | 8 | 52 51 | |
| 20 28 | - 8 | ۳ | |
| 10 9.71 393 9.78 163 9.91 29 0.21 837 9.93 230 | 7 | 50 | |
| 9.76 192 28 0.21 808 9.93 223 | 8 | 49 | |
| 12 9.71 435 21 9.76 220 29 0.21 780 9.93 215 | 8 | 48 | |
| 13 9.71 490 21 9.76 249 28 0.21 751 9.93 207 | 7 | 47 | İ |
| 14 9.71 477 21 9.78 277 29 0.21 723 9.93 200 | - 8 | 46 | |
| 15 9.71 498 9.78 306 9 0.21 694 9.93 192 | ١. | 45 | 1 |
| 16 9.71 519 21 9.78 334 28 0.21 666 9.93 184 | 8 7 | 44 | |
| 9.71 539 21 9.78 363 28 0.21 637 9.93 177 | lά | 43 |] |
| 16 9.71 500 1 9.78 391 1 00 0.21 809 9.93 169 | l å | 42 | Ī |
| 19 9.71 581 21 9.78 419 29 0.21 581 9.93 161 | ر ا | 41 | |
| 20 9.71 602 9.78 448 0.21 552 9.93 154 | 1 | 40 | |
| 21 9.71 622 ²⁰ 9.78 476 ²⁸ 0.21 524 9.93 146 | 8 | 39 | |
| 22 9.71 643 21 9.76 505 29 0.21 495 9.93 138 | 8 7 | 38 | |
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| 38 9.71 973 ²¹ 9.78 959 ²⁹ 0.21 041 9.93 014 | 8 | 22 | |
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| 26 | | 25 | 9.72 922 | | 9.80 279 | l | 0.19 721 | 9.92 643 | | 35 | |
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| 28 9.72 982 20 9.80 363 28 0.19 637 9.92 619 8 31 31 9.73 002 19 9.80 391 28 0.19 637 9.92 611 8 31 31 9.73 002 19 9.80 447 28 0.19 553 9.92 563 8 29 9.80 530 28 0.19 498 9.92 579 8 27 337 9.73 160 20 9.80 586 28 0.19 442 9.92 555 9.80 586 28 0.19 442 9.92 583 8 21 9.80 669 27 0.19 331 9.92 583 8 21 9.80 669 28 0.19 381 9.92 584 19 9.80 687 29 9.80 882 28 9.80 882 28 9.80 882 28 9.80 882 28 9.80 882 28 9.80 882 28 9.80 882 28 9.80 882 28 9.80 919 29 2485 8 19 9.80 687 9.80 882 28 9.80 919 28 481 9.73 396 20 9.80 882 28 9.80 882 27 0.19 19 9.80 882 28 9.80 919 28 481 9.73 397 19 9.80 882 28 0.19 19 9.80 882 28 0.19 19 9.92 488 8 17 9.73 397 19 9.80 882 28 0.19 19 9.80 883 16 0.19 108 19 9.92 489 8 16 0.19 108 19 9.92 489 8 17 0.19 108 19 9.92 489 8 16 0.19 108 19 9.92 489 8 16 0.19 108 19 9.92 489 8 16 0.19 108 19 9.92 489 8 11 0.19 108 19 9.80 884 11 0.19 108 19 9.80 884 11 0.19 108 108 108 108 108 108 108 108 108 108 | | | | | 9.80 335 | | 0.19 665 | 9.92 627 | | 33 | |
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| 35 | | 34 | 9.73 101 | | 9.80 530 | | 0.19 470 | 9.92 571 | | 26 | |
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| | 0 | 9.73 611 | 19 | 9.81 252 | 27 | 0.18 748 | 9.92 359 | ۱. | 60 | ı | ĺ |
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| | 2 | 9.73 650 | 19 | 9.81 307 | 28 | 0.18 693 | 9.92 343 | 8 | 58 | ı | |
| | 3 4 | 9.73 669 9.73 689 | 20 | 9.81 335 | 27 | 0.18 665 | 9.92 335 | 9 | 57 | | |
| | | 9.73 669 | 19 | 9.81 362 | 28 | 0.18 638 | 9.92 326 | 8 | 56 | | |
| | 5 | 9.73 708 | 19 | 9.81 390 | 28 | 0.18 610 | 9.92 318 | 8 | 55 | ı | |
| | 6 | 9.73 727 | 20 | 9.81 418 | 27 | 0.18 582 | 9.92 310 | l å | 54 | | |
| | 7 | 9.73 747 | 19 | 9.81 445 | 28 | 0.18 555 | 9.92 302 | 9 | 53 | | |
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| | 12 | 9.73 843 | 19 | 9.81 583 | 27 | 0.18 444 0.18 417 | 9.92 269 9.92 260 | 9 | 49 48 | | |
| | 13 | 9.73 863 | 20 | 9.81 611 | 28 | 0.18 389 | 9.92 252 | 8 | 47 | | |
| | 14 | 9.73 882 | 19 | 9.81 638 | 27 | 0.18 362 | 9.92 244 | 8 | 46 | | |
| | 15 | 9.73 901 | 19 | | 28 | | | 9 | | | |
| | 16 | 9.73 901 | 20 | 9.81 666 9.81 693 | 27 | 0.18 334 0.18 307 | 9.92 235 9.92 227 | 8 | 45 44 | | |
| | 17 | 9.73 940 | 19 | 9.81 721 | 28 | 0.18 279 | 9.92 227 | 8 | 43 | | |
| | 18 | 9.73 959 | 19 | 9.81 748 | 27 | 0.18 252 | 9.92 211 | 8 | 42 | | |
| | 19 | 9.73 978 | 19 19 | 9.81 776 | 28 27 | 0.18 224 | 9.92 202 | 9 | 41 | | |
| | 20 | 9.73 997 | | 9.81 803 | | 0.18 197 | 9.92 194 | 8 | 40 | | |
| | 21 | 9.74 017 | 20 | 9.81 831 | 28 | 0.18 169 | 9.92 186 | 8 | 39 | | |
| | 22 | 9.74 036 | 19 | 9.81 858 | 27 | 0.18 142 | 9.92 177 | 9 | 38 | | |
| | 23 | 9.74 055 | 19 19 | 9.81 886 | 28 27 | 0.18 114 | 9.92 169 | 8 8 | 37 | | |
| | 24 | 9.74 074 | 19 | 9.81 913 | 27 28 | 0.18 087 | 9.92 161 | , ° | 36 | | |
| | 25 | 9.74 093 | | 9.81 941 | i | 0.18 059 | 9.92 152 | 1 | 35 | 1 | |
| | 26 | 9.74 113 | 20 19 | 9.81 968 | 27 | 0.18 032 | 9.92 144 | 8 | 34 | | |
| | 27 | 9.74 132 | 19 | 9.81 996 | 28 27 | 0.18 004 | 9.92 136 | 8 | 33 | | |
| | 28 29 | 9.74 151 | 19 | 9.62 023 | 28 | 0.17 977 | 9.92 127 | 8 | 32 | | |
| | 29 | 9.74 170 | 19 | 9.82 051 | 27 | 0.17 949 | 9.92 119 | 8 | 31 | | |
| | 30 | 9.74 189 | 19 | 9.82 078 | 28 | 0.17 922 | 9.92 111 | 9 | 30 | | |
| | 31 | 9.74 208 | 19 | 9.82 106 | 27 | 0.17 894 | 9.92 102 | 8 | 29 | | |
| | 32 33 | 9.74 227 9.74 246 | 19 | 9.82 133 9.82 161 | 28 | 0.17 867 | 9.92 094 | 8 | 28 | | |
| | 34 | 9.74 265 | 19 | 9.82 188 | 27 | 0.17 839 0.17 812 | 9.92 086 9.92 077 | 9 | 27 26 | | |
| | 35 | 9.74 284 | 19 | | 27 | | | 8 | _ | | |
| | 36 | 9.74 204 | 19 | 9.82 215 9.82 243 | 28 | 0.17 785 0.17 757 | 9.92 069 9.92 060 | 9 | 25 24 | | ŀ |
| | 37 | 9.74 322 | 19 | 9.82 270 | 27 | 0.17 730 | 9.92 052 | 8 | 23 | ı | |
| | 38 | 9.74 341 | 19 | 9.82 298 | 28 | 0.17 702 | 9.92 044 | 8 | 22 | ı | |
| | 39 | 9.74 360 | 19 19 | 9.82 325 | 27 27 | 0.17 675 | 9.92 035 | 9 8 | 21 | Į | |
| | 40 | 9.74 379 | | 9.82 352 | | 0.17 648 | 9.92 027 | 1 | 20 | ١ | |
| | 41 | 9.74 398 | 19 | 9.82 380 | 28 | 0.17 648 | 9.92 018 | 9 | 19 | ı | |
| | 42 | 9.74 417 | 19 19 | 9.82 407 | 27 | 0.17 593 | 9.92 010 | 8 | 18 | ĺ | |
| | 43 | 9.74 436 | 19 | 9.82 435 | 28 27 | 0.17 565 | 9.92 002 | 8 9 | 17 | | |
| | 44 | 9.74 455 | 19 | 9.82 462 | 27 | 0.17 538 | 9.91 993 | 8 | 16 | ı | |
| | 45 | 9.74 474 | 19 | 9.82 489 | | 0.17 511 | 9.91 985 | i . | 15 | | |
| | 46 | 9.74 493 | 19 | 9.82 517 | 28 27 | 0.17 483 | 9.91 976 | 9 8 | 14 | ļ | |
| | 47 | 9.74 512 | 19 | 9.82 544 | 27 | 0.17 456 | 9.91 968 | 9 | 13 | ļ | |
| | 48 49 | 9.74 531 9.74 549 | 18 | 9.82 571 9.82 599 | 28 | 0.17 429 | 9.91 959 | 8 | 12 | ı | ŀ |
| | | | 19 | | 27 | 0.17 401 | 9.91 951 | 9 | 11 | ۱ | |
| | 50 | 9.74 568 | 19 | 9.82 626 | 27 | 0.17 374 | 9.91 942 | 8 | 10 | ı | |
| | 51 52 | 9.74 587 | 19 | 9.82 653 | 28 | 0.17 347 | 9.91 934 | 9 | 9 | ı | |
| | 52 53 | 9.74 606 9.74 625 | 19 | 9.82 681 9.82 708 | 27 | 0.17 319 | 9.91 925 | 8 | 8 7 | | |
| | 54 | 9.74 644 | 19 | 9.82 708 | 27 | 0.17 292 0.17 265 | 9.91 917 9.91 908 | 9 | 7 6 | | |
| | | | 18 | | 27 | | | 8 | | | |
| | 55 56 | 9.74 662 9.74 681 | 19 | 9.82 762 | 28 | 0.17 238 | 9.91 900 | 9 | 5 | | |
| | 56 57 | 9.74 681 | 19 | 9.82 790 9.82 817 | 27 | 0.17 210 0.17 183 | 9.91 891 9.91 883 | 8 | 3 | | |
| | 58 | 9.74 719 | 19 | 9.82 844 | 27 | 0.17 155 | 9.91 874 | 9 | 2 | | |
| | 59 | 9.74 737 | 18 | 9.82 871 | 27 | 0.17 129 | 9.91 866 | 8 | 1 | | |
| | 60 | 9.74 756 | 19 | 9.82 899 | 28 | 0.17 101 | 9.91 857 | 9 | 0 | | |
| | | L SIN | D | L TAN | CD | L COT | L COS | , | | | 32 |
| Ì | | L COS | ٠ | L COT | JJ | L TAN | L SIN | D | | | 23 |
| l | | 2 300 | | 200, | | E IAN | LON | | | | ۷. |

| | | | | | | | | | | _ |
|-----------------------------------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|--------|------------|-----------------------------------|
| 34 ⁰ 214 ⁰ | | L SIN | D | L TAN | CD | L COT | L COS | Ь | | |
| 124 ^o 304 ^o | | L COS | | L COT | | L TAN | L SIN | | | |
| | 0 | 9.74 756 | | 9.82 899 | | 0.17 101 | 9.91 857 | | 60 | |
| | 1 | 9.74 775 | 19 | 9.82 926 | 27 | 0.17 074 | 9.91 849 | 8 | 59 | |
| | 2 | 9.74 794 | 19 | 9.82 953 | 27 | 0.17 047 | 9.91 840 | 9 | 58 | |
| | 3 | 9.74 812 | 18 19 | 9.82 980 | 27 28 | 0.17 020 | 9.91 832 | 8 | 57 | |
| | 4 | 9.74 831 | 19 | 9.83 008 | 27 | 0.16 992 | 9.91 823 | 9 8 | 56 | 1 |
| | 5 | 9.74 850 | 18 | 9.83 035 | 27 | 0.16 956 | 9.91 815 | 9 | 55 | |
| | 6 | 9.74 868 | 19 | 9.83 062 | 27 | 0.16 938 | 9.91 806 | 8 | 54 | |
| | 7 8 | 9.74 887 9.74 906 | 19 | 9.83 089 9.83 117 | 28 | 0.16 911 | 9.91 798 | 9 | 53 | |
| | 9 | 9.74 924 | 18 | 9.83 144 | 27 | 0.16 883 0.16 856 | 9.91 789 9.91 781 | 8 | 52 51 | |
| | | | 19 | | 27 | | | 9 | | 1 |
| | 10 | 9.74 943 | 18 | 9.83 171 | 27 | 0.16 829 | 9.91 772 | 9 | 50 | |
| | 11 12 | 9.74 961 9.74 980 | 19 | 9.83 198 9.83 225 | 27 | 0.16 802 0.16 775 | 9.91 763 9.91 755 | 8 | 49 | |
| | 13 | 9.74 999 | 19 | 9.83 252 | 27 | 0.16 7/8 | 9.91 746 | 9 | 48 47 | |
| | 14 | 9.75 017 | 18 | 9.83 280 | 28 | 0.16 720 | 9.91 738 | 8 | 46 | |
| | 45 | | 19 | | 27 | | | 9 | | İ |
| | 15 16 | 9.75 036 9.75 054 | 18 | 9.83 307 9.83 334 | 27 | 0.16 693 0.16 666 | 9.91 729 | 9 | 45 | |
| | 17 | 9.75 054 | 19 | 9.83 334 9.83 361 | 27 | 0.16 666 | 9.91 720 9.91 712 | 8 | 44 43 | |
| | 18 | 9.75 091 | 18 | 9.83 388 | 27 | 0.16 612 | 9.91 703 | 9 | 43 42 | |
| | 19 | 9.75 110 | 19 | 9.83 415 | 27 | 0.16 585 | 9.91 695 | 8 | 41 | |
| | 20 | 9.75 128 | 18 | 9.83 442 | 27 | 0.16 558 | | 9 | lacksquare | 1 |
| | 21 | 9.75 128 9.75 147 | 19 | 9.83 442 9.83 470 | 28 | 0.16 558 0.16 530 | 9.91 686 9.91 677 | 9 | 40 39 | |
| | 22 | 9.75 165 | 18 | 9.83 497 | 27 | 0.16 503 | 9.91 669 | 8 | 38 | |
| | 23 | 9.75 184 | 19 | 9.83 524 | 27 | 0.16 476 | 9.91 660 | 9 | 37 | |
| | 24 | 9.75 202 | 18 19 | 9.83 551 | 27 27 | 0.16 449 | 9.91 651 | 9 | 36 | |
| | 25 | 9.75 221 | | 9.83 578 | 1 | 0.16 422 | 9.91 643 | B | 35 | 1 |
| | 26 | 9.75 239 | 18 | 9.83 605 | 27 | 0.16 395 | 9.91 634 | 9 | 34 | |
| | 27 | 9.75 258 | 19 | 9.83 632 | 27 | 0.16 368 | 9.91 625 | 9 | 33 | |
| | 28 | 9.75 276 | 18 18 | 9.83 659 | 27 27 | 0.16 341 | 9.91 617 | 8 9 | 32 | |
| | 29 | 9.75 294 | 19 | 9.83 686 | 27 | 0.16 314 | 9.91 608 | 9 | 31 | 1 |
| | 30 | 9.75 313 | 18 | 9.83 713 | 27 | 0.16 287 | 9.91 599 | | 30 | |
| | 31 32 | 9.75 331 | 19 | 9.83 740 | 28 | 0.16 260 | 9.91 591 | 8 9 | 29 | |
| | 32 | 9.75 350 9.75 368 | 18 | 9.83 768 9.83 795 | 27 | 0.16 232 0.16 205 | 9.91 582 9.91 573 | 9 | 28 27 | |
| | 34 | 9.75 386 | 18 | 9.83 822 | 27 | 0.16 203 | 9.91 565 | 8 | 26 | |
| | 35 | 9.75 405 | 19 | 9.83 849 | 27 | 0.16 151 | 9.91 556 | 9 | | ł |
| | 36 | 9.75 423 | 18 | 9.83 876 | 27 | 0.16 124 | 9.91 547 | 9 | 25 24 | |
| | 37 | 9.75 441 | 18 | 9.83 903 | 27 | 0.16 097 | 9.91 538 | 9 | 23 | |
| | 38 | 9.75 459 | 18 | 9.83 930 | 27 | 0.16 070 | 9.91 530 | 8 | 22 | |
| | 39 | 9.75 478 | 19 18 | 9.83 957 | 27 27 | 0.16 043 | 9.91 521 | 9 | 21 | |
| | 40 | 9.75 496 | | 9.83 984 | | 0.16 016 | 9.91 512 | | 20 | 1 |
| | 41 | 9.75 514 | 18 | 9.84 011 | 27 | 0.15 989 | 9.91 504 | 8 | 19 | |
| | 42 | 9.75 533 | 19 18 | 9.84 038 | 27 27 | 0.15 962 | 9.91 495 | 9 | 18 | |
| | 43 44 | 9.75 551 9.75 569 | 18 | 9.84 065 | 27 | 0.15 935 | 9.91 486 | 9 | 17 | |
| | | | 18 | 9.84 092 | 27 | 0.15 908 | 9.91 477 | 8 | 16 | Ì |
| | 45 | 9.75 587 | 18 | 9.84 119 | 27 | 0.15 881 | 9.91 469 | 9 | 15 | |
| | 46 47 | 9.75 605 9.75 624 | 19 | 9.84 146 9.84 173 | 27 | 0.15 854 0.15 827 | 9.91 460 9.91 451 | 9 | 14 | ĺ |
| | 48 | 9.75 624 9.75 642 | 18 | 9.84 200 | 27 | 0.15 827 | 9.91 451 | 9 | 13 12 | ĺ |
| | 49 | 9.75 660 | 18 | 9.84 227 | 27 | 0.15 773 | 9.91 433 | 9 | 11 | |
| | 50 | 9.75 678 | 18 | 9.84 254 | 27 | 0.15 746 | 9.91 425 | 8 | 10 | l |
| | 51 | 9.75 696 | 18 | 9.84 280 | 26 | 0.15 720 | 9.91 416 | 9 | 9 | I |
| | 52 | 9.75 714 | 18 | 9.84 307 | 27 | 0.15 693 | 9.91 407 | 9 | 8 | Ī |
| | 53 | 9.75 733 | 19 18 | 9.84 334 | 27 27 | 0.15 666 | 9.91 398 | 9 | 7 | |
| | 54 | 9.75 751 | 18 | 9.84 361 | 27 | 0.15 639 | 9.91 389 | 8 | 6 | |
| | 55 | 9.75 769 | | 9.84 388 | | 0.15 612 | 9.91 381 | | 5 | |
| | 56 | 9.75 787 | 18 18 | 9.84 415 | 27 27 | 0.15 585 | 9.91 372 | 9 | 4 | |
| | 57 50 | 9.75 805 | 18 | 9.84 442 | 27 | 0.15 558 | 9.91 363 | 9 | 3 | |
| | 58 59 | 9.75 823 9.75 841 | 18 | 9.84 469 | 27 | 0.15 531 | 9.91 354 | 9 | 2 | |
| | | 9.75 841 | 18 | 9.84 496 | 27 | 0.15 504 | 9.91 345 | 9 | 1 | |
| | 60 | 9.75 859 | | 9.84 523 | | 0.15 477 | 9.91 336 | | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | D | | 325 ⁰ 145 ⁰ |
| | | L COS | | L COT | | L TAN | L SIN | | | 235 [°] 55 [°] |

| | т— | | | | | | ı | | | |
|----------|------------|----------------------|----------|-------------------------------|----------|----------------------|----------------------|--------|----------|----------------------------------|
| 35°215° | | L SIN | D | L TAN | CD | L COT | L COS | D | | |
| 125°305° | | L COS | | L COT | | L TAN | L SIN | | | |
| | 0 | 9.75 859 | 4.0 | 9.84 523 | | 0.15 477 | 9.91 336 | ١. | 60 | |
| | 1 | 9.75 877 | 18 18 | 9.84 550 | 27 26 | 0.15 450 | 9.91 328 | 8 9 | 59 | |
| | 2 | 9.75 895 | 18 | 9.84 576 | 27 | 0.15 424 | 9.91 319 | 9 | 58 | |
| | 3 | 9.75 913 | 18 | 9.84 603 | 27 | 0.15 397 | 9.91 310 | 9 | 57 | |
| | 4 | 9.75 931 | 18 | 9.84 630 | 27 | 0.15 370 | 9.91 301 | 9 | 56 | |
| | 5 | 9.75 949 | ا ۱۰ | 9.84 657 |] | 0.15 343 | 9.91 292 | ١, | 55 | |
| | 6 | 9.75 967 | 18 | 9.84 684 | 27 | 0.15 316 | 9.91 283 | 9 | 54 | |
| | 7 | 9.75 985 | 18 18 | 9.84 711 | 27 27 | 0.15 289 | 9.91 274 | 9 8 | 53 | |
| | 8 | 9.76 003 | 18 | 9.84 738 | 26 | 0.15 262 | 9.91 266 | 9 | 52 | |
| | 9 | 9.76 021 | 18 | 9.84 764 | 27 | 0.15 236 | 9.91 257 | 9 | 51 | |
| | 10 | 9.76 039 | 40 | 9.84 791 | | 0.15 209 | 9.91 248 | } ' | 50 | |
| | 11 | 9.76 057 | 18 | 9.84 818 | 27 27 | 0.15 182 | 9.91 239 | 9 | 49 | |
| | 12 | 9.76 075 | 18 18 | 9.84 845 | 27 | 0.15 155 | 9.91 230 | 9 | 48 | |
| | 13 | 9.76 093 | 18 | 9.84 872 | 27 | 0.15 128 | 9.91 221 | 9 | 47 | |
| | 14 | 9.76 111 | 18 | 9.84 899 | 26 | 0.15 101 | 9.91 212 | 9 | 46 | |
| | 15 | 9.76 129 | | 9.84 925 | | 0.15 075 | 9.91 203 | | 45 | |
| | 16 | 9.76 146 | 17 | 9.84 952 | 27 | 0.15 048 | 9.91 194 | 9 | 44 | |
| | 17 | 9.76 164 | 18 | 9.84 979 | 27 | 0.15 021 | 9.91 185 | 9 | 43 | |
| | 18 | 9.76 182 | 18 | 9.85 006 | 27 | 0.14 994 | 9.91 176 | 9 | 42 | |
| | 19 | 9.76 200 | 18 18 | 9.85 033 | 27 26 | 0.14 967 | 9.91 167 | 9 | 41 | |
| | 20 | 9.76 218 | | 9.85 059 | | 0.14 941 | 9.91 158 | | 40 | |
| | 21 | 9.76 236 | 18 | 9.85 086 | 27 | 0.14 941 | 9.91 156 | 9 | 39 | |
| | 22 | 9.76 253 | 17 | 9.85 113 | 27 | 0.14 887 | 9.91 141 | 8 | 38 | |
| | 23 | 9.76 271 | 18 | 9.85 140 | 27 | 0.14 860 | 9.91 132 | 9 | 37 | |
| | 24 | 9.76 289 | 18 18 | 9.85 166 | 26 27 | 0.14 834 | 9.91 123 | 9 | 36 | |
| | 25 | 0.76.207 | 10 | 0.05.100 | 1 | 0.14.007 | 0.04.444 | ľ | 25 | |
| | 25 26 | 9.76 307 9.76 324 | 17 | 9.85 193 9.85 220 | 27 | 0.14 807 | 9.91 114 | 9 | 35 | |
| | 27 | 9.76 342 | 18 | 9.85 247 | 27 | 0.14 780 0.14 753 | 9.91 105 9.91 096 | 9 | 34 33 | |
| | 28 | 9.76 360 | 18 | 9.85 273 | 26 | 0.14 733 | 9.91 087 | 9 | 32 | |
| | 29 | 9.76 378 | 18 | 9.85 300 | 27 | 0.14 700 | 9.91 078 | 9 | 31 | |
| | - 20 | 0.70.005 | . 17 | 0.05.007 | 27 | 0.44.070 | | 9 | | |
| | 30 31 | 9.76 395 9.76 413 | 18 | 9.85 327 9.85 354 | 27 | 0.14 673 | 9.91 069 | 9 | 30 | |
| | 32 | 9.76 431 | 18 | 9.85 380 | 26 | 0.14 646 0.14 620 | 9.91 060 9.91 051 | 9 | 29 28 | |
| | 33 | 9.76 448 | 17 | 9.85 407 | 27 | 0.14 593 | 9.91 042 | 9 | 27 | |
| | 34 | 9.76 466 | 18 | 9.85 434 | 27 | 0.14 566 | 9.91 033 | 9 | 26 | |
| | 0.5 | | 18 | | 26 | | | 10 | | |
| | 35 36 | 9.76 484 9.76 501 | 17 | 9.85 460 9.85 487 | 27 | 0.14 540 | 9.91 023 | 9 | 25 | |
| | 37 | 9.76 519 | 18 | 9.85 514 | 27 | 0.14 513 0.14 486 | 9.91 014 9.91 005 | 9 | 24 23 | |
| | 38 | 9.76 537 | 18 | 9.85 540 | 26 | 0.14 460 | 9.90 996 | 9 | 22 | |
| | 39 | 9.76 554 | 17 | 9.85 567 | 27 | 0.14 433 | 9.90 987 | 9 | 21 | |
| | 40 | | 18 | | 27 | | | 9 | | |
| | 40 41 | 9.76 572 9.76 590 | 18 | 9.85 594 9.85 620 | 26 | 0.14 406 | 9.90 978 | 9 | 20 | 1 |
| | 41 | 9.76 590 | 17 | 9.85 620 9.85 647 | 27 | 0.14 380 0.14 353 | 9.90 969 9.90 960 | 9 | 19 18 | l |
| | 43 | 9.76 625 | 18 | 9.85 674 | 27 | 0.14 333 | 9.90 951 | 9 | 17 | |
| | 44 | 9.76 642 | 17 | 9.85 700 | 26 | 0.14 300 | 9.90 942 | 9 | 16 | |
| | | | 18 | | 27 | | | 9 | | |
| | 45 46 | 9.76 660 | 17 | 9.85 727 | 27 | 0.14 273 | 9.90 933 | 9 | 15 | |
| | 46 47 | 9.76 677 9.76 695 | 18 | 9.85 7 5 4 9.85 780 | 26 | 0.14 246 0.14 220 | 9.90 924 9.90 915 | 9 | 14 | l |
| | 48 | 9.76 712 | 17 | 9.85 /80 | 27 | 0.14 220 | 9.90 915 | 9 | 13 12 | |
| | 49 | 9.76 730 | 18 | 9.85 834 | 27 | 0.14 166 | 9.90 896 | 10 | 11 | |
| | — — | | 17 | | 26 | - | | 9 | | |
| | 50 | 9.76 747 | 18 | 9.85 860 | 27 | 0.14 140 | 9.90 887 | 9 | 10 | |
| | 51 52 | 9.76 765 9.76 782 | 17 | 9.85 887 9.85 913 | 26 | 0.14 113 0.14 087 | 9.90 878 | 9 | 9 | |
| | 53 | 9.76 800 | 18 | 9.85 940 | 27 | 0.14 087 | 9.90 869 9.90 860 | 9 | 8 7 | |
| | 54 | 9.76 817 | 17 | 9.85 967 | 27 | 0.14 033 | 9.90 851 | 9 | 6 | |
| | | | 18 | | 26 | | | 9 | | |
| | 55 56 | 9.76 835 | 17 | 9.85 993 | 27 | 0.14 007 | 9.90 842 | 10 | 5 | |
| | 56 57 | 9.76 852 | 18 | 9.86 020 | 26 | 0.13 980 | 9.90 832 | 9 | 4 | |
| | 57 58 | 9.76 870 9.76 887 | 17 | 9.86 046 9.86 073 | 27 | 0.13 954 | 9.90 823 | 9 | 3 | |
| | 58 59 | 9.76 904 | 17 | 9.86 100. | 27 | 0.13 927 0.13 900 | 9.90 814 9.90 805 | 9 | 2 | 1 |
| | | | 18 | | 26 | , | | 9 | | |
| | 60 | 9.76 922 | | 9.86 126 | | 0.13 874 | 9.90 796 | | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | ٥ | | 324°144° |
| | | L COS | | L COT | | L TAN | L SIN | | | 234 ⁰ 54 ⁰ |
| |] | | , | | |] | ! | | | |

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|----------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|---------|----------|---|---------|
| 36°216° | | L SIN | _ | L TAN | | L COT | L COS | | . 1 | l | |
| 126°306° | | L COS | D | L COT | CD | L TAN | L SIN | D | | | |
| 120300 | | 2000 | | - 1001 | | E 1/A.V | Lonv | | | | |
| | 0 | 9.76 922 | 17 | 9.86 126 | 27 | 0.13 874 | 9.90 796 | 9 | 60 | | |
| | 1 | 9.76 939 | 18 | 9.86 153 | 26 | 0.13 847 | 9.90 787 | 10 | 59 | | |
| | 2 | 9.76 957 | 17 | 9.86 179 | 27 | 0.13 821 | 9.90 777 | 9 | 58 | | |
| | 3 4 | 9.76 974 9.76 991 | 17 | 9.86 206 9.86 232 | 26 | 0.13 794 0.13 768 | 9.90 768 9.90 759 | 9 | 57 56 | | |
| | | 3.70 331 | 18 | 9.00 232 | 27 | 0.13 700 | 9.90 7.09 | 9 | 30 | | |
| | 5 | 9.77 009 | 17 | 9.86 259 | 26 | 0.13 741 | 9.90 750 | 9 | 55 | | |
| | 6 | 9.77 026 | 17 | 9.86 285 | 27 | 0.13 715 | 9.90 741 | 10 | 54 | | |
| | 7 | 9.77 043 | 18 | 9.86 312 | 26 | 0.13 688 | 9.90 731 | 9 | 53 | | |
| | 8 9 | 9.77 061 9.77 078 | 17 | 9.86 338 9.86 365 | 27 | 0.13 662 0.13 635 | 9.90 722 9.90 713 | 9 | 52 51 | | |
| | | | 17 | | 27 | | | 9 | - | | |
| | 10 | 9.77 095 | 17 | 9.86 392 | 26 | 0.13 608 | 9.90 704 | 10 | 50 | | |
| | 11 12 | 9.77 112 9.77 130 | 18 | 9.86 418 9.86 445 | 27 | 0.13 582 0.13 555 | 9.90 694 9.90 685 | 9 | 49 48 | | |
| | 13 | 9.77 147 | 17 | 9.86 471 | 26 | 0.13 529 | 9.90 676 | 9 | 47 | ֡ | |
| | 14 | 9.77 164 | 17 | 9.86 498 | 27 | 0.13 502 | 9.90 667 | 9 | 46 | | l |
| | - | | 17 | | 26 | | | 10 | | | |
| | 15 16 | 9.77 181 9.77 199 | 18 | 9.86 524 9.86 551 | 27 | 0.13 476 0.13 449 | 9.90 657 9.90 648 | 9 | 45 44 | | |
| | 17 | 9.77 199 9.77 216 | 17 | 9.86 577 | 26 | 0.13 449 | 9.90 646 | 9 | 43 | | |
| | 18 | 9.77 233 | 17 | 9.86 603 | 26 | 0.13 397 | 9.90 630 | 9 | 42 | | |
| | 19 | 9.77 250 | 17 | 9.86 630 | 27 | 0.13 370 | 9.90 620 | 10 | 41 | | l |
| | 20 | 9.77 268 | 18 | 9.86 656 | 26 | 0.13 344 | 9.90 611 | 9 | 40 | | |
| | 21 | 9.77 285 | 17 | 9.86 683 | 27 | 0.13 344 | 9.90 602 | 9 | 39 | | |
| | 22 | 9.77 302 | 17 | 9.86 709 | 26 | 0.13 291 | 9.90 592 | 10 | 38 | | |
| | 23 | 9.77 319 | 17 | 9.86 736 | 27 | 0.13 264 | 9.90 583 | 9 | 37 | | |
| | 24 | 9.77 336 | 17 17 | 9.86 762 | 26 27 | 0.13 238 | 9.90 574 | 9 | 36 | | l |
| | 25 | 9.77 353 |) ' | 9.86 789 | 1 | 0.13 211 | 9.90 565 | 1 1 | 35 | | ŀ |
| | 26 | 9.77 370 | 17 | 9.86 815 | 26 | 0.13 185 | 9.90 555 | 10 | 34 | | |
| | 27 | 9.77 387 | 17 | 9.86 842 | 27 | 0.13 158 | 9.90 546 | 9 | 33 | | |
| | 28 | 9.77 405 | 18 17 | 9.86 868 | 26 26 | 0.13 132 | 9.90 537 | 10 | 32 | | |
| | 29 | 9.77 422 | 17 | 9.86 894 | 27 | 0.13 106 | 9.90 527 | 9 | 31 | | |
| | 30 | 9.77 439 | 1,, | 9.86 921 | | 0.13 079 | 9.90 518 | ١, ١ | 30 | | 1 |
| | 31 | 9.77 456 | 17 17 | 9.86 947 | 26 27 | 0.13 053 | 9.90 509 | 9 10 | 29 | | |
| | 32 | 9.77 473 | 17 | 9.86 974 | 26 | 0.13 026 | 9.90 499 | ě | 28 | | ŀ |
| | 33 34 | 9.77 490 | 17 | 9.87 000 | 27 | 0.13 000 | 9.90 490 | 10 | 27 26 | | |
| | 34 | 9.77 507 | 17 | 9.87 027 | 26 | 0.12 973 | 9.90 480 | 9 | 20 | | |
| | 35 | 9.77 524 | 17 | 9.87 053 | 26 | 0.12 947 | 9.90 471 | 9 | 25 | | |
| | 36 | 9.77 541 | 17 | 9.87 079 | 27 | 0.12 921 | 9.90 462 | 10 | 24 | | |
| | 37 | 9.77 558 | 17 | 9.87 106 | 26 | 0.12 894 | 9.90 452 | 9 | 23 | | |
| | 38 39 | 9.77 575 9.77 592 | 17 | 9.87 132 9.87 158 | 26 | 0.12 868 0.12 842 | 9.90 443 9.90 434 | 9 | 22 21 | | i |
| | - | | 17 | | 27 | | | 10 | | | ł |
| | 40 | 9.77 609 | 17 | 9.87 185 | 26 | 0.12 815 | 9.90 424 | 9 | 20 | | |
| | 41 42 | 9.77 626 9.77 643 | 17 | 9.87 211 9.87 238 | 27 | 0.12 789 0.12 762 | 9.90 415 9.90 405 | 10 | 19 18 | | |
| | 43 | 9.77 643 9.77 660 | 17 | 9.87 264 | 26 | 0.12 762 | 9.90 405 | 9 | 17 | | Į |
| | 44 | 9.77 677 | 17 | 9.87 290 | 26 | 0.12 710 | 9.90 386 | 10 | 16 | | |
| | 45 | 9.77 694 | 17 | 9.87 317 | 27 | 0.12 683 | 9.90 377 | 9 | 15 | | |
| | 45 46 | 9.77 694 | 17 | 9.87 343 | 26 | 0.12 663 | 9.90 377 | 9 | 14 | | |
| | 47 | 9.77 728 | 17 | 9.87 369 | 26 | 0.12 631 | 9.90 358 | 10 | 13 | | |
| | 48 | 9.77 744 | 16 | 9.87 396 | 27 | 0.12 604 | 9.90 349 | 9 | 12 | | |
| | 49 | 9.77 761 | 17 17 | 9.87 422 | 26 26 | 0.12 578 | 9.90 339 | 10 9 | 11 | | |
| | 50 | 9.77 778 | | 9.87 448 | | 0.12 552 | 9.90 330 | [] | 10 | | |
| | 51 | 9.77 795 | 17 | 9.87 475 | 27 | 0.12 525 | 9.90 320 | 10 | 9 | | |
| | 52 | 9.77 812 | 17 | 9.87 501 | 26 26 | 0.12 499 | 9.90 311 | 9 | 8 | | |
| | 53 | 9.77 829 | 17 17 | 9.87 527 | 26 27 | 0.12 473 | 9.90 301 | 10 9 | 7 | | |
| | 54 | 9.77 846 | 16 | 9.87 554 | 26 | 0.12 446 | 9.90 292 | 10 | 6 | | |
| | 55 | 9.77 862 | | 9.87 580 | | 0.12 420 | 9.90 282 | | 5 | | |
| | 56 | 9.77 879 | 17 17 | 9.87 606 | 26 27 | 0.12 394 | 9.90 273 | 9 10 | 4 | | |
| | 57 | 9.77 896 | 17 | 9.87 633 | 26 | 0.12 367 | 9.90 263 | 9 | 3 | | |
| | 58 59 | 9.77 913 | 17 | 9.87 659 | 26 | 0.12 341 | 9.90 254 | 10 | 2 | | |
| | | 9.77 930 | 16 | 9.87 685 | 26 | 0.12 315 | 9.90 244 | 9 | 1 | | l |
| | 60 | 9.77 946 | | 9.87 711 | | 0.12 289 | 9.90 235 | | ٥ | | <u></u> |
| | | L SIN | D | L TAN | CD | L COT | L COS | ٥ | | | 32: |
| | 1 | L COS | | L COT | | L TAN | L SIN | | | | 233 |
| | l | l I | l i | J | | | J | | | | l |

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|----------|-------------|----------------------|----------|--------------------------------------|-----------------|----------------------|----------------------|----------|----------|---|----|
| 37°217° | | L SIN | _ ' | L TAN | | L COT | L COS | | | | |
| 127°307° | | L COS | D | L COT | CD | L TAN | L SIN | 1 | | | |
| 127507 | | 1003 | | 2001 | | LIAN | L 3114 | _ | | ı | |
| | 0 | 9.77 946 | ., | 9.87 711 | 27 | 0.12 289 | 9.90 235 | ١,, ا | 60 | | |
| | 1 | 9.77 963 | 17 17 | 9.87 738 | 27 26 | 0.12 262 | 9.90 225 | 10 9 | 59 | | |
| | 2 | 9.77 980 | 17 | 9.87 764 | 26 | 0.12 236 | 9.90 216 | 10 | 58 | I | İ |
| | 3 4 | 9.77 997 9.78 013 | 16 | 9.87 7 90 9.87 8 17 | 27 | 0.12 210 0.12 183 | 9.90 206 | 9 | 57 56 | | |
| | | 9.76 013 | 17 | 9.07 617 | 26 | 0.12 163 | 9.90 197 | 10 | 36 | | |
| | 5 | 9.78 030 | 17 | 9.87 843 | 26 | 0.12 157 | 9.90 187 | 9 | 55 | | |
| | 6 | 9.78 047 | 16 | 9.87 869 | 26 | 0.12 131 | 9.90 178 | 10 | 54 | | |
| | 7 8 | 9.78 063 | 17 | 9.87 8 95 9.87 92 2 | 27 | 0.12 105 0.12 078 | 9.90 168 | 9 | 53 | | |
| | ů | 9.78 080 9.78 097 | 17 | 9.87 9 22 9.87 9 48 | 26 | 0.12 078 | 9.90 159 9.90 149 | 10 | 52 51 | | |
| | | - | 16 | | 26 | | | 10 | | | ŀ |
| | 10 11 | 9.78 113 | 17 | 9.87 974 | 26 | 0.12 026 | 0.90 139 | 9 | 50 | | |
| | 12 | 9.78 130 9.78 147 | 17 | 9.88 000 9.88 027 | 27 | 0.12 000 0.11 973 | 9.90 130 9.90 120 | 10 | 49 48 | | l |
| | 13 | 9.78 163 | 16 | 9.88 053 | 26 | 0.11 947 | 9.90 111 | 9 | 47 | | i |
| | 14 | 9.78 180 | 17 | 9.88 079 | 26 | 0.11 921 | 9.90 101 | 10 | 46 | | l |
| | 15 | 9.78 197 | 17 | 9.88 105 | 26 | 0.11 895 | 9.90 091 | 10 | 45 | | |
| | 16 | 9.78 213 | 16 | 9.88 131 | 26 | 0.11 869 | 9.90 082 | 9 | 44 | | ļ |
| | 17 | 9.78 230 | 17 | 9.88 158 | 27 | 0.11 842 | 9.90 072 | 10 | 43 | | |
| | 18 | 9.78 246 | 16 17 | 9.88 184 | 26 26 | 0.11 816 | 9.90 063 | 9 10 | 42 | | |
| | 19 | 9.78 263 | 17 | 9.88 210 | 26 26 | 0.11 790 | 9.90 053 | 10 | 41 | | |
| | 20 | 9.78 280 | | 9.88 236 | | 0.11 764 | 9.90 043 | 1 | 40 | | |
| | 21 | 9.78 296 | 16 | 9.88 262 | 26 | 0.11 738 | 9.90 034 | 9 | 39 | | |
| | 22 | 9.78 313 | 17 16 | 9.88 289 | 27 26 | 0.11 711 | 9.90 024 | 10 10 | 38 | | |
| | 23 | 9.78 329 | 17 | 9.88 315 | 26 | 0.11 685 | 9.90 014 | 9 | 37 | | |
| | 24 | 9.78 346 | 16 | 9.88 341 | 26 | 0.11 659 | 9.90 005 | 10 | 36 | | Į |
| | 25 | 9.78 362 | ,, | 9.88 367 | 200 | 0.11 633 | 9.89 995 | ١., | 35 | | l |
| | 26 | 9.78 379 | 17 16 | 9.88 393 | 26 27 | 0.11 607 | 9.89 985 | 10 9 | 34 | | i |
| | 27 28 | 9.78 395 | 17 | 9.88 420 | 26 | 0.22 580 | 9.89 976 | 10 | 33 | | l |
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| | 30 | 9.78 445 | 16 | 9.88 498 | 26 | 0.11 502 | 9.89 947 | 10 | 30 | | ı |
| | 31 32 | 9.78 461 9.78 478 | 17 | 9.88 524 9.88 550 | 26 | 0.11 476 0.11 450 | 9.89 937 9.89 927 | 10 | 29 28 | | • |
| | 33 | 9.78 494 | 16 | 9.88 577 | 27 | 0.11 430 | 9.89 918 | 9 | 27 | | 1 |
| | 34 | 9.78 510 | 16 | 9.88 603 | 26 | 0.11 397 | 9.89 908 | 10 | 26 | | |
| | 35 | 9.78 527 | 17 | 9.88 629 | 26 | 0.11.271 | 0.90.908 | 10 | 25 | | ı |
| | 36 | 9.78 543 | 16 | 9.88 655 | 26 | 0.11 371 0.11 345 | 9.89 898 9.89 888 | 10 | 25 24 | | l |
| | 37 | 9.78 560 | 17 | 9.88 681 | 26 | 0.11 319 | 9.89 879 | 9 | 23 | | |
| | 38 | 9.78 576 | 16 | 9.88 707 | 26 | 0.11 293 | 0.89 869 | 10 | 22 | | |
| | 39 | 9.78 592 | 16 17 | 9.88 733 | 26 26 | 0.11 267 | 9.89 859 | 10 10 | 21 | | |
| | 40 | 9.78 609 | '' | 9.88 759 | 1 ²⁰ | 0.11 241 | 9.89 849 | 1'' ' | 20 | | 1 |
| | 41 | 9.78 625 | 16 | 9.88 786 | 27 | 0.11 214 | 9.89 840 | 9 | 19 | | |
| | 42 | 9.78 642 | 17 | 9.88 812 | 26 | 0.11 188 | 9.89 830 | 10 | 18 | | |
| | 43 | 9.78 658 | 16 16 | 9.88 838 | 26 26 | 0.11 162 | 9.89 820 | 10 10 | 17 | | |
| | 44 | 9.78 674 | 17 | 9.88 864 | 26 | 0.11 136 | 9.89 810 | 9 | 16 | | |
| | 45 | 9.78 691 | 16 | 9.88 890 | 26 | 0.11 110 | 9.89 801 | 10 | 15 | | |
| | 46 | 9.78 707 | 16 | 9.88 916 | 26 | 0.11 084 | 9.89 791 | 10 10 | 14 | | |
| | 47 48 | 9.78 723 9.78 739 | 16 | 9.88 942 | 26 | 0.11 058 | 9.89 781 | 10 | 13 | | |
| | 48 49 | 9.78 739 9.78 756 | 17 | 9.88 968 9.88 994 | 26 | 0.11 032 0.11 006 | 9.89 771 0.89 761 | 10 | 12 11 | | |
| | \vdash | | 16 | -11 | 26 | | | 9 | | | |
| | 50 | 9.78 772 | 16 | 0.89 020 | 26 | 0.10 980 | 9.89 752 | 10 | 10 | | |
| | 51 52 | 9.78 788 9.78 805 | 17 | 9.89 046 9.89 073 | 27 | 0.10 954 0.10 927 | 9.89 742 | 10 | 9 | | |
| | 52 53 | 9.78 821 | 16 | 9.89 073 | 26 | 0.10 927 | 9.89 732 9.89 722 | 10 | 8 7 | | |
| | 54 | 9.78 837 | 16 | 9.89 125 | 26 | 0.10 875 | 9.89 712 | 10 | 6 | | |
| | | | 16 | | 26 | | | 10 | | | |
| | 55 56 | 9.78 853 9.78 869 | 16 | 9.89 151 9.89 177 | 26 | 0.10 849 0.10 823 | 9.89 702 9.89 693 | 9 | 5 4 | | |
| | 57 | 9.78 886 | 17 | 9.89 203 | 26 | 0.10 523 | 9.89 683 | 10 | 3 | | |
| | 58 | 9.78 902 | 16 | 9.89 229 | 26 | 0.10 771 | 0.89 673 | 10 | 2 | | |
| | 59 | 9.78 918 | 16 | 9.89 255 | 26 | 0.10 745 | 9.89 663 | 10 | 1 | | |
| | 60 | 9.78 934 | 16 | 9.89 281 | 26 | 0.10 719 | 9.89 653 | 10 | 0 | | |
| | | L SIN | , | L TAN | 05 | L COT | L COS | _ | | | 3: |
| | | 1 000 | D | LCOT | CD | I TAN | 1 6151 | ¹º∣ | | | 一 |
| | | L COS | | L COT | | L TAN | L SIN | | | | 2: |

| 38°_216° LSNN D LCOT LCOS D LTAN LSNN D | | | | | | - | | | | | • |
|--|----------------------------------|------------------|----------|--|----------|------------|----------|----------|------------|-------------|----------|
| 128° 308° LCOS LCOT LTAN LSIN See Se | 38 ⁰ 218 ⁰ | | L SIN | <u> </u> | L TAN | | L COT | L COS |] , | | |
| 1 | 128°308° | | L COS | | L COT | | L TAN | L SIN | | | |
| 1 | | 0 | 9.78.934 | | 9 89 281 | | 0.10.719 | 9.89.653 | | 60 | : |
| 2 9.78 987 17 18 989 33 28 0.10 647 9.88 953 10 55 9.89 914 10 9.89 914 10 9.8 | | | | | | | | | | | |
| 3 9.76 983 10 9.86 985 20 0.10 615 9.86 9624 10 55 9.86 114 10 55 | | | | | | | | | | | |
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| 6 9.77 031 16 9.88 437 28 0.10 583 9.88 584 10 54 10 59 9.79 079 079 16 0.08 400 28 0.10 511 9.88 515 10 10 10 9.79 079 16 0.08 516 10 0.08 541 10 11 9.79 111 1 77 9.89 593 26 0.10 457 9.88 514 10 51 12 9.79 144 10 9.88 517 9.88 584 10 12 12 9.79 144 10 9.88 517 9.88 584 10 14 47 9.79 140 16 9.88 541 10 1 | | - 5 | 9.79.016 | ۱ '۱ | 0.80.411 | 1 ~ | 0.10.580 | 0 80 604 | 1 '° | 55 | |
| 7 9.79 047 19 9.89 483 28 0.10 537 0.89 584 10 85 10 11 10 .37 79 059 11 9.89 515 28 0.10 485 0.89 584 10 11 9.79 112 17 9.79 128 16 9.89 515 28 0.10 485 0.89 584 10 48 10 48 11 11 9.79 111 11 9.79 112 16 9.89 543 20 0.10 443 9.89 584 10 48 11 4 9.79 160 16 9.89 543 20 0.10 437 9.89 543 10 48 11 4 9.79 160 16 9.89 543 20 0.10 437 9.89 543 10 48 11 4 9.79 160 16 9.89 543 28 0.10 381 9.88 544 10 47 9.89 543 10 48 11 9.89 545 10 51 9.89 543 10 47 9.89 543 10 48 11 9.89 545 10 48 | | | | 16 | | 26 | | | 10 | | |
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| 9 9.75 079 16 9.86 515 26 10 0.10 455 9.88 564 10 51 10 50 11 11 5.79 111 17 5.88 567 26 0.10 457 9.88 554 10 48 9.88 514 10 48 9.88 513 12 9.79 176 16 9.79 176 16 9.79 176 16 9.79 192 16 9.88 587 26 0.10 457 9.88 514 10 48 9.88 514 10 9.88 | | | | | | | | | | | |
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| 28 | | 27 | 9.79 367 | | 9.89 983 | | 0.10 017 | 9.89 385 | | 33 | f |
| 30 | | 28 | 9.79 383 | | 9.90 009 | 1 | 0.09 991 | 9.89 375 | | 32 | |
| 30 | | 29 | 9.79 399 | | 9.90 035 | | 0.09 965 | 9.89 364 | • | 31 | 1 |
| 31 | | 30 | 9.79 415 | " | 9.90.061 | | 0.09.939 | 9 89 354 |] `` | 30 | |
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| 35 9.79 478 16 9.90 190 190 26 0.09 810 9.89 314 10 25 26 0.09 784 9.89 284 10 22 24 38 9.79 542 16 9.90 284 26 0.09 786 9.89 284 10 22 38 9.79 542 16 9.90 284 26 0.09 786 9.89 284 10 22 24 24 24 9.79 605 16 9.90 371 26 0.09 654 9.89 244 11 18 18 18 18 18 18 18 18 18 18 18 18 | | | | | | | | | • | | 1 |
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| | | | L COS | | L COT |] - | L TAN | L SIN |] | | 2310 510 |
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| 39°219° | | L SIN | | L TAN | | L COT | L COS | _ | | 1 | Ì |
|-----------------------------------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|----------|----------|---|----|
| 129 ⁰ 309 ⁰ | | L COS | ╸ | L COT | CD | L TAN | L SIN | P | | | |
| | 0 | 9.79 887 | | 9.90 837 | | 0.09 163 | 9.89 050 | | 60 | 1 | 1 |
| | 1 | 9.79 903 | 16 | 9.90 863 | 26 | 0.09 137 | 9.89 040 | 10 | 59 | | |
| | 2 | 9.79 918 | 15 | 9.90 889 | 26 | 0.09 111 | 9.89 030 | 10 | 58 | | |
| | 3 | 9.79 934 | 16 | 9.90 914 | 25 | 0.09 086 | 9.89 020 | 10 | 57 | | |
| | 4 | 9.79 950 | 16 | 9.90 940 | 26 | 0.09 060 | 9.89 009 | 11 | 56 | | |
| | 5 | 9.79 965 | 15 | 9.90 966 | 26 | 0.00.004 | 0.00.000 | 10 | | 1 | |
| | 6 | 9.79 981 | 16 | 9.90 966 | 26 | 0.09 034 0.09 008 | 9.88 999 | 10 | 55 | ı | |
| | 7 | 9.79 996 | 15 | 9.91 018 | 26 | 0.08 982 | 9.88 989 9.88 978 | 11 | 54 53 | ı | |
| | 8 | 9.80 012 | 16 | 9.91 043 | 25 | 0.08 957 | 9.88 968 | 10 | 52 | | |
| | 9 | 9.80 027 | 15 | 9.91 069 | 26 | 0.08 931 | 9.88 958 | 10 | 51 | | |
| | 10 | 9.80 043 | 16 | 9.91 095 | 26 | 0.08 905 | 0.00.040 | 10 | | - | |
| | 11 | 9.80 058 | 15 | 9.91 121 | 26 | 0.08 879 | 9.88 948 9.88 937 | 11 | 50 49 | | |
| | 12 | 9.80 074 | 16 | 9.91 147 | 26 | 0.08 853 | 9.88 927 | 10 | 48 | | |
| | 13 | 9.80 089 | 15 | 9.91 172 | 25 | 0.08 828 | 9.88 917 | 10 | 47 | | |
| | 14 | 9.80 105 | 16 | 9.91 198 | 26 | 0.08 802 | 9.88 906 | 11 | 46 | | |
| | 15 | 9.80 120 | 15 | 9.91 224 | 26 | 0.00 770 | | 10 | | • | |
| | 16 | 9.80 120 9.80 136 | 16 | 9.91 224 | 26 | 0.08 776 0.08 750 | 9.88 896 9.88 886 | 10 | 45 44 | | |
| | 17 | 9.80 151 | 15 | 9.91 276 | 26 | 0.08 750 | 9.88 875 | 11 | 43 | | |
| | 18 | 9.80 166 | 15 | 9.91 301 | 25 | 0.08 699 | 9.88 865 | 10 | 42 | | |
| | 19 | 9.80 182 | 16 | 9.91 327 | 26 | 0.08 673 | 9.88 855 | 10 | 41 | | |
| | 30 | 9.80 197 | 15 | | 26 | | | 11 | | | |
| | 20 21 | 9.80 197 9.80 213 | 16 | 9.91 353 9.91 379 | 26 | 0.08 647 0.08 621 | 9.88 844 9.88 834 | 10 | 40 | | |
| | 22 | 9.80 228 | 15 | 9.91 404 | 25 | 0.08 596 | 9.88 834 9.88 824 | 10 | 39 38 | | |
| | 23 | 9.80 244 | 16 | 9.91 430 | 26 | 0.08 570 | 9.88 813 | 11 | 37 | | |
| | 24 | 9.80 259 | 15 | 9.91 456 | 26 | 0.08 544 | 9.88 803 | 10 | 36 | | |
| | 25 | 9.80 274 | 15 | 9.91 482 | 26 | 0.08 518 | | 10 | | | |
| | 26 | 9.80 290 | 16 | 9.91 482 | 25 | 0.08 518 | 9.88 793 9.88 782 | 11 | 35 | | |
| | 27 | 9.80 305 | 15 | 9.91 533 | 26 | 0.08 467 | 9.88 772 | 10 | 34 33 | | |
| | 28 | 9.80 320 | 15 | 9.91 559 | 26 | 0.08 441 | 9.88 761 | 11 | 32 | | |
| | 29 | 9.80 336 | 16 | 9.91 585 | 26 | 0.08 415 | 9.88 751 | 10 | 31 | | |
| | 30 | 9.80 351 | 15 | 9.91 610 | 25 | 0.00.000 | | 10 | _ | | |
| | 31 | 9.80 366 | 15 | 9.91 636 | 26 | 0.08 390 0.08 364 | 9.88 741 9.88 730 | 11 | 30 | | |
| | 32 | 9.80 382 | 16 | 9.91 662 | 26 | 0.08 338 | 9.88 720 | 10 | 29 28 | ı | |
| | 33 | 9.80 397 | 15 | 9.91 688 | 26 | 0.08 312 | 9.88 709 | 11 | 27 | | İ |
| | 34 | 9.80 412 | 15 | 9.91 713 | 25 | 0.08 287 | 9.88 699 | 10 | 26 | | |
| | 35 | 9.80 428 | 16 | 9.91 739 | 26 | 0.08 261 | 0.00.000 | 11 | 75 | 1 | |
| | 36 | 9.80 443 | 15 | 9.91 765 | 26 | 0.08 281 | 9.88 688 9.88 678 | 10 | 25 24 | | |
| | 37 | 9.80 458 | 15 | 9.91 791 | 26 | 0.08 209 | 9.88 668 | 10 | 23 | | |
| | 38 | 9.80 473 | 15 | 9.91 816 | 25 | 0.08 184 | 9.88 657 | 11 | 22 | į | |
| | 39 | 9.80 489 | 16 | 9.91 842 | 26 | 0.08 158 | 9.88 647 | 10 | 21 | i | |
| | 40 | 9.80 504 | 15 | 9.91 868 | 26 | 0.08 132 | 9.88 636 | 11 | 20 | ł | |
| | 41 | 9.80 519 | 15 | 9.91 893 | 25 | 0.08 107 | 9.88 626 | 10 | 19 | | |
| | 42 | 9.80 534 | 15 | 9.91 919 | 26 | 0.08 081 | 9.88 615 | 11 | 18 | | |
| | 43 | 9.80 550 | 16 15 | 9.91 945 | 26 | 0.08 055 | 9.88 605 | 10 | 17 | | |
| | 44 | 9.80 565 | 15 | 9.91 971 | 26 25 | 0.08 029 | 9.88 594 | 11 10 | 16 | | |
| | 45 | 9.80 580 | | 9.91 996 | | 0.08 004 | 9.88 584 | | 15 | ١ | |
| | 46 | 9.80 595 | 15 15 | 9.92 022 | 26 | 0.07 978 | 9.88 573 | 11 | 14 | 1 | |
| | 47 | 9.80 610 | 15 15 | 9.92 048 | 26 | 0.07 952 | 9.88 563 | 10 | 13 | ١ | |
| | 48 | 9.80 625 | 15 16 | 9.92 073 | 25 26 | 0.07 927 | 9.88 552 | 11 10 | 12 | ١ | |
| | 49 | 9.80 641 | 15 | 9.92 099 | 26 | 0.07 901 | 9.88 542 | 11 | 11 | J | |
| | 50 | 9.80 656 | | 9.92 125 | | 0.07 875 | 9.88 531 | | 10 | ١ | |
| | 51 | 9.80 671 | 15 16 | 9.92 150 | 25 | 0.07 850 | 9.88 521 | 10 | 9 | ļ | |
| | 52 | 9.80 686 | 15 15 | 9.92 176 | 26 26 | 0.07 824 | 9.88 510 | 11 | 8 | ١ | |
| | 53 | 9.80 701 | 15 | 9.92 202 | 26 25 | 0.07 798 | 9.88 499 | 11 10 | 7 | ĺ | |
| | 54 | 9.80 716 | 15 | 9.92 227 | 26 | 0.07 773 | 9.88 489 | 11 | 6 | ĺ | 1 |
| | 55 | 9.80 731 | | 9.92 253 | | 0.07 747 | 9.88 478 | | 5 | ĺ | |
| | 56 | 9.80 746 | 15 16 | 9.92 279 | 26 25 | 0.07 721 | 9.88 468 | 10 | 4 | ĺ | |
| | 57 | 9.80 762 | 15 | 9.92 304 | 25 26 | 0.07 696 | 9.88 457 | 11 | 3 | ļ | |
| | 58 | 9.80 777 | 15 | 9.92 330 | 26 | 0.07 670 | 9.88 447 | 10 11 | 2 | ı | ŀ |
| | 59 | 9.80 792 | 15 | 9.92 356 | 25 | 0.07 644 | 9.88 436 | 11 | 1 | ı | |
| | 60 | 9.80 807 | | 9.92 381 | | 0.07 619 | 9.88 425 | | 0 | | |
| | | L SIN | D | L TAN | CD | L COT | L COS | D | | ı | 32 |
| | | L COS | | L COT | | L TAN | L SIN | | | l | 23 |
| | | | | | | | | | | ۱ | |

| | | | | | | | | | _ | 1 |
|----------|----------|----------------------|----------|--|----------|----------------------|----------------------|----------|----------|----------------|
| 40°220° | | L SIN | D | L TAN | CD | L COT | L COS | D | | |
| 130°310° | | LCOS | | LCOT | | L TAN | L SIN | | | |
| | 0 | 9.80 807 | 45 | 9.92 381 | 20 | 0.07 619 | 9.88 425 | 10 | 60 | |
| | 1 1 | 9.80 822 | 15 15 | 9.92 407 | 26 26 | 0.07 593 | 9.88 415 | 11 | 59 | |
| | 2 | 9.80 837 | 15 | 9.92 433 | 25 | 0.07 567 | 9.88 404 | 10 | 58 | |
| | 3 4 | 9.80 852 9.80 867 | 15 | 9.92 458 9.92 484 | 26 | 0.07 542 0.07 516 | 9.88 394 9.88 383 | 11 | 57 56 | |
| | 5 | 9.80 882 | 15 | 9.92 510 | 26 | 0.07 490 | 9.88 372 | 11 | 55 | |
| | 6 | 9.80 897 | 15 | 9.92 535 | 25 | 0.07 465 | 9.88 362 | 10 | 54 | |
| | 7 | 9.80 912 | 15 | 9.92 561 | 26 | 0.07 439 | 9.88 351 | 11 | 53 | |
| | 8 | 9.80 927 | 15 15 | 9.92 587 | 26 25 | 0.07 413 | 9.88 340 | 11 10 | 52 | |
| | 9 | 9.80 942 | 15 | 9.92 612 | 26 | 0.07 388 | 9.88 330 | 11 | 51 | |
| | 10 | 9.80 957 | 15 | 9.92 638 | 25 | 0.07 362 | 9.88 319 | 11 | 50 | |
| | 11 | 9.80 972 | 15 | 9.92 663 | 26 | 0.07 337 | 9.88 308 | 10 | 49 | |
| | 12 13 | 9.80 987 9.81 002 | 15 | 9.92 689 9.92 715 | 26 | 0.07 311 0.07 285 | 9.88 298 9.88 287 | 11 | 48 47 | |
| | 14 | 9.81 017 | 15 | 9.92 740 | 25 | 0.07 260 | 9.88 276 | 11 | 46 | |
| | | | 15 | ······································ | 26 | | | 10 | | |
| | 15 16 | 9.81 032 9.81 047 | 15 | 9.92 766 9.92 792 | 26 | 0.07 234 0.07 208 | 9.88 266 9.88 255 | 11 | 45 44 | 1 |
| | 17 | 9.81 061 | 14 | 9.92 817 | 25 | 0.07 208 | 9.88 244 | 11 | 43 | |
| | 18 | 9.81 076 | 15 | 9.92 843 | 26 | 0.07 157 | 9.88 234 | 10 | 42 | |
| | 19 | 9.81 091 | 15 15 | 9.92 868 | 25 26 | 0.07 132 | 9.88 223 | 11 11 | 41 | |
| | 20 | 9.81 106 | | 9.92 894 | i | 0.07 106 | 9.88 212 | l | 40 | |
| | 21 | 9.81 121 | 15 | 9.92 920 | 26 | 0.07 080 | 9.88 201 | 11 | 39 | |
| | 22 | 9.81 136 | 15 15 | 9.92 945 | 25 26 | 0.07 055 | 9.88 191 | 10 11 | 38 | |
| | 23 24 | 9.81 151 | 15 | 9.92 971 | 25 | 0.07 029 | 9.88 180 | 11 | 37 | |
| | <u> </u> | 9.81 166 | 14 | 9.92 996 | 26 | 0.07 004 | 9.88 169 | 11 | 36 | |
| | 25 | 9.81 180 | 15 | 9.93 022 | 26 | 0.06 978 | 9.88 158 | 10 | 35 | |
| | 26 27 | 9.81 195 9.81 210 | 15 | 9.93 048 9.93 073 | 25 | 0.06 952 0.06 927 | 9.88 148 9.88 137 | 11 | 34 33 | |
| | 28 | 9.81 225 | 15 | 9.93 099 | 26 | 0.06 901 | 9.88 126 | 11 | 32 | |
| | 29 | 9.81 240 | 15 | 9.93 124 | 25 | 0.06 876 | 9.88 115 | 11 10 | 31 | |
| | 30 | 9.81 254 | 14 | 9.93 150 | 26 | 0.06 850 | 9.88 105 | l | 30 | |
| | 31 | 9.81 269 | 15 | 9.93 175 | 25 | 0.06 825 | 9.88 094 | 11 | 29 | |
| | 32 | 9.81 284 | 15 15 | 9.93 201 | 26 26 | 0.06 799 | 9.88 083 | 11 11 | 28 | |
| | 33 | 9.81 299 | 15 | 9.93 227 | 25 | 0.06 773 | 9.88 072 | 11 | 27 | |
| | 34 | 9.81 314 | 14 | 9.93 252 | 26 | 0.06 748 | 9.88 061 | 10 | 26 | |
| | 35 | 9.81 328 | 15 | 9.93 278 | 25 | 0.06 722 | 9.88 051 | 11 | 25 | |
| | 36 37 | 9.81 343 9.81 358 | 15 | 9.93 303 9.93 329 | 26 | 0.06 697 0.06 671 | 9.88 040 9.88 029 | 11 | 24 23 | |
| | 38 | 9.81 372 | 14 | 9.93 354 | 25 | 0.06 646 | 9.88 018 | 11 | 22 | |
| | 39 | 9.81 387 | 15 15 | 9.93 380 | 26 | 0.06 620 | 9.88 007 | 11 11 | 21 | |
| | 40 | 9.81 402 | | 9.93 406 | 26 | 0.06 594 | 9.87 996 | l | 20 | |
| | 41 | 9.81 417 | 15 | 9.93 431 | 25 | 0.06 569 | 9.87 985 | 11 | 19 | Ī |
| | 42 | 9.81 431 | 14 15 | 9.93 457 | 26 25 | 0.06 543 | 9.87 975 | 10 11 | 18 | |
| | 43 44 | 9.81 446 | 15 | 9.93 482 | 26 26 | 0.06 518 | 9.87 964 | 11 | 17 | |
| | Η | 9.81 461 | 14 | 9.93 508 | 25 | 0.06 492 | 9.87 953 | 11 | 16 | Ī |
| | 45 46 | 9.81 475 | 15 | 9.93 533 | 26 | 0.06 467 | 9.87 942 | 11 | 15 | |
| | 46 47 | 9.81 490 9.81 505 | 15 | 9.93 559 9.93 584 | 25 | 0.06 441 0.06 416 | 9.87 931 9.87 920 | 11 | 14 13 | |
| | 48 | 9.81 519 | 14 | 9.93 610 | 26 | 0.06 390 | 9.87 909 | 11 | 12 | |
| | 49 | 9.81 534 | 15 15 | 9.93 636 | 26 25 | 0.06 364 | 9.87 898 | 11 | 11 | |
| | 50 | 9.81 549 | | 9.93 661 | | 0.06 339 | 9.87 887 | 1 | 10 | |
| | 51 | 9.81 563 | 14 15 | 9.93 687 | 26 25 | 0.06 313 | 9.87 877 | 10 | 9 | |
| | 52 50 | 9.81 578 | 15 14 | 9.93 712 | 25 26 | 0.06 288 | 9.87 866 | 11 | 8 | |
| | 53 54 | 9.81 592 9.81 607 | 15 | 9.93 738 9.93 763 | 25 | 0.06 262 0.06 237 | 9.87 855 9.87 844 | 11 | 7 6 | |
| | | | 15 | | 26 | | | 11 | | |
| | 55 56 | 9.81 622 | 14 | 9.93 789 | 25 | 0.06 211 | 9.87 833 9.87 822 | 11 | 5 | |
| | 56 57 | 9.81 636 9.81 651 | 15 | 9.93 814 9.93 840 | 26 | 0.06 186 0.06 160 | 9.87 822 9.87 811 | 11 | 4 | |
| | 58 | 9.81 665 | 14 | 9.93 865 | 25 | 0.06 135 | 9.87 800 | 11 | 2 | |
| | 59 | 9.81 680 | 15 14 | 9.93 891 | 26 25 | 0.06 109 | 9.87 789 | 11 | 1 | |
| | 60 | 9.81 694 | | 9.93 916 | | 0.06 084 | 9.87 778 | <u> </u> | 0 | |
| | | L SIN | D | L TAN | CD | L COT | LCOS | D | | 319°139° |
| | | L COS | | L COT | ן יי | L TAN | L SIN | ľ | | 229° 49° |
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|-----------------------------------|-----|----------|----------|----------|-------------|----------|----------|----------|----|-----------------------------------|
| 41°221° | | L SIN | D | L TAN | CD | L COT | L COS | D | • | |
| 131 ⁰ 311 ⁰ | | L COS | | L COT | | L TAN | L SIN | | | 1 |
| | 0 | 9.81 694 | 15 | 9.93 916 | , . | 0.06 084 | 9.87 778 | ۱., | 60 | |
| | 1 | 9.81 709 | 14 | 9.93 942 | 26 25 | 0.06 058 | 9.87 767 | 11 | 59 | |
| | 2 | 9.81 723 | 15 | 9.93 967 | 26 | 0.06 033 | 9.87 756 | 11 | 58 | |
| | 3 | 9.81 738 | 14 | 9.93 993 | 25 | 0.06 007 | 9.87 745 | 11 | 57 | |
| | 4 | 9.81 752 | 15 | 9.94 018 | 26 | 0.05 982 | 9.87 734 | 11 | 56 | ł |
| | 5 | 9.81 767 | | 9.94 044 | i | 0.05 956 | 9.87 723 | l | 55 | |
| | 6 | 9.81 781 | 14 15 | 9.94 069 | 25 | 0.05 931 | 9.87 712 | 11 | 54 | 1 |
| | 7 | 9.81 796 | 14 | 9.94 095 | 26 25 | 0.05 905 | 9.87 701 | 11 | 53 | |
| | 8 | 9.81 810 | 15 | 9.94 120 | 26 | 0.05 880 | 9.87 690 | 11 | 52 | |
| | 9 | 9.81 825 | 14 | 9.94 146 | 25 | 0.05 854 | 9.87 679 | 11 | 51 | |
| | 10 | 9.81 839 | | 9.94 171 | | 0.05 829 | 9.87 668 | l | 50 | |
| | 11 | 9.81 854 | 15 14 | 9.94 197 | 26 25 | 0.05 803 | 9.87 657 | 11 | 49 | |
| | 12 | 9.81 868 | 14 | 9.94 222 | 26 | 0.05 778 | 9.87 646 | 111 | 48 | l |
| | 13 | 9.81 882 | 15 | 9.94 248 | 25 | 0.05 752 | 9.87 635 | 11 | 47 | |
| | 14 | 9.81 897 | 14 | 9.94 273 | 26 | 0.05 727 | 9.87 624 | 11 | 46 | l |
| | 15 | 9.81 911 | 4.5 | 9.94 299 | 25 | 0.05 701 | 9.87 613 | l | 45 | ľ |
| | 16 | 9.81 926 | 15 14 | 9.94 324 | 25 26 | 0.05 676 | 9.87 601 | 12 | 44 | |
| | 17 | 9.81 940 | 15 | 9.94 350 | 26 25 | 0.05 650 | 9.87 590 | 11 11 | 43 | |
| | 18 | 9.81 955 | 14 | 9.94 375 | 26 | 0.04 625 | 9.87 579 | 11 | 42 | |
| | 19 | 9.81 969 | 14 | 9.94 401 | 25 | 0.05 599 | 9.87 568 | 11 | 41 | I |
| | 20 | 9.81 983 | | 9.94 426 | | 0.05 574 | 9.87 557 | i | 40 | I |
| | 21 | 9.81 998 | 15 | 9.94 452 | 26 25 | 0.05 548 | 9.87 546 | 11 | 39 | 1 |
| | 22 | 9.82 012 | 14 | 9.94 477 | 25 26 | 0.05 523 | 9.87 535 | 11 | 38 | ı |
| | 23 | 9.82 026 | 14 15 | 9.94 503 | 26 25 | 0.05 497 | 9.87 524 | 11 | 37 | 1 |
| | 24 | 9.82 041 | 14 | 9.94 528 | 26 | 0.05 472 | 9.87 513 | 12 | 36 | I |
| | 25 | 9.82 055 | | 9.94 554 | } | 0.05 446 | 9.87 501 | l | 35 | 1 |
| | 26 | 9.82 069 | 14 | 9.94 579 | 25 | 0.05 421 | 9.87 490 | 11 | 34 | |
| | 27 | 9.82 084 | 15 14 | 9.94 604 | 25 26 | 0.05 396 | 9.87 479 | 11 | 33 | I |
| | 28 | 9.82 098 | 14 14 | 9.94 630 | 26 25 | 0.05 370 | 9.87 468 | 11 11 | 32 | |
| | 29 | 9.82 112 | 14 | 9.94 655 | 26 | 0.05 345 | 9.87 457 | 11 | 31 | |
| | 30 | 9.82 126 | | 9.94 681 | | 0.05 319 | 9.87 446 | | 30 | • |
| | 31 | 9.82 141 | 15 | 9.94 706 | 25 | 0.05 319 | 9.87 434 | 12 | 29 | |
| | 32 | 9.82 155 | 14 | 9.94 732 | 26 25 | 0.05 268 | 9.87 423 | 11 | 28 | |
| | 33 | 9.82 169 | 14 15 | 9.94 757 | 25 | 0.05 243 | 9.87 412 | 11 | 27 | |
| | 34 | 9.82 184 | 14 | 9.94 783 | 26 25 | 0.05 217 | 9.87 401 | 11 11 | 26 | |
| | 35 | 9.82 198 | ŀ | 9.94 808 | | 0.05 192 | 9.87 390 | | 25 | |
| | 36 | 9.82 212 | 14 | 9.94 834 | 26 | 0.05 166 | 9.87 378 | 12 | 24 | |
| | 37 | 9.82 226 | 14 | 9.94 859 | 25 26 | 0.05 141 | 9.87 367 | 11 | 23 | |
| | 38 | 9.82 240 | 14 15 | 9.94 884 | 25 26 | 0.05 116 | 9.87 356 | 11 11 | 22 | |
| | 39 | 9.82 255 | 14 | 9.94 910 | 25 | 0.05 090 | 9.87 345 | 11 | 21 | |
| | 40 | 9.82 269 | | 9.94 935 | | 0.05 065 | 9.87 324 | | 20 | |
| | 41 | 9.82 283 | 14 | 9.94 961 | 26 | 0.05 039 | 9.87 322 | 12 | 19 | |
| | 42 | 9.82 297 | 14 | 9.94 986 | 25 | 0.05 014 | 9.87 311 | 11 | 18 | |
| | 43 | 9.82 311 | 14 15 | 9.95 012 | 26 25 | 0.04 988 | 9.87 300 | 11 12 | 17 | |
| | 44 | 9.82 326 | 14 | 9.95 037 | 25 25 | 0.04 963 | 9.87 288 | 11 | 16 | |
| | 45 | 9.82 340 | | 9.95 062 | | 0.04 938 | 9.87 277 | | 15 | l |
| | 46 | 9.82 354 | 14 | 9.95 088 | 26 | 0.04 938 | 9.87 266 | 11 | 14 | |
| | 47 | 9.82 368 | 14 | 9.95 113 | 25 | 0.04 887 | 9.87 255 | 11 | 13 | |
| | 48 | 9.82 382 | 14 14 | 9.95 139 | 26 25 | 0.04 861 | 9.87 243 | 12 11 | 12 | ł |
| | 49 | 9.82 396 | 14 | 9.95 164 | 25 26 | 0.04 836 | 9.87 232 | 11 | 11 | |
| | 50 | 9.82 410 | | 9.95 190 | | 0.04 810 | 9.87 221 | | 10 | |
| | 51 | 9.82 424 | 14 | 9.95 215 | 25 | 0.04 785 | 9.87 209 | 12 | 9 | |
| | 52 | 9.82 439 | 15 | 9.95 240 | 25 | 0.04 760 | 9.87 198 | 11 | 8 | |
| | 53 | 9.82 453 | 14 14 | 9.95 266 | 26 25 | 0.04 734 | 9.87 187 | 11 | 7 | |
| | 54 | 9.82 467 | 14 | 9.95 291 | 25 26 | 0.04 709 | 9.87 175 | 12 11 | 6 | |
| | 55 | 9.82 481 | | 9.95 317 | | 0.04 683 | 9.87 164 | '' | 5 | |
| | 56 | 9.82 495 | 14 | 9.95 342 | 25 | 0.04 658 | 9.87 153 | 11 | 4 | |
| | 57 | 9.82 509 | 14 | 9.95 368 | 26 | 0.04 632 | 0.87 141 | 12 | 3 | |
| | 58 | 9.82 523 | 14 | 9.95 393 | 25 26 | 0.04 607 | 9.87 130 | 11 | 2 | |
| | 59 | 9.82 537 | 14 14 | 9.95 418 | 25 26 | 0.04 582 | 9.87 119 | 11 | 1 | |
| | 60 | 9.82 551 | 14 | 9.95 444 | 26 | 0.04 556 | 9.87 107 | 12 | 0 | |
| | | L SIN | | L TAN | | L COT | L COS | | | 318 ⁰ 138 ⁰ |
| | | | D | | CD | | | D | | |
| | | L COS | | L COT | | L TAN | L SIN | | | 228 ⁰ 48 ⁰ |
| | • { | , | | J | | , , | j l | | 1 | I |

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|----------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|----------|----------|-----------------------------------|
| 42°222° | | L SIN | a | L TAN | CD | L COT | L COS | D | | |
| 132°312° | | L COS | | L COT | 00 | L TAN | L SIN | | | |
| | o | 9.82 551 | | 9.95 444 | | 0.04 556 | 9.87 107 | | 60 | |
| | 1 | 9.82 565 | 14 | 9.95 469 | 25 | 0.04 531 | 9.87 096 | 11 | 59 | |
| | 2 | 9.82 579 | 14 | 9.95 495 | 26 | 0.04 505 | 9.87 085 | 11 | 58 | |
| | 3 | 9.82 593 | 14 | 9.95 520 | 25 | 0.04 480 | 9.87 073 | 12 | 57 | |
| | 4 | 9.82 607 | 14 14 | 9.95 545 | 25 26 | 0.04 455 | 9.87 062 | 11 12 | 56 | |
| | 5 | 9.82 621 | '- | 9.95 571 | | 0.04 429 | 9.87 050 | | 55 | |
| | 6 | 9.82 635 | 14 | 9.95 596 | 25 | 0.04 404 | 9.87 039 | 11 | 54 | |
| | 7 | 9.82 649 | 14 | 9.95 622 | 26 | 0.04 378 | 9.87 028 | 11 | 53 | |
| | 8 | 9.82 663 | 14 | 9.95 647 | 25 | 0.04 353 | 9.87 016 | 12 | 52 | |
| | 9 | 9.82 677 | 14 14 | 9.95 672 | 25 26 | 0.04 328 | 9.87 005 | 11 12 | 51 | |
| | 10 | 9.82 691 | i | 9.95 698 | | 0.04 302 | 9.86 993 | | 50 | |
| | 11 | 9.82 705 | 14 | 9.95 723 | 25 | 0.04 277 | 9.86 982 | 11 | 49 | |
| | 12 | 9.82 719 | 14 | 9.95 748 | 25 | 0.04 252 | 9.86 970 | 12 | 48 | |
| | 13 | 9.82 733 | 14 | 9.95 774 | 26 | 0.04 226 | 9.86 959 | 11 | 47 | |
| | 14 | 9.82 747 | 14 14 | 9.95 799 | 25 26 | 0.04 201 | 9.86 947 | 12 11 | 46 | |
| | 15 | 9.82 761 | , '* | 9.95 825 | 1 | 0.04 175 | 9.86 936 | ' | 45 | |
| | 16 | 9.82 775 | 14 | 9.95 850 | 25 | 0.04 150 | 9.86 924 | 12 | 44 | |
| | 17 | 9.82 788 | 13 | 9.95 875 | 25 | 0.04 125 | 9.86 913 | 11 | 43 | |
| | 18 | 9.82 802 | 14 | 9.95 901 | 26 | 0.04 099 | 9.86 902 | 11 | 42 | |
| | 19 | 9.82 816 | 14 | 9.95 926 | 25 | 0.04 074 | 9.86 890 | 12 | 41 | |
| | | 0.80.820 | 14 | 0.05.050 | 26 | 0.04 048 | 0.86.870 | 11 | 40 | |
| | 20 21 | 9.82 830 9.82 844 | 14 | 9.95 952 9.95 977 | 25 | 0.04 048 | 9.86 879 9.86 867 | 12 | 40 39 | |
| | 22 | 9.82 858 | 14 | 9.96 002 | 25 | 0.03 998 | 9.86 855 | 12 | 38 | |
| | 23 | 9.82 872 | 14 | 9.96 028 | 26 | 0.03 972 | 9.86 844 | 11 | 37 | |
| | 24 | 9.82 885 | 13 | 9.96 053 | 25 | 0.03 947 | 9.86 832 | 12 11 | 36 | |
| | 25 | 9.82 899 | 14 | 9.96 078 | 25 | 0.03 922 | 9.86 821 | 1 '' 1 | 35 | |
| | 26 26 | 9.82 913 | 14 | 9.96 104 | 26 | 0.03 822 | 9.86 809 | 12 | 34 | |
| | 27 | 9.82 927 | 14 | 9.96 129 | 25 | 0.03 871 | 9.86 798 | 11 | 33 | |
| | 28 | 9.82 941 | 14 | 9.96 155 | 26 | 0.03 845 | 9.86 786 | 12 | 32 | |
| | 29 | 9.82 955 | 14 13 | 9.96 180 | 25 25 | 0.03 820 | 9.86 775 | 11 12 | 31 | |
| | 30 | 9.82 968 | i | 9.96 205 | | 0.03 795 | 9.86 763 | | 30 | |
| | 31 | 9.82 982 | 14 | 9.96 231 | 26 | 0.03 769 | 9.86 752 | 11 | 29 | |
| | 32 | 9.82 996 | 14 | 9.96 256 | 25 | 0.03 744 | 9.86 740 | 12 | 28 | |
| | 33 | 9.83 010 | 14 | 9.96 281 | 25 | 0.03 719 | 9.86 728 | 12 | 27 | |
| | 34 | 9.83 023 | 13 14 | 9.96 307 | 26 25 | 0.03 693 | 9.86 717 | 11 12 | 26 | |
| | 35 | 9.83 037 | l . | 9.96 332 |] | 0.03 668 | 9.86 705 | 1 | 25 | |
| | 36 | 9.83 051 | 14 | 9.96 357 | 25 | 0.03 643 | 9.86 694 | 11 | 24 | |
| | 37 | 9.83 065 | 14 13 | 9.96 383 | 26 25 | 0.03 617 | 9.86 682 | 12 12 | 23 | |
| | 38 | 9.83 078 | 14 | 9.96 408 | 25 | 0.03 592 | 9.86 670 | 11 | 22 | |
| | 39 | 9.83 092 | 14 | 9.96 433 | 26 | 0.03 567 | 9.86 659 | 12 | 21 | |
| | 40 | 9.83 106 | | 9.96 459 | 25 | 0.03 541 | 9.86 647 | ا ۱ | 20 | |
| | 41 | 9.83 120 | 14 13 | 9.96 484 | 25 26 | 0.03 516 | 9.86 635 | 12 11 | 19 | l |
| | 42 | 9.83 133 | 14 | 9.96 510 | 25 | 0.03 490 | 9.86 624 | 12 | 18 | ı |
| 1 | 43 | 9.83 147 | 14 | 9.96 535 | 25 | 0.03 465 | 9.86 612 | 12 | 17 | I |
| | 44 | 9.83 161 | 13 | 9.96 560 | 26 | 0.03 440 | 9.86 600 | 11 | 16 | |
| | 45 | 9.83 174 | 14 | 9.96 586 | 25 | 0.03 414 | 9.86 589 | 12 | 15 | |
| | 46 | 9.83 188 | 14 | 9.96 611 | 25 | 0.03 389 | 9.86 577 | 12 | 14 | 1 |
| | 47 | 9.83 202 | 13 | 9.96 636 | 26 | 0.03 364 | 9.86 565 | 11 | 13 | I |
| | 48 49 | 9.83 215 9.83 229 | 14 | 9.96 662 9.96 687 | 25 | 0.03 338 0.03 313 | 9.86 554 9.86 542 | 12 | 12 11 | ĺ |
| | | | 13 | | 25 | | | 12 | | |
| | 50 | 9.83 242 | 14 | 9.96 712 | 26 | 0.03 288 | 9.86 530 | 12 | 10 | 1 |
| | 51 52 | 9.83 256 | 14 | 9.96 738 | 25 | 0.03 262 | 9.86 518 | 11 | 9 | ŀ |
| | 52 53 | 9.83 270 9.83 283 | 13 | 9.96 763 9.96 788 | 25 | 0.03 237 0.03 212 | 9.86 507 9.86 495 | 12 | 8 7 | |
| | 53 54 | 9.83 297 | 14 | 9.96 814 | 26 | 0.03 212 | 9.86 483 | 12 | 6 | I |
| | | | 13 | | 25 | | | 11 | | l |
| | 55 56 | 9.83 310 9.83 324 | 14 | 9.96 839 9.96 864 | 25 | 0.03 161 0.03 136 | 9.86 472 9.86 460 | 12 | 5 4 | |
| | 56 57 | 9.83 324 9.83 338 | 14 | 9.96 864 | 26 | 0.03 136 | 9.86 448 | 12 | 3 | ŀ |
| | 58 | 9.83 351 | 13 | 9.96 915 | 25 | 0.03 110 | 9.86 436 | 12 | 2 | I |
| | 59 | 9.83 365 | 14 | 9.96 940 | 25 | 0.03 060 | 9.86 425 | 11 | 1 | I |
| | 60 | 9.83 378 | 13 | 9.96 966 | 26 | 0.03 034 | 9.86.413 | 12 | 0 | 1 |
| | - 80 | 8.03 3/6 | | 9.90 900 | | 0.03 034 | 9.00.413 | | | |
| | | L SIN | D | L TAN | CD | L COT | L COS | D | | 317 ⁰ 137 ⁰ |
| | | L COS | | LCOT |] | L TAN | L SIN | | | 227° 47° |
| | | | | | 1 | | | I | | ŀ |

| | 1 | T | | | · · · · · · · · · · · · · · · · · · · | | | | | 1 |
|----------|--|----------------------|----------|----------------------|---------------------------------------|----------------------|----------------------|-------------|----------|-----------------------------------|
| 43°223° | <u></u> | L SIN | | L TAN | | L COT | L COS | _ | | ł |
| 133°313° | | L COS | D | L COT | CD | L TAN | L SIN | P | | |
| | | | | | | | | | | ł |
| | 0 | 9.83 378 | 14 | 9.96 966 | 25 | 0.03 034 | 9.86 413 | 12 | 60 | |
| | 1 | 9.83 392 | 13 | 9.96 991 | 25 | 0.03 009 | 9.86 401 | 12 | 59 | |
| | 2 | 9.83 405 | 14 | 9.97 016 | 26 | 0.02 984 | 9.86 389 | 12 | 58 | |
| | 3 | 9.83 419 | 13 | 9.97 042 | 25 | 0.02 958 | 9.86 377 | 11 | 57 | |
| | 4 | 9.83 432 | 14 | 9.97 067 | 25 | 0.02 933 | 9.86 366 | 12 | 56 | Į. |
| | 5 | 9.83 446 | ۱., | 9.97 092 | . | 0.02 908 | 9.86 354 | | 55 | |
| | 6 | 9.83 459 | 13 14 | 9.97 118 | 26 25 | 0.02 882 | 9.86 342 | 12 12 | 54 | |
| | 7 | 9.83 473 | 13 | 9.97 143 | 25 | 0.02 857 | 9.86 330 | 12 | 53 | |
| | 8 | 9.83 486 | 14 | 9.97 168 | 25 | 0.02 832 | 9.86 318 | 12 | 52 | |
| | 9 | 9.93 500 | 13 | 9.97 193 | 26 | 0.02 807 | 9.86 306 | 11 | 51 | J |
| | 10 | 9.83 513 | l | 9.97 219 | | 0.02 781 | 9.86 295 | | 50 | |
| | 11 | 9.83 527 | 14 | 9.97 244 | 25 | 0.02 756 | 9.86 283 | 12 | 49 | |
| | 12 、 | 9.83 540 | 13 14 | 9.97 269 | 25 26 | 0.02 731 | 9.86 271 | 12 | 48 | ł |
| | 13 | 9.83 554 | 13 | 9.97 295 | 25 | 0.02 705 | 9.86 259 | 12 12 | 47 | Ī |
| | 14 | 9.83 567 | 14 | 9.95 320 | 25 | 0.02 680 | 9.86 247 | 12 | 46 | |
| | 15 | 9.83 581 | | 9.97 345 | | 0.02 655 | 9.86 235 | | 45 | l |
| | 16 | 9.83 594 | 13 | 9.97 371 | 26 | 0.02 620 | 9.86 223 | 12 | 44 | ı |
| | 17 | 9.83 608 | 14 | 9.97 396 | 25 25 | 0.02 601 | 9.86 211 | 12 | 43 | l |
| | 18 | 9.83 621 | 13 13 | 9.97 421 | 25 26 | 0.02 579 | 9.86 200 | 11 | 42 | i |
| | 19 | 9.83 634 | 13 | 9.97 447 | 26 25 | 0.02 553 | 9.86 188 | 12 12 | 41 | I |
| | 20 | 9.83 648 | | 9.97 472 | | 0.02 528 | 9.86 176 | l | 40 | i |
| | 21 | 9.83 661 | 13 | 9.97 497 | 25 | 0.02 503 | 9.86 164 | 12 | 39 | I |
| | 22 | 9.83 674 | 13 | 9.97 523 | 26 | 0.02 477 | 9.86 152 | 12 | 38 | i |
| | 23 | 9.83 688 | 14 | 9.97 548 | 25 | 0.02 452 | 9.86 140 | 12 | 37 | |
| | 24 | 9.83 701 | 13 14 | 9.97 573 | 25 25 | 0.02 427 | 9.86 128 | 12 12 | 36 | |
| | 25 | 9.83 715 | '- | 9.97 598 | 25 | 0.02 402 | 9.86 116 | '* | 95 | i |
| | 26 | 9.83 728 | 13 | 9.97 624 | 26 | 0.02 402 | 9.86 104 | 12 | 35 34 | |
| | 27 | 9.83 741 | 13 | 9.97 649 | 25 | 0.02 370 | 9.86 092 | 12 | 33 | 1 |
| | 28 | 9.83 755 | 14 | 9.97 674 | 25 | 0.02 326 | 9.86 080 | 12 | 32 | i |
| | 29 | 9.83 768 | 13 | 9.97 700 | 26 | 0.02 300 | 9.86 068 | 12 | 31 | i |
| | 30 | 0.00.701 | 13 | 0.07.705 | 25 | 0.00.075 | | 12 | | i |
| | 30 31 | 9.83 781 9.83 795 | 14 | 9.97 725 9.97 750 | 25 | 0.02 275 0.02 250 | 9.86 056 9.86 044 | 12 | 30 | 1 |
| | 32 | 9.83 808 | 13 | 9.97 776 | 26 | 0.02 230 | 9.86 032 | 12 | 29 28 | 1 |
| | 33 | 9.83 821 | 13 | 9.97 801 | 25 | 0.02 190 | 9.86 020 | 12 | 27 | i |
| | 34 | 9.83 834 | 13 | 9.97 826 | 25 | 0.02 174 | 9.86 008 | 12 | 26 | i |
| | 25 | 9.83 848 | 14 | 0.07.004 | 25 | 0.00.440 | 0.05.000 | 12 | | 1 |
| | 35 36 | 9.83 861 | 13 | 9.97 861 9.97 877 | 26 | 0.02 149 0.02 123 | 9.85 996 9.85 984 | 12 | 25 24 | i |
| | 37 | 9.83 874 | 13 | 9.97 902 | 25 | 0.02 123 | 9.85 972 | 12 | 23 | 1 |
| | 38 | 9.83 887 | 13 | 9.97 927 | 25 | 0.02 030 | 9.85 960 | 12 | 22 | i |
| | 39 | 9.83 901 | 14 | 9.97 953 | 26 | 0.02 047 | 9.85 948 | 12 | 21 | 1 |
| | 40 | 0.00.014 | 13 | | 25 | | | 12 | | i |
| | 40 41 | 9.83 914 | 13 | 9.97 978 | 25 | 0.02 022 | 9.85 936 | 12 | 20 | i |
| | 42 | 9.83 927 9.83 940 | 13 | 9.98 003 9.98 029 | 26 | 0.01 997 0.01 971 | 9.85 924 9.85 912 | 12 | 19 | i |
| | 42 | 9.83 940 9.83 954 | 14 | 9.98 029 9.98 054 | 25 | 0.01 9/1 | 9.85 912 9.85 900 | 12 | 18 17 | i |
| | 44 | 9.83 967 | 13 | 9.98 079 | 25 | 0.01 946 | 9.85 888 | 12 | 16 | i |
| | | | 13 | | 25 | | | 12 | | i |
| | 45 46 | 9.83 980 | 13 | 9.98 104 | 26 | 0.01 896 | 9.85 876 | 12 | 15 | i |
| | 46 47 | 9.83 993 | 13 | 9.98 130 | 25 | 0.01 870 | 9.85 864 | 13 | 14 | i |
| | 47 48 | 9.84 006 9.84 020 | 14 | 9.98 155 9.98 180 | 25 | 0.01 845 0.01 820 | 9.85 851 9.85 839 | 12 | 13 12 | i |
| | 49 | 9.84 033 | 13 | 9.98 206 | 26 | 0.01 820 | 9.85 827 | 12 | 11 | i |
| | | _ | 13 | | 25 | | | 12 | | ı |
| | 50 | 9.84 046 | 13 | 9.96 231 | 25 | 0.01 769 | 9.85 815 | 12 | 10 | i |
| | 51 52 | 9.84 059 | 13 | 9.98 256 | 25 | 0.01 744 | 9.85 803 | 12 | 9 | i |
| | 52 53 | 9.84 072 | 13 | 9.98 281 | 26 | 0.01 719 | 9.85 791 | 12 | 8 | i |
| | 53 54 | 9.83 085 9.84 098 | 13 | 9.98 307 9.98 332 | 25 | 0.01 693 0.01 668 | 9.85 779 | 13 | 7 6 | i |
| | | | 14 | 8.80 JJZ | 25 | 0.01 000 | 9.85 766 | 12 | - | i |
| | 55 | 9.84 112 | 13 | 9.98 357 | 26 | 0.01 643 | 9.85 754 | 12 | 5 | i |
| | 56 | 9.84 125 | 13 | 9.98 383 | 26 25 | 0.01 617 | 9.85 742 | 12 | 4 | i |
| | 57 | 9.84 138 | 13 | 9.98 408 | 25 | 0.01 592 | 9.85 730 | 12 | 3 | i |
| | 58 | 9.84 151 | 13 | 9.98 433 | 25 | 0.01 567 | 9.85 718 | 12 | 2 | i |
| | 59 | 9.84 164 | 13 | 9.98 458 | 26 | 0.01 542 | 9.85 706 | 13 | 1 | i |
| | 60 | 9.84 177 | | 9.98 484 | | 0.01 516 | 9.85 693 | | 0 | |
| | | L SIN | D | L TAN | CD | L COT | L COS | D | | 316 ⁰ 136 ⁰ |
| | 1 | L COS | | L COT | | L TAN | L SIN | | | 226° 46° |
| | | | , | | 1 1 | | | | | |

| 44°224° | | L SIN | D | L TAN | CD | L COT | L COS | D | | |
|----------|----------|----------------------|----------|----------------------|----------|----------------------|----------------------|----------|----------|----------------------------------|
| 134°314° | | L COS | | L COT | | L TAN | L SIN | | | |
| | 0 | 9.84 177 | | 9.98 484 | ĺ | 0.01 516 | 9.85 693 | | 60 | |
| | 1 | 9.84 190 | 13 | 9.98 509 | 25 | 0.01 491 | 9.85 681 | 12 | 59 | |
| | 2 | 9.84 203 | 13 | 9.98 534 | 25 | 0.01 466 | 9.85 669 | 12 | 58 | |
| | 3 | 9.84 216 | 13 | 9.98 560 | 26 | 0.01 440 | 9.85 657 | 12 | 57 | |
| | 4 | 9.84 229 | 13 13 | 9.98 585 | 25 25 | 0.01 415 | 9.85 645 | 12 | 56 | |
| | 5 | 9.84 242 | | 9.98 610 | i l | 0.01 390 | 9.85 632 | | 55 | |
| | 6 | 9.84 255 | 13 | 9.98 635 | 25 | 0.01 365 | 9.85 620 | 12 | 54 | |
| | 7 | 9.84 269 | 14 | 9.98 661 | 26 | 0.01 339 | 9.85 608 | 12 | 53 | |
| | 8 | 9.84 282 | 13 13 | 9.98 686 | 25 25 | 0.01 314 | 9.85 598 | 12 13 | 52 | |
| | 9 | 9.84 295 | 13 | 9.98 711 | 26 | 0.01 289 | 9.85 583 | 12 | 51 | |
| | 10 | 9.84 308 | | 9.98 737 | | 0.01 263 | 9.85 571 | | 50 | |
| | 11 | 9.84 321 | 13 | 9.98 762 | 25 | 0.01 238 | 9.85 559 | 12 | 49 | |
| | 12 | 9.84 334 | 13 | 9.98 787 | 25 | 0.01 213 | 9.85 547 | 12 | 48 | `` |
| | 13 | 9.84 347 | 13 13 | 9.98 812 | 25 26 | 0.01 188 | 9.85 534 | 13 12 | 47 | |
| | 14 | 9.84 360 | 13 | 9.98 838 | 25 | 0.01 162 | 9.85 522 | 12 | 46 | |
| | 15 | 9.84 373 | | 9.98 863 | i I | 0.01 137 | 9.85 510 | | 45 | |
| | 16 | 9.84 385 | 12 | 9.98 888 | 25 | 0.01 112 | 9.85 497 | 13 | 44 | |
| | 17 | 9.84 398 | 13 | 9.98 913 | 25 | 0.01 087 | 9.85 485 | 12 | 43 | |
| | 18 | 9.84 411 | 13 | 9.98 939 | 26 25 | 0.01 061 | 9.85 473 | 12 13 | 42 | |
| | 19 | 9.84 424 | 13 13 | 9.98 964 | 25 25 | 0.01 036 | 9.85 460 | 12 | 41 | |
| | 20 | 9.84 437 | | 9.98 989 | 1 | 0.01 011 | 9.85 448 | | 40 | |
| | 21 | 9.84 450 | 13 | 9.99 015 | 26 | 0.00 985 | 9.85 436 | 12 | 39 | |
| | 22 | 9.84 463 | 13 | 9.99 040 | 25 | 0.00.960 | 9.85 423 | 13 | 38 | |
| | 23 | 9.84 476 | 13 13 | 9.99 065 | 25 25 | 0.00 935 | 9.85 411 | 12 12 | 37 | |
| | 24 | 9.84 489 | 13 | 9.99 090 | 26 | 0.00 910 | 9.85 399 | 13 | 36 | |
| | 25 | 9.84 502 | | 9,99 116 | | 0.00 884 | 9.85 386 | I I | 35 | |
| | 26 | 9.84 515 | 13 | 9.99 141 | 25 | 0.00 859 | 9.85 374 | 12 | 34 | |
| | 27 | 9.84 528 | 13 12 | 9.99 166 | 25 25 | 0.00 834 | 9.85 361 | 13 12 | 33 | |
| | 28 | 9.84 540 | 13 | 9.99 191 | 26 | 0.00 809 | 9.85 349 | 12 | 32 | |
| | 29 | 9.84 553 | 13 | 9.99 217 | 25 | 0.00 783 | 9.85 337 | 13 | 31 | |
| | 30 | 9.84 566 | 13 | 9.99 242 | 25 | 0.00 758 | 9.85 324 | 12 | 30 | |
| | 31 | 9.84 579 | 13 | 9.99 267 | 25 26 | 0.00 733 | 9.85 312 | 13 | 29 | |
| | 32 | 9.84 592 | 13 | 9.99 293 | 25 | 0.00 707 | 9.85 299 | 12 | 28 | |
| | 33 | 9.84 605 | 13 | 9.99 318 | 25 | 0.00 682 | 9.85 287 | 13 | 27 26 | |
| | 34 | 9.84 618 | 12 | 9.99 343 | 25 | 0.00 657 | 9.85 274 | 12 | 20 | |
| | 35 | 9.84 630 | 13 | 9.99 368 | 26 | 0.00 632 | 9.85 262 | 12 | 25 | |
| | 36 | 9.84 643 | 13 | 9.99 394 | 25 | 0.00 606 | 9.85 250 | 13 | 24 | |
| | 37 38 | 9.84 656 | 13 | 9.99 419 | 25 | 0.00 581 0.00 556 | 9.85 237 9.85 225 | 12 | 23 22 | |
| | 39 | 9.84 669 9.84 682 | 13 | 9.99 444 9.99 469 | 25 | 0.00 531 | 9.85 212 | 13 | 21 | |
| | | | 12 | | 26 | | | 12 | | |
| | 40 41 | 9.84 694 9.84 707 | 13 | 9.99 495 9.99 520 | 25 | 0.00 505 0.00 480 | 9.85 200 9.85 187 | 13 | 20 19 | |
| | 41 | 9.84 707 9.84 720 | 13 | 9.99 520 9.99 545 | 25 | 0.00 455 | 9.85 187 9.85 175 | 12 | 18 | |
| | 43 | 9.84 733 | 13 | 9.99 570 | 25 | 0.00 430 | 9.85 162 | 13 | 17 | |
| | 44 | 9.84 745 | 12 | 9.99 596 | 26 25 | 0.00 404 | 9.85 150 | 12 | 16 | |
| | 45 | 9.84 758 | 13 | 9.99 621 | 25 | 0.00 379 | 9.85 137 | 13 | 15 | |
| | 46 | 9.84 771 | 13 | 9.99 646 | 25 | 0.00 354 | 9.85 125 | 12 | 14 | 1 |
| | 47 | 9.84 784 | 13 | 9.99 672 | 26 | 0.00 328 | 9.85 112 | 13 | 13 | |
| | 48 | 9.84 796 | 12 13 | 9.99 697 | 25 25 | 0.00 303 | 9.85 100 | 12 13 | 12 | |
| | 49 | 9.84 809 | 13 | 9.99 722 | 25 25 | 0.00 278 | 9.85 087 | 13 13 | 11 | |
| | 50 | 9.84 822 | 13 | 9.99 747 | 26 | 0.00 253 | 9.85 074 | 12 | 10 | |
| | 51 | 9.84 835 | 13 | 9.99 773 | 26 25 | 0.00 227 | 9.85 062 | 13 | 9 | |
| | 52 | 9.84 847 | 13 | 9.99 798 | 25 | 0.00 202 | 9.85 049 | 12 | 8 | |
| | 53 54 | 9.84 860 9.84 873 | 13 | 9.99 823 9.99 848 | 25 | 0.00 177 0.00 152 | 9.85 037 9.85 024 | 13 | 7 6 | ľ |
| | | | 12 | | 26 | | | 12 | | |
| | 55 56 | 9.84 885 | 13 | 9.99 874 | 25 | 0.00 126 | 9.85 012 | 13 | 5 | |
| | 56 57 | 9.84 898 9.84 911 | 13 | 9.99 899 9.99 924 | 25 | 0.00 101 0.00 076 | 9.84 999 9.84 986 | 13 | 4 | |
| | 57 58 | 9.84 911 | 12 | 9.99 924 | 25 | 0.00 076 | 9.84 986 9.84 974 | 12 | 3 2 | |
| | 59 | 9.84 936 | 13 | 9.99 975 | 26 | 0.00 031 | 9.84 961 | 13 | 1 | |
| | | | 13 | | 25 | | | 12 | | |
| | 60 | 9.84 949 | | 0.00 000 | | 0.00 000 | 9.84 949 | | ٥ | |
| | | L SIN | D | L TAN | CD | L COT | L COS | D | | 315°135° |
| | | r cos | | L COT | [| L TAN | L SIN | | | 225 ⁰ 45 ⁰ |
| | | - | | | | - | - | | | |

APPENDIX B

DEAD-RECKONING ALTITUDE AND AZIMUTH TABLE

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 1 | , l |] , 1 | | . 1 | 1 |
|----|------------------------|------------------------|--------------------------|--------------------------|--------------------------|---------|
| | 0,00. | 0 ₀ 30, | 1 [°] 00' | 1 [°] 30′ | 2 ⁰ 00' | |
| | A B | A B | A B | A B | A B | |
| 0 | 0.0 | 2059161.7 | 1758146.6 | 15820814.9 | 14571826.5 | 30 |
| 1 | 3837300.0 3536270.0 | 2051981.7 2044921.8 | 1754546.7 1750976.8 | 15796715.1 15772815.2 | 14553826.7 14535826.9 | 29 |
| | 3360180.0 | 2037971.8 | 1747427.0 | 15749015.4 | 14517927.1 | |
| 2 | 3235240.0 | 2031131.9 | 1743917.1 | 15725415.6 | 14500027.3 | 28 |
| 3 | 3138330.0 3059150.0 | 2024401.9 2017772.0 | 1740427.2 1736967.3 | 15701915.7 15678415.9 | 14482327.6 14464627.8 | 27 |
| | 2992210.0 | 2011242.1 | 1733527.4 | 15655216.1 | 14447028.0 | |
| 4 | 2934210.0 | 2004802.1 | 1730127.5 | 15632016.2 | 14429528.3 | 26 |
| 5 | 2883060.0 2837300.0 | 1998462.2 1992212.3 | 1726747.6 1723397.8 | 15609016.4 15586116.6 | 14412028.5 14394628.7 | 25 |
| | 2795910.1 | 1986052.3 | 1720067.9 | 15563316.8 | 14377328.9 | |
| 6 | 2758120.1 | 1979982.4 | 1716768.0 | 15540616.9 | 14360029.2 | 24 |
| 7 | 2723360.1 2691180.1 | 1973992.4 1968082.5 | 1713488.1 1710238.2 | 15518017.1 15495617.3 | 14342829.4 14325729.6 | 23 |
| | 2661210.1 | 1962252.6 | 1707008.4 | 15473317.5 | 14308629.9 | |
| 8 | 2633180.1 | 1956502.7 | 1703798.5 | 15451117.6 | 14291630.1 | 22 |
| 9 | 2606850.1 2582030.1 | 1950822.7 1945222.8 | 1700618.6 1697458.7 | 15429017.8 15407018.0 | 14274730.4 14257930.6 | 21 |
| | 2558550.2 | 1939692.9 | 1694328.9 | 15385118.2 | 14241130.8 | |
| 10 | 2536270.2 | 1934222.9 | 1691219.0 | 15363318.4 | 14224331.1 | 20 |
| 11 | 2515080.2 2494880.2 | 1928833.0 1923503.1 | 1688119.1 1685059.3 | 15341718.6 15320118.7 | 14207731.3 14191131.5 | 19 |
| | 2475580.2 | 1918243.2 | 1682009.4 | 15298718.9 | 14174531.8 | |
| 12 | 2457090.3 | 1913033.2 | 1678979.5 | 15277419.1 | 14158132.0 | 18 |
| 13 | 2439360.3 2422330.3 | 1907903.3 1902823.4 | 1675979.7 1672989.8 | 15256119.3 15235019.5 | 14141732.3 14125332.5 | 17 |
| | 2405940.3 | 1897803.5 | 1670029.9 | 15214019.7 | 14109032.8 | |
| 14 | 2390150.4 | 1892833.6 | 16670810.1 | 15193119.9 | 14092833.0 | 16 |
| 15 | 2374910.4 2360180.4 | 1887933.6 1883073.7 | 16641510.2 16612510.3 | 15172220.1 15151520.3 | 14076633.3 14060533.5 | 15 |
| | 2345940.4 | 1878273.8 | 16583610.5 | 15130920.5 | 14044533.7 | |
| 16 | 2332150.5 | 1873533.9 | 16555010.6 | 15110420.6 | 14028534.0 | 14 |
| 17 | 2318790.5 2305830.5 | 1868834.0 1864194.1 | 16526510.8 16498210.9 | 15089920.8 15069621.0 | 14012534.2 13996734.5 | 13 |
| | 2293240.6 | 1859594.1 | 16470111.0 | 15049421.2 | 13980934.7 | |
| 18 | 2281000.6 | 1855054.2 | 16442211.2 | 15029221.4 | 13965135.0 | 12 |
| 19 | 2269100.6 2257520,7 | 1850554.3 1846094.4 | 16414411.3 16386811.5 | 15009221.6 14989221.8 | 13949435.3 13933835.5 | 11 |
| | 2246240.7 | 1841684.5 | 16359411.6 | 14969322.0 | 13918235.8 | |
| 20 | 2235250.7 | 1837324.6 | 16332211.8 | 14949522.2 | 13902736.0 | 10 |
| 21 | 2224520.8 2214060.8 | 1833004.7 1828724.8 | 16305211.9 16278312.1 | 14929922.4 14910322.6 | 13887236.3 13871836.5 | 9 |
| | 2203840.9 | 1824484.9 | 16251612.2 | 14890722.9 | 13856436.8 | |
| 22 | 2193850.9 | 1820295.0 | 16225012.4 | 14871323.1 | 13841137.1 | 8 |
| 23 | 2184090.9 2174551.0 | 1816135.1 1812015.2 | 16198612.5 16172412.7 | 14852023.3 14832723.5 | 13825837.3 13810637.6 | 7 |
| | 2165211.0 | 1807945.3 | 16146312.8 | 14813523.7 | 13795537.9 | |
| 24 | 2156071.1 | 1803905.4 | 16120413.0 | 14794523.9 | 13780438.1 | 6 |
| 25 | 2147111.1 2138341.1 | 1799905.5 1795935.6 | 16094613.1 16069013.3 | 14775524.1 14756624.3 | 13765338.4 13750438.6 | 5 |
| | 2129741.2 | 1792005.7 | 16043513.4 | 14737724.5 | 13735438.9 | |
| 26 | 2121301.2 | 1788105.8 | 16018213.6 | 14719024.7 | 13720539.2 | 4 |
| 27 | 2113031.3 2104911.3 | 1784245.9 1780426.0 | 15993013.8 15968013.9 | 14700324.9 14681725.2 | 13705739.4 13690939.7 | 3 |
| | 2096951.4 | 1776636.1 | 15943114.1 | 14663225.4 | 13676140.0 | <u></u> |
| 28 | 2089121.4 | 1772876.2 | 15918414.2 | 14644825.6 | 13661540.3 | 2 |
| 29 | 2081431.5 2073881.5 | 1769146.3 1765446.4 | 15893814.4 15869314.6 | 14626425.8 14608126.0 | 13646840.5 13632240.8 | 1 |
| | 2066461.6 | 1761786.5 | 15845014.7 | 14589926.2 | 13617741.1 | |
| 30 | 2059161.7 | 1758146.6 | 15820814.9 | 14571826.5 | 13603241.4 | 0 |
| | A B | A B | A B | A B | A B | |
| | 179 ⁰ 30' | 179 ⁰ 00' | 178 ⁰ 30' | 178 ⁰ 00' | 177 ⁰ 30' | |
| | | l l | l l | | l l | I |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 2°30′ | 3°00' | 3°30' | 4°00' | 4°30' | |
|----|--|--|--|---|---|----------|
| | A B | A B | A B | A B | А В | |
| 0 | 13603241.4 13588841.6 13574441.9 | 12812059.6 12800059.9 12788060.2 | 12143281.1 12132981.5 12122681.9 | 115641105.9 115551106.4 115461106.8 | 110536134.1 110455134.6 110375135.1 | 30 29 |
| | 13560042.2 | 12776060.6 | 12112482.2 | 115371107.3 | 110296135.6 | |
| 2 | 13545742.5 13531542.7 | 12764060.9 12752161.2 | 12102182.6 12091983.0 | 115282107.7 115192108.1 | 110216136.1 110136136.6 | 28 |
| 3 | 13517343.0 13503143.3 | 12740361.6 12728461.9 | 12081783.4 12071583.8 | 115103108.6 115014109.0 | 110057137.1 109977137.6 | 27 |
| 4 | 13489043.6 13474943.9 | 12716662.2 12704962.6 | 12061484.2 12051384.6 | 114925109.5 114836109.9 | 109898138.1 109819138.6 | 26 |
| 5 | 13460944.2 13446944.4 | 12693162.9 12681463.3 | 12041285.0 12031185.4 | 114747110.4 114659110.8 | 109740139.1 109662139.6 | 25 |
| 6 | 13433044.7 13419145.0 | 12669763.6 12658163.9 | 12021185.8 12011086.2 | 114571111.3 114483111.7 | 109583140.1 109505140.6 | 24 |
| 7 | 13405245.3 13391445.6 | 12646564.3 12634964.6 | 12001086.6 11991087.0 | 114395112.2 114307112.7 | 109426141.1 109348141.7 | 23 |
| 8 | 13377745.9 13364046.2 | 12623365.0 12611865.3 | 11981187.4 11971187.8 | 114220113.1 114133113.6 | 109270142.2 109192142.7 | 22 |
| 9 | 13350346.5 | 12600365.7 | 11961288.2 | 114045114.0 | 109115143.2 | 21 |
| 10 | 13336746.8 13323147.1 | 12588866.0 12577466.4 | 11951388.6 11941589.0 | 113958114.5 113872114.9 | 109037143.7 108960144.2 | 20 |
| | 13309647.4 | 12566066.7 | 11931689.4 | 113785115.4 | 108882144.7 | |
| 11 | 13296147.6 13282647.9 | 12554667.1 12543367.4 | 11921889.8 11912090.2 | 113699115.9 113612116.3 | 108805145.2 108728145.8 | 19 |
| 12 | 13269248.2 | 12532067.8 | 11902290.6 | 113526116.8 | 108651146.3 | 18 |
| 13 | 13255848.5 13242548.8 | 12520768.1 12509468.5 | 11892591.0 11882791.4 | 113440117.3 113354117.7 | 108574146.8 108498147.3 | 17 |
| | 13229249.1 | 12498268.8 | 11873091.8 | 113269118.2 | 108421147.8 | |
| 14 | 13215949.4 13202749.7 | 12487069.2 12475969.6 | 11863392.3 11853792.7 | 113183118.7 113098119.1 | 108345148.4 108269148.9 | 16 |
| 15 | 13189650.0 13176450.3 | 12464769.9 12453670.3 | 11844093.1 11834493.5 | 113013119.6 112928120.1 | 108193149.4 108117149.9 | 15 |
| 16 | 13163350.7 13150351.0 | 12442570.6 12431571.0 | 11824893.9 11815294.3 | 112843120.5 112759121.0 | 108041150.5 107965151.0 | 14 |
| 17 | 13137351.3 13124351.6 | 12420471.3 12409571.7 | 11805694.7 11796195.2 | 112674121.5 112590121.9 | 107890151.5 107814152.1 | 13 |
| 18 | 13111451.9 | 12398572.1 | 11786695.6 | 112506122.4 | 107739152.6 | 12 |
| 19 | 13098552.2 13085652.5 | 12387572.4 12376672.8 | 11777196.0 11767696.4 | 112422122.9 112338123.4 | 107664153.1 107589153.6 | 11 |
| | 13072852.8 | 12365773.2 | 11758196.9 | 112255123.9 | 107514154.2 | |
| 20 | 13060053.1 13047353.4 | 12354973.5 12344173.9 | 11748797.3 11739397.7 | 112171124.3 112088124.8 | 107439154.7 107364155.2 | 10 |
| 21 | 13034653.7 | 12333274.3 | 11729998.1 | 112005125.3 | 107290155.8 | 9 |
| 22 | 13021954.1 13009354.4 | 12322574.6 12311775.0 | 11720598.5 11711299.0 | 111922125.8 111839126.2 | 107216156.3 107141156.9 | |
| | 12996754.7 | 12301075.4 | 11701899.4 | 111757126.7 | 107067157.4 | |
| 23 | 12984155.0 12971655.3 | 12290375.8 12279676.1 | 11692599.8 116832100.3 | 111674127.2 111592127.7 | 106993157.9 106919158.5 | 7 |
| 24 | 12959155.7 | 12269076.5 | 116739100.7 | 111510128.2 | 106846159.0 | 6 |
| 25 | 12946656.0 12934256.3 | 12258476.9 12247877.3 | 116647101.1 116554101.6 | 111428128.7 111346129.2 | 106772159.6 106698160.1 | 5 |
| | 12921856.6 | 12237277.6 | 116462102.0 | 111264129.7 | 106625160.6 | |
| 26 | 12909556.9 12897257.3 | 12226778.0 12216178.4 | 116370102.4 116278102.9 | 111183130.1 111101130.6 | 106552161.2 106479161.7 | 4 |
| 27 | 12884957.6 12872757.9 | 12205778.8 12195279.2 | 116187103.3 116096103.7 | 111020131.1 110939131.6 | 106406162.3 106333162.8 | 3 |
| 28 | 12860558.2 | 12184879.5 | 116004104.2 | 110858132.1 | 106260163.4 | 2 |
| 29 | 12848358.6 12836258.9 | 12174379.9 12163980.3 | 115913104.6 115823105.0 | 110777,132.6 110696,133.1 | 106187163.9 106115164.5 | 1 |
| | 12824059.2 | 12153680.7 | 115732105.5 | 110616133.6 | 106043165.0 | |
| 30 | 12812059.6 | 12143281.1 | 115641105.9 | 110536134.1 | 105970165.6 | ° |
| | A B | A B | A B | A B | A B | |
| | 177 ⁰ 00' | 176 ⁰ 30' | 176 ⁰ 00' | 175 ⁰ 30' | 175 ⁰ 00' | |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 5°00' | 5 [°] 30′ | 6°00' | 6°30′ | 7°00' | ĺ |
|----|---|---|----------------------------------|----------------------------------|----------------------------------|----|
| | А В | A B | A B | A B | , ос А В | |
| 0 | 105970165.6 105898166.1 | 101843200.4 101777201.0 | 98076239 98017239 | 94614280 94559281 | 91411325 91359326 | 30 |
| 1 | 105826166.7 105754167.2 | 101712201.6 101646202.2 | 97957240 97897241 | 94503281 94448282 | 91308326 91257327 | 29 |
| 2 | 105683167.8 | 101581202.8 | 97837241 | 94393283 | 91205328 | 28 |
| 3 | 105611168.4 105539168.9 105468169.4 | 101516203.5 101451204.1 101386204.7 | 97777242 97717243 97658243 | 94338284 94283284 94228285 | 91154329 91103330 91052330 | 27 |
| 4 | 105397170.0 | 101321205.3 | 97598244 | 94173286 | 91001331 | 26 |
| 5 | 105325170.6 105254171.1 105183171.7 | 101256205.9 101192206.5 101127207.1 | 97539245 97480245 97420246 | 94118287 94063287 94009288 | 90950332 90899333 90848333 | 25 |
| 6 | 105113172.3 | 101063207.8 | 97361247 | 93954289 | 90798334 | 24 |
| 7 | 105042172.8 104971173.4 | 100998208.4 100934209.0 | 97302247 97243248 | 93899289 93845290 | 90747335 90696336 | 23 |
| | 104901174.0 | 100870209.6 | 97184249 | 93790291 | 90646337 | |
| 8 | 104830174.5 104760175.1 | 100806210.3 100742210.9 | 97126249 97067250 | 93736292 93682292 | 90595337 90545338 | 22 |
| 9 | 104690175.7 104620176.2 | 100678211.5 100614212.1 | 97008251 96950251 | 93628293 93573294 | 90494339 90444340 | 21 |
| 10 | 104550176.8 104480177.4 | 100550212.8 100487213.4 | 96891252 96833253 | 93519295 93465295 | 90394341 90344341 | 20 |
| 11 | 104411178.0 | 100423214.0 100360214.6 | 96774253 | 93411296 | 90293342 | 19 |
| 12 | 104341178.5 104272179.1 | 100380214.8 | 96716254 96658255 | 93358297 93304298 | 90243343 | 18 |
| 13 | 104202179.7 104133180.3 | 100233215.9 100170216.5 | 96600255 96542256 | 93250298 93196299 | 90143345 90093345 | 17 |
| | 104133180.8 | 100170217.2 | 96484257 | 93143300 | 90044346 | |
| 14 | 103995181.4 103926182.0 | 100044217.8 99981218.4 | 96426257 96368258 | 93089301 93036301 | 89994347 89944348 | 16 |
| 15 | 103857182.6 | 99918219.1 | 96310259 | 92982302 | 89894349 | 15 |
| 16 | 103788183.2 103720183.7 | 99856219.7 99793220.3 | 96253260 96195260 | 92929303 92876304 | 89845349 89795350 | 14 |
| | 103651184.3 | 99731221.0 | 96138261 | 92823304 | 89746351 | |
| 17 | 103583184.9 103515185.5 | 99668221.6 99606222.3 | 96080262 96023262 | 92769305 92716306 | 89696352 89647353 | 13 |
| 18 | 103447186.1 103379186.7 | 99544222.9 99481223.5 | 95966263 95909264 | 92663307 92610307 | 89597353 89548354 | 12 |
| 19 | 103311187.2 | 99420224.2 | 95851264 | 92558308 | 89499355 | 11 |
| 20 | 103243187.8 103175188.4 | 99357224.8 99296225.5 | 95795265 95737266 | 92505309 93452310 | 89450356 89401357 | 10 |
| | 103107189.0 | 99234226.1 | 95681267 | 92399310 | 89352357 | |
| 21 | 103040189.6 102973190.2 | 99172226.8 99110227.4 | 95624267 95567268 | 92347311 92294312 | 89303358 89254359 | 9 |
| 22 | 102905190.8 | 99049228.1 | 95510269 | 92242313 | 89205360 | 8 |
| 23 | 102838191.4 102771192.0 | 98988228.7 98926229.4 | 95454269 95397270 | 92189313 92137314 | 89156361 89107362 | 7 |
| | 102704192.6 | 98865230.0 | 95341271 | 92085315 | 89059362 | |
| 24 | 102637193.2 102570193.8 | 98804230.7 98743231.3 | 95285271 95228272 | 92032316 91980316 | 89010363 88961364 | 6 |
| 25 | 102504194.4 102437195.0 | 98682232.0 98621232.6 | 95172273 95116274 | 91928317 91876318 | 88913365 88864366 | 5 |
| 26 | 102371195.6 102304196.2 | 98560233.3 98499233.9 | 95060274 95004275 | 91824319 91772319 | 88816366 88767367 | 4 |
| 27 | 102238196.8 | 98439234.6 | 94948276 | 91720320 | 88719368 | 3 |
| 28 | 102172197.4 102106198.0 | 98378235.3 98318235.9 | 94892276 94836277 | 91668321 91617322 | 88671369 88623370 | |
| | 102040198.6 | 98257236.6 | 94781278 | 91565323 | 88574371 | |
| 29 | 101974199.2 101908199.8 | 98197237.2 98137237.9 | 94725279 94670279 | 91514323 91462324 | 88526371 88478372 | 1 |
| 30 | 101843200.4 | 98076238.6 | 94614280 | 91411325 | 88430373 | 0 |
| | A B | А В | А В | A B | А В | |
| | 174 ⁰ 30' | 174 ⁰ 00' | 173 [°] 30' | 173 ⁰ 00' | 172 ⁰ 30' | |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 7 [°] 30' | 8°00' | 8°30′ | 9°00' | 9°30' | 1 |
|------|----------------------|----------------------|-----------------------|----------------------|----------------------|-------------|
| | | | | | | 4 |
| | A B | A B | A B | A B | A B | |
| 0 | 88430373 88382374 | 85644425 85599426 | 83030480 82987481 | 80567538 80527539 | 78239600 78201601 | 30 |
| 1 | 88334375 | 85555426 | 82945482 | 80487540 | 78164602 | 29 |
| | 88286376 | 85510427 | 82903482 | 80447541 | 78126603 | |
| 2 | 88239376 88191377 | 85465428 85420429 | 82861483 82819484 | 80407542 80368543 | 78088604 78051605 | 28 |
| 3 | 88143378 | 85376430 | 82777485 | 80328544 | 78013606 | 27 |
| | 88096379 | 85331431 | 82735486 | 80288545 | 77976607 | <u> </u> |
| 4 | 88048380 88001381 | 85286432 85242433 | 82693487 | 80249546 80209547 | 77938608 77901609 | 26 |
| 5 | 87953381 | 85197434 | 82651488 82609489 | 80170548 | 77863610 | 25 |
| | 87906382 | 85153434 | 82567490 | 80130549 | 77826611 | Ь. |
| 6 | 87858383 | 85108435 | 82526491 | 80091550 | 77788612 | 24 |
| . 7 | 87811384 87764385 | 85064436 85020437 | 82484492 82442493 | 80051551 80012552 | 77751614 77714615 | 23 |
| | 87716386 | 84976438 | 82400494 | 79973553 | 77677616 | |
| 8 | 87669387 | 84931439 | 82359495 | 79933554 | 77639617 | 22 |
| 9 | 87622387 87575388 | 84887440 84843441 | 82317496 82276497 | 79894555 79855556 | 77602618 77565619 | 21 |
| ŭ | 87528389 | 84799442 | 82234498 | 79816557 | 77528620 | l |
| 10 | 87481390 | 84755443 | 82193499 | 79777558 | 77491621 | 20 |
| 11 | 87434391 | 84711444 | 82151500 82110 501 | 79737559 | 77454622 | 19 |
| •• | 87387392 87341392 | 84667444 84623445 | 82110501 82069502 | 79698560 79659561 | 77417623 77380624 | " |
| 12 | 87294393 | 84579446 | 82027503 | 79620562 | 77343625 | 18 |
| 40 | 87247394 | 84535447 | 81986504 | 79581563 | 77306626 | |
| 13 | 87201395 87154396 | 84492448 84448449 | 81945504 81904505 | 79542564 79503565 | 77269627 77232629 | 17 |
| 14 | 87107397 | 84404450 | 81863506 | 79465566 | 77195630 | 16 |
| | 87061398 | 84361451 | 81821507 | 79426567 | 77158631 | |
| 15 | 87015399 86968399 | 84317452 84273453 | 81780508 81739509 | 79387568 79348569 | 77122632 77085633 | 15 |
| 16 | 86922400 | 84230454 | 81698510 | 79309570 | 77048634 | 14 |
| | 86876401 | 84186454 | 81657511 | 79271571 | 77011635 | 1 |
| 17 | 86829402 86783403 | 84143455 84100456 | 81617512 81576513 | 79232573 79193574 | 76975636 76938637 | 13 |
| 18 | 86737404 | 84056457 | 81535514 | 79155575 | 76902638 | 12 |
| | 86691405 | 84013458 | 81494515 | 79116576 | 76865639 | |
| 19 | 86645405 86599406 | 83970459 83927460 | 81453516 81413517 | 79078577 79039578 | 76828641 76792642 | 11 |
| 20 | 86553407 | 83884461 | 81372518 | 79001579 | 76756643 | 10 |
| | 86507408 | 83840462 | 81331519 | 78962580 | 76719644 | " |
| 21 | 86461409 86415410 | 83797463 83754464 | 81291520 81250521 | 78924581 78886582 | 76683645 76646646 | 9 |
| | 86370411 | 83711465 | 81210522 | | 76610647 | 8 |
| 22 | 86324411 | 83668466 | 81169523 | 78847583 78809584 | 76574648 | ľ |
| 23 | 86278412 86233413 | 83626467 | 81129524 | 78771585 | 76537649 | 7 |
| - 24 | | 83583467 | 81088525 | 78733586 | 76501650 | |
| 24 | 86187414 86142415 | 83540468 83497469 | 81048526 81008527 | 78694587 78656588 | 76465652 76429653 | 6 |
| 25 | 86096416 | 83455470 | 80967528 | 78618589 | 76393654 | 5 |
| | 86051417 | 83412471 | 80927529 | 78580590 | 76357655 | |
| 26 | 86006418 85960418 | 83369472 83327473 | 80887530 80847531 | 78542591 78504592 | 76320656 76284657 | 4 |
| 27 | 85915419 | 83284474 | 80807532 | 78466593 | 76248658 | 3 |
| | 85870420 | 83242475 | 80767533 | 78428594 | 76212659 | ↓ |
| 28 | 85825421 85779422 | 83199476 83157477 | 80727534 80687535 | 78390595 78352597 | 76176660 76141661 | 2 |
| 29 | 85734423 | 83114478 | 80647536 | 78315598 | 76105663 | 1 |
| | 85689424 | 83072479 | 80607537 | 78277599 | 76069664 | <u></u> |
| 30 | 85644425 | 83030480 | 80567538 | 78239600 | 76033665 | 0 |
| | А В | А В | A B | A B | A B |] |
| | 172 ⁰ 00' | 171°30' | 171 ⁰ 00' | 170 ⁰ 30' | 170 ⁰ 00' | 1 |
| | 1 | | | | J | ı |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 10°00' | | | | | 1 |
|-----|----------------------|-----------------------|-----------------------|----------------------|-------------------------|---------------|
| | | 10°30' | 11°00' | 11°30' | 12 ^o 00' | 1 |
| | A B | A B | A B | A B | A B | |
| 0 | 76033665 75997666 | 73937733 73903735 | 71940805 71908807 | 70034681 70003882 | 68212960 68182961 | 30 |
| 1 | 75961667 | 73869736 | 71875808 | 69972883 | 68153962 | 29 |
| | 75926668 | 73835737 | 71843809 | 66941885 | 68123964 | |
| 2 | 75890669 75854670 | 73801738 73767739 | 71810810 71778811 | 69910886 69879887 | 68093965 68064966 | 28 |
| 3 | 75819672 | 73733740 | 71746813 | 69849888 | 68034968 | 27 |
| 4 | 75783673 75747674 | 73699742 73665743 | 71713814 71681815 | 69818890 69787891 | 68005969 | 26 |
| - | 75712675 | 73631744 | 71649816 | 69756892 | 67975970 67945972 | 40 |
| 5 | 75676676 75641677 | 73597745 73563746 | 71616818 71584819 | 69725894 69694895 | 67916973 67886974 | 25 |
| 6 | 75605678 | 73530747 | 71552820 | 69664896 | 67857976 | 24 |
| • | 75570679 | 73496749 | 71520821 | 69633897 | 67828977 | - |
| 7 | 75534680 75499682 | 73462750 73429751 | 71488823 71455824 | 69602899 69571900 | 67796978 67769980 | 23 |
| | 75464683 | 73395752 | 71423825 | 69541901 | 67739981 | 22 |
| | 75428684 | 73361753 | 71391826 | 69510903 | 67710982 | l |
| 9 | 75393685 75358686 | 73328755 73294756 | 71359828 71327829 | 69479904 69449905 | 67681984 67651985 | 21 |
| 10 | 75322687 | 73260757 | 71295830 | 69418907 | 67622987 | 20 |
| | 75287688 | 73227758 | 71263831 | 69387908 | 67593988 | • |
| 11 | 75252690 75217691 | 73193759 73160761 | 71231833 71199834 | 69357909 69326910 | 67563989 67534991 | 19 |
| 12 | 75182692 | 73127762 | 71167835 | 69296912 | 67505992 | 18 |
| 13 | 75147693 75112694 | 73093763 73060764 | 71135836 71104838 | 69265913 69235914 | 67476993 | ., |
| ,,, | 75077695 | 73026765 | 71072839 | 69204916 | 67447995 67417996 | 17 |
| 14 | 75042696 | 72993766 | 71040840 | 69174917 | 67388997 | 16 |
| 15 | 75007698 74972699 | 72960768 72926769 | 71008841 70976843 | 69144918 69113920 | 67359999 673301000 | 15 |
| | 74937700 | 72893770 | 70945844 | 69083921 | 673011002 | " |
| 16 | 74902701 | 72860771 | 70913845 | 69053922 | 672721003 | 14 |
| 17 | 74867702 74832703 | 72827772 72794774 | 70881846 70850848 | 69022924 68992925 | 672431004 672141006 | 13 |
| | 74797704 | 72760775 | 70818849 | 68962926 | 671851007 | |
| 18 | 74763706 74728707 | 72727776 72694777 | 70786850 70755851 | 68931928 68901929 | 671561008 671271010 | 12 |
| 19 | 74693708 | 72661779 | 70723853 | 68871930 | 670981011 | 11 |
| | 74659709 | 72628780 | 70692854 | 68841932 | 670691013 | <u> </u> |
| 20 | 74624710 74589711 | 72595781 72562782 | 70660855 70629856 | 68811933 68781934 | 670401014 670111015 | 10 |
| 21 | 74555712 | 72529783 | 70597858 | 68750935 | 669821017 | 9 |
| 22 | 74520714 74486715 | 72496785 | 70566859 | 68720937 | 669531018 | <u> </u> |
| 22 | 74450715 | 72463786 72430787 | 70534860 70503862 | 68690938 68660939 | 669251020 668961021 | 8 |
| 23 | 74417717 74382718 | 72397788 72365 790 | 70471863 70440 864 | 68630941 | 668671022 66838 1024 | 7 |
| 24 | 74348719 | 72365790 72332791 | 70440864 70409865 | 68600942 68570943 | 668381024 668101025 | 6 |
| | 74313721 | 72299792 | 70377867 | 68540945 | 667811026 | l |
| 25 | 74279722 74245723 | 72266793 72234794 | 70346868 70315869 | 68510946 68480947 | 667521028 667241029 | 5 |
| 26 | 74210724 | 72201796 | 70284870 | 68450949 | 666951031 | 4 |
| 27 | 74176725 | 72168797 | 70252872 | 68421950 | 666661032 | |
| 27 | 74142726 74107728 | 72135798 72103799 | 70221873 70190874 | 68391951 68361953 | 666381033 666091035 | 3 |
| 28 | 74073729 | 72070800 | 70159876 | 68331954 | 665801036 | 2 |
| 29 | 74039730 74005731 | 72038802 72005803 | 70128877 70097878 | 68301955 68272957 | 665521038 665231039 | 1 |
| | 73971732 | 71973804 | 70065879 | 68242958 | 664951040 | l ' |
| 30 | 73937733 | 71940805 | 70034881 | 68212960 | 664661042 | 0 |
| | A B | A B | А В | A B | АВ | |
| | 169 [°] 30' | 169°00' | 168 [°] 30' | 168 ⁰ 00' | 167 ⁰ 30' | |
| l | l i | | į | | | J |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| 19 ² -30 | | 1 | · |] | 1 | 1 | 1 |
|---|----|---------------------|---------------------|---------------------|---------------------|---------------------|----------|
| 0 664661042 | | 12 ⁰ 30' | 13 ⁰ 00' | 13 ⁰ 30' | 14 ⁰ 00' | 14 ⁰ 30' | |
| 66498 | | A B | A B | A B | A B | A B | |
| 66409_1045 | 0 | | | | | | 30 |
| 2 683821047 646821130 630761223 615311316 600621412 28 682541050 648551135 630561224 61601317 6007161414 28 682541050 648551136 630541228 614611319 550941416 27 64600113 62261051 64600113 62261227 614551321 5509451416 27 64600113 62261227 614551321 5509451416 27 64600113 622651221 614511319 5509451416 27 64600113 622651221 614511319 5509451417 22 6 64500113 622651221 614511319 5509451419 26 645061141 622651222 614511322 598451419 26 645061141 622651222 614511322 598451419 26 645061141 622651222 615451322 598451419 26 615421057 6446911144 622651223 613031329 5984681425 22 68 61541057 6446911144 622671223 613031329 5984681425 24 680681059 644671414 622811235 613041333 598271424 22 68 600831050 644571414 622811235 613041333 598271426 23 680681059 644571414 622811235 613041333 598271426 23 6806811059 645281151 627631240 612641333 598771432 22 685881050 645281151 627631241 612291335 597781432 22 685881050 645281152 627571244 612041333 597771435 612681340 613041335 697781435 22 685881050 642781155 622691247 611041343 598501445 61041340 61041341 6104 | 1 | | | | | 600911409 | 29 |
| 68324 | | | | · · | | | |
| Separal | 2 | | | | | | 28 |
| 4 662391053 | 3 | 662961050 | 646271136 | 630241226 | 614811319 | 599941416 | 27 |
| 662111054 64561142 629451220 614051324 599211421 5661541057 644911142 629351234 613501325 598961422 25 661541057 626211059 626061050 644941145 628051233 613001330 598241427 626061060 644051149 628151238 613001330 598241427 626061063 64303159 627991240 612541333 597751430 22 660411063 643031150 627991240 612541333 597751430 22 62606 | | | | | | | |
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| 6 6 651261059 6 444641145 528671235 6 13301329 598481425 24 7 869691060 64437147 522411237 61301329 598241425 23 686411063 644351164 528181239 612791322 598201429 23 686411063 644351150 627691241 61291335 59771430 664411063 644351150 627691241 61291335 597731432 22 659851066 643291152 627371243 612041336 597271431 659851069 643291152 627371243 612041338 597731432 21 659851069 643751155 626851246 611541340 598731435 21 659821071 643211157 628291241 611791339 597031435 21 659821071 642211157 628691249 611041343 598301440 5985721071 642211158 628631249 611041343 598301440 598581444 598061073 641941160 628071250 610791344 59806142 19 659781074 641671161 6225811252 610541349 598581445 18 657801074 641671161 6225811252 610541349 598581445 18 657801077 643131164 625531255 610041349 598581445 18 657801079 64086108 625531257 610791349 598581445 18 657801079 64086108 625531257 610791349 598581445 18 657801079 64086108 625531257 610791349 598581445 18 657801079 64086108 625531257 610791349 598581445 18 658681349 640051170 624251261 609041349 598581445 18 65868139 640051170 624251261 609041355 593481447 17 642211261 640581361 640581170 624251261 609041355 593481447 17 642211261 640581361 640581170 624251261 609041365 593481445 18 658681081 6400581170 624251261 609041365 593481445 18 658681361 6400581170 624251261 609041365 593481445 17 658681361 640581170 624251261 609041365 593481445 17 658681361 640581170 624251261 609041365 593481445 17 658681361 640581170 62425 | 5 | 661821056 | 645181142 | | 613801325 | | 25 |
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| 8 660411063 | 0 | | | | | | 24 |
| 8 660131064 643561151 627831241 612291335 597511432 22 958951066 643291152 627371243 612041336 597271434 597271434 6159152 626591067 643021154 62711244 611791338 597271434 21 650281069 642751155 628681246 611541340 596791437 21 650281069 64281157 628681246 611541340 596791437 21 650281067 64281157 628691246 611541340 596791437 22 685721071 642211158 628331249 611041343 596301440 61 61 61 61 61 61 61 61 61 61 61 61 61 | 7 | | | | | | 23 |
| 9 | 8 | | | | | | 22 |
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| 658161074 | 11 | | | | | | 19 |
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| 13 | 12 | | | | | | 18 |
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| 15 65520_1086 63978_1172 624701263 608791357 594141455 15 655921086 639521173 623741264 608551359 593901457 14 655921087 639251175 622481266 608551360 593661459 14 655571089 538981176 623221267 608051362 593421480 17 655091099 638711178 622961269 607801364 593181462 13 654611091 638451179 622711270 607551365 59241464 18 654531093 638181181 622451272 607301367 592701465 12 654251094 637911182 622191274 607061368 592461467 19 653981096 637641184 621941275 608811370 592221469 11 653701097 637381185 621681277 608581370 592221469 11 653701097 637381185 621681277 606581372 591981470 12 653141100 538641184 621171280 606071375 591511472 10 653141100 538641188 621171280 606071375 591511475 9 652691101 636581190 620651283 605571378 591031477 19 652591104 636511191 620651283 605571378 591031477 19 652691104 636051194 620141286 605081381 590051470 635611196 635781196 619891284 605331380 590791479 8 652411100 635511196 619891284 605331380 590791479 8 651761107 635511196 619891288 604831383 500321482 7 651481109 635251196 619891288 604831383 500321482 7 651481109 635251197 619631289 604591385 590081447 64983111 634481200 619121229 604101388 599001487 64983111 633481196 619891289 604591385 590081487 649831112 634721200 619121292 604101388 599001487 649831114 634191203 618611299 603111394 588611490 589371499 5648281120 633131209 619381291 604341386 589801495 590651490 649831112 633471200 619121292 604101388 599001487 649831112 633681206 618101299 603111394 588861495 59066 | 14 | | | | | | 16 |
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| 655371089 638981176 623221267 608051362 593421460 13 | | | | | | | |
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| 23 651761107 651481109 635511196 635251197 619631289 604831383 604591385 590321482 590081484 7 24 651211110 650931112 650931112 650931112 650381114 654451202 618871294 650381114 634491203 618611295 650381114 634191203 618611295 649831117 633661205 648931117 633661206 618101299 64928120 649281120 649281120 633131209 647591301 649281123 649281123 649281123 649281123 649281123 649281123 649281123 649281216 648191123 648461125 648191123 648461125 648191128 648 | 22 | | | | | | 8 |
| 651481109 635251197 619631289 604591385 590081484 24 651211110 634981199 619381291 604341386 589841485 6 650931112 634721200 619121292 604101388 589601487 5 25 650661113 634451202 618871294 603851390 589371489 5 650381114 634191203 618611295 603661391 588131490 5 26 65011116 633921205 618361297 603361393 588891492 4 649831117 633661206 618101299 603111394 588661494 588661494 27 649561119 633401208 617851300 602871396 588421495 3 649281120 633131209 617591301 602621398 588181497 28 649011122 632871211 617341303 602381399 587951499 2 64873123 | 23 | | | | | | 7 |
| 25 650931112 634721200 619121292 604101388 589601487 650661113 634451202 618871294 603851390 589371489 5 650381114 634191203 618611295 603601391 589131490 5 26 650111116 633921205 618361297 603361393 588891492 4 649831117 633961206 618101299 603111394 588681494 588661494 27 649561119 633401208 617851300 602871396 588421495 3 649281120 633131209 617591301 602621398 588181497 28 649011122 632871211 617341303 602381399 587951499 2 648731123 632601212 617091305 602131401 587711500 1 29 648461125 632341214 616581308 601641404 587241504 1 30 64791 | | | | | | | |
| 25 650661113 634451202 618871294 603851390 589371489 5 650381114 634191203 618611295 603601391 589371489 5 26 650111116 633921205 618361297 603361393 588891492 4 649831117 633661206 618101299 603111394 588661494 588661494 27 649561119 633401208 617851300 602871396 588421495 3 649281120 633131209 617591301 602621398 588181497 28 649011122 632871211 617341303 602381399 587951499 2 29 648461125 632601212 617091305 602131401 587711500 1 29 648461126 632341214 616831306 601891403 587481502 1 30 647911128 631811217 616581310 601401406 587001506 <t< th=""><th>24</th><th></th><th></th><th></th><th></th><th></th><th>6</th></t<> | 24 | | | | | | 6 |
| 650381114 634191203 618611295 603601391 589131490 26 650111116 633921205 618361297 603361393 588891492 4 649831117 633661206 618101299 603111394 588661494 588661494 588661494 588661494 588661495 3 649561199 633131209 617851300 602871396 588421495 3 588181497 3 649281120 633131209 617591301 602621398 588181497 2 648731123 632671211 617341303 602381399 587951499 2 648731123 632601212 617091305 602131401 587711500 587141500 587481502 1 648191126 632341214 616831306 601891403 587481502 1 648191216 632081215 616581308 601641404 587241504 3 647911128 631811217 616321310 601401406 587001506 0 0 | 25 | | | | | | 5 |
| 27 649831117 649561119 649281120 633661206 633401208 633131209 617851300 617591301 617591301 602621398 588661494 588421495 588181497 3 28 649011122 648731123 648731123 6486125 6486125 632631214 616831306 648191126 632081215 648191126 632081215 616581308 631811217 616321310 601401406 631811217 616321310 601401406 6387001506 0 587001506 0 30 647911128 631811217 631811217 631811217 631811217 631821310 631811217 631821310 631811310 631401406 631811310 631401406 6387001506 0 0 | | 650381114 | | | | | |
| 27 649561119 633401208 617851300 602871396 588421495 3 28 649011122 632871211 617341303 602381399 587951499 2 648731123 632601212 617091305 602131401 587711500 2 29 648461125 632341214 616831306 601891403 587481502 1 648191126 632081215 616581308 601641404 587241504 30 647911128 631811217 616321310 601401406 587001506 0 A B A B A B A B | 26 | | | | | | 4 |
| 28 649011122 632871211 617341303 602381399 587951499 2 648731123 632601212 617091305 602131401 587711500 2 648461125 632341214 616831306 601891403 587481502 1 648191126 632081215 616581308 601641404 587241504 30 647911128 631811217 616321310 601401406 587001506 0 A B A B A B A B A B A B | 27 | 649561119 | 633401208 | 617851300 | 602871396 | 588421495 | 3 |
| 29 648731123 648461125 648191126 632601212 632341214 632081215 616831306 616581308 602131401 601891403 601641404 587711500 587481502 587241504 30 647911128 631811217 616321310 601401406 601401406 587001506 587001506 0 A B A B A B A B | | | | | | | <u> </u> |
| 29 648461125 648191126 632341214 632081215 616831306 616581308 601891403 601641404 587481502 587241504 1 30 647911128 631811217 616321310 601401406 587001506 0 A B A B A B A B A B | 28 | | | | | | 2 |
| 30 647911128 631811217 616321310 601401406 587001506 0 A B A B A B A B A B A B | 29 | 648461125 | | 616831306 | 601891403 | 587481502 | 1 |
| A B A B A B A B | 30 | | | | | | _ |
| | | | | | | | <u> </u> |
| 107 00 100 30 100 00 100 30 165 00 | | | | | | | |
| | | 107 00 | 100 30 | 160 00 | 100 30 | 105 00 | l |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 15 [°] 00' | 15°30' | 16 ⁰ 00' | 16°30' | 17°00' | 1 |
|----|------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-----|
| | A B | A B | A B | A B | A B | |
| 0 | 587001506 | 573101609 | 559661716 | 546661826 | 534061940 | 30 |
| 1 | 586771507 | 572871611 57265 1612 | 559441718 55933 1719 | 546441828 | 533861942 | 200 |
| • | 586531509 586301511 | 572651612 572421614 | 559221719 559001721 | 546231830 546021832 | 533651944 533441946' | 29 |
| 2 | 586061512 | 572191616 | 558781723 | 545811834 | 533241948 | 28 |
| 3 | 585831514 585591516 | 571961618 571741619 | 558561725 558341727 | 545591836 545381837 | 533031950 532831952 | 27 |
| | 585361517 | 571511621 | 558121728 | 545171839 | 532621954 | |
| 4 | 585121519 584891521 | 571281623 571061625 | 557901730 557681732 | 544961841 544741843 | 532411956 53231 1058 | 26 |
| 5 | 584651523 | 571061625 570831627 | 557461734 | 544741845 544531845 | 532211958 532001960 | 25 |
| | 584421524 | 570601628 | 557251736 | 544321847 | 531801962 | |
| 6 | 584181526 583951528 | 570381630 570151632 | 557031738 556811739 | 544111849 543901851 | 531591964 531391966 | 24 |
| 7 | 583721529 | 569921634 | 556591741 | 543681853 | 531181967 | 23 |
| | 583481531 | 569701935 | 556371743 | 543471854 | 530981969 | |
| 8 | 583251533 583021534 | 569471637 569251639 | 556151745 555931747 | 543261856 543051858 | 530771971 530571973 | 22 |
| 9 | 582781536 582551538 | 569021641 568801642 | 555721749 555501750 | 542841860 542631862 | 530361975 530161977 | 21 |
| 10 | 582321540 | 568571644 | 555281752 | 542421864 | 529951979 | 20 |
| | 582081541 | 568351646 | 555061754 | 542201866 | 529751981 | |
| 11 | 581851543 581621545 | 568121648 567901649 | 554841756 554631758 | 541991868 541781870 | 529541983 529341985 | 19 |
| 12 | 581381546 | 567671651 | 554411760 | 541571871 | 529141987 | 18 |
| 13 | 581151548 580921550 | 567451653 567221655 | 554191761 553971763 | 541361873 541151875 | 528931989 528731991 | 17 |
| | 580691552 | 567001657 | 553761765 | 540941877 | 528521993 | l " |
| 14 | 580461553 | 566771658 | 553541767 | 540731879 | 528321995 | 16 |
| 15 | 580221555 579991557 | 566551660 566321662 | 553321769 553111771 | 540521881 540311883 | 528121997 527911999 | 15 |
| | 579761559 | 566101664 | 552891772 | 540101885 | 527712001 | |
| 16 | 579531560 579301562 | 565881665 565651667 | 552671774 552461776 | 539891887 539681889 | 527512003 527302005 | 14 |
| 17 | 579071564 | 565431669 | 552241778 | 539471890 | 527102007 | 13 |
| 18 | 578841565 578601567 | 565211671 564981673 | 552021780 551811782 | 539261892 539051894 | 526902009 526702010 | 12 |
| | 578371569 | 564761674 | 551591783 | 538841896 | 526492012 | 12 |
| 19 | 578141571 577911572 | 564541676 564311678 | 551381785 551161787 | 538641898 538431900 | 526292014 526092016 | 11 |
| 20 | 577681574 | 564091680 | 550951789 | 538221902 | 525882018 | 10 |
| 21 | 577451576 | 563871682 | 550731791 | 538011904 | 525682020 | _ |
| 21 | 577221578 576991579 | 563651683 563421685 | 550511793 550301795 | 537801906 537591908 | 525482022 525282024 | 9 |
| 22 | 576761581 | 563201687 | 550081796 | 537381910 | 525082026 | 8 |
| 23 | 576531583 576301584 | 562981689 562761691 | 549871798 549651800 | 537181911 536971913 | 524872028 524672030 | 7 |
| | 576071586 | 562541692 | 549441802 | 536761915 | 524472032 | |
| 24 | 575841588 575611590 | 562311694 562091696 | 549221804 | 536551917 536341919 | 524272034 524072036 | 6 |
| 25 | 575381591 | 561871698 | 549011806 548801808 | 536141921 | 523872038 | 5 |
| | 575161593 | 561651700 | 548581809 | 535931923 | 523662040 | |
| 26 | 574931595 574701597 | 561431701 561211703 | 548371811 548151813 | 535721925 535511927 | 523462042 523262044 | 4 |
| 27 | 574471598 574241600 | 560991705 56076 1707 | 547941815 | 535311929 53510 1931 | 523062046 | 3 |
| 28 | 574011602 | 560761707 560541709 | 547731817 547511819 | 535101931 534891933 | 522862048 522662050 | 2 |
| | 573781604 | 560321710 | 547301821 | 534681935 | 522462052 | |
| 29 | 573561605 573331607 | 560101712 559881714 | 547081823 546871824 | 534481936 534271938 | 522262054 522062056 | 1 |
| 30 | 573101609 | 559661716 | 546661826 | 534061940 | 521862058 | 0 |
| | A B | A B | А В | АВ | АВ | |
| | 164 ⁰ 30' | 164 ⁰ 00' | 163 [°] 30′ | 163 ⁰ 00' | 162 ⁰ 30' | |
| | J | l | · | | | J |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 17 ⁰ 30' | 18 ⁰ 00' | 18 ⁰ 30' | 19°00' | 19 ⁰ 30' | 1 |
|-----|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|----------|
| | A B | A B | A B | A B | A B | 1 |
| 0 | 521862058 521662060 | 510022179 509822181 | 498522304 498332306 | 487362433 487172435 | 476502565 476332568 | 30 |
| 1 | 521462062 521262064 | 509632183 509432185 | 498152309 497962311 | 486992437 486812439 | 476152570 475972572 | 29 |
| 2 | 521062066 | 509242188 | 497772313 | 486622442 | 475792574 | 28 |
| 3 | 520862068 520662070 520462072 | 509052190 508852192 508662194 | 497582315 497392317 497202319 | 486442444 486262446 486082448 | 475612576 475442579 475262581 | 27 |
| 4 | 520262074 | 508462196 | 497022321 | 485892450 | 475082583 | 26 |
| 5 | 520062076 519862078 519662080 | 508272198 508082200 507882202 | 496832323 496642325 496452328 | 485712453 485532456 485342457 | 474902585 474722588 474552590 | 25 |
| - 6 | 519462082 | 507692204 | 496262330 | 485162459 | 474372592 | 24 |
| 7 | 519262084 519062086 518862088 | 507502206 507302208 507112210 | 496082332 495892334 495702336 | 484982461 484802463 484622466 | 474192594 474022597 473842599 | 23 |
| 8 | 518672090 | 506922212 | 495512338 | 484432468 | 473662601 | 22 |
| 9 | 518472092 518272094 | 506732214 506532216 | 495332340 495142343 | 484252470 484072472 | 473482603 473312606 | 21 |
| | 518072096 | 506342218 | 494952345 | 483892474 | 473132608 | <u> </u> |
| 10 | 517872098 517672100 | 506152221 505962223 | 494772347 494582349 | 483712477 483522479 | 472952610 472782613 | 20 |
| 11 | 517472102 517282104 | 505762225 505572227 | 494392351 494212353 | 483342481 483162483 | 472602515 472422617 | 19 |
| 12 | 517082106 516882108 | 505382229 505192231 | 494022355 493832357 | 482982485 482802488 | 472252619 472072622 | 18 |
| 13 | 516682110 | 504992233 | 493652360 | 482622490 | 471892624 | 17 |
| 14 | 516492112 516292114 | 504802235 504612237 | 493462362 493272364 | 482442492 482252494 | 471722626 471542628 | 16 |
| 15 | 516092116 515892118 | 504422239 504232241 | 493092366 492902368 | 482072496 481892499 | 471372631 471192633 | 15 |
| | 515702120 | 504042243 | 492712370 | 481712501 | 471012635 | L¨ |
| 16 | 515502122 515302124 | 503852246 503652248 | 492532372 492342375 | 481532503 481352505 | 470842637 470662640 | 14 |
| 17 | 515102126 514912128 | 503462250 503272252 | 492162377 491972379 | 481172507 480992510 | 470492642 470312644 | 13 |
| 18 | 514712130 514512132 | 503082254 502892256 | 491792381 491602383 | 480812512 480632514 | 470142646 469962649 | 12 |
| 19 | 514322134 514122136 | 502702258 502512260 | 491412385 491232387 | 480452516 480272519 | 469782651 469612653 | 11 |
| 20 | 513922138 | 502322262 | 491042390 | 480092521 | 469432656 | 10 |
| 21 | 513732141 513532143 | 502132264 501942266 | 490862392 490672394 | 479912523 479732525 | 469262658 469082660 | 9 |
| | 513342145 | 501752269 | 490492396 | 479552527 | 468912662 | <u> </u> |
| 22 | 513142147 512942149 | 501562271 501372273 | 490302398 490122400 | 479372530 479192532 | 468732665 468562667 | 8 |
| 23 | 512752151 512552153 | 501172275 500982277 | 489932403 489752405 | 479012534 478832536 | 468392669 468212672 | 7 |
| 24 | 512362155 512162157 | 500802279 500612281 | 489572407 | 478652539 47847 2541 | 468042674 | 6 |
| 25 | 511972159 511772161 | 500422283 500232285 | 489382409 489202411 489012413 | 478472541 478292543 478112545 | 467862676 467692678 467512681 | 5 |
| 26 | 511582163 | 500042287 | 488832416 | 477932547 | 467342683 | 4 |
| 27 | 511382165 511192167 | 499852290 499662292 | 488642418 488462420 | 477752550 477582552 | 467162685 466992688 | 3 |
| 28 | 510992169 510802171 | 499472294 499282296 | 488282422 488092424 | 477402554 477222556 | 466822690 466642692 | 2 |
| 29 | 510602173 510412175 | 499092298 498902300 | 487912426 487722429 | 477042559 476862561 | 466472694 466302697 | 1 |
| -53 | 510212177 | 498902302 | 487542431 | 476682563 | 466302697 466122699 | |
| 30 | 510022179 | 498522304 | 487362433 | 476502565 | 465952701 | 0 |
| | A B | A B | A B | A B | A B | |
| | 162 ⁰ 00' | 161 ⁰ 30' | 161 ⁰ 00' | 160°30' | 160 ⁰ 00' | |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 20°00' | | 0 | 21 ⁰ 30' | 22°00' | ł |
|-------------|------------------------|-------------------------|------------------------|------------------------|------------------------|--------------|
| | | 20°30' | 21000 | | | |
| 0 | A B 465952701 | A B 455672841 | A B 445672985 | A B 435923132 | A B 426423283 | 30 |
| | 465772704 | 455512844 | 445512988 | 435763135 | 426273286 | " |
| 1 | 465602706 465432708 | 455342846 455172848 | 445342990 445182992 | 435603137 435443140 | 426113288 425963291 | 29 |
| 2 | 465252711 | 455002851 | 445012994 | 435283142 | 425803294 | 28 |
| 3 | 465082713 464912715 | 454832853 454662855 | 444852997 444682999 | 435123145 | 425643296 | 27 |
| | 464732717 | 454492858 | 444523002 | 434963147 434803150 | 425493299 425333301 | 27 |
| 4 | 464562720 | 454332860 | 444363004 | 434643152 | 425183304 | 26 |
| 5 | 464392722 464222724 | 454162862 453992865 | 444193007 444033009 | 434483155 434323157 | 425023306 424863309 | 25 |
| | 464042727 | 453822867 | 443863012 | 434163160 | 424713312 | |
| 6 | 463872729 463702731 | 453652870 453482872 | 443703014 443543016 | 434003162 433853165 | 424553314 424493317 | 24 |
| 7 | 463532734 | 453322874 | 443373019 | 433693167 | 424243319 | 23 |
| 8 | 463352736 463182738 | 453152877 452982879 | 443213021 443053024 | 433533170 433373172 | 424093322 423933324 | 22 |
| • | 463012741 | 452812881 | 442883026 | 433213175 | 423783327 | 22 |
| 9 | 462842743 462662745 | 452652884 452482886 | 442723029 442563031 | 433053177 432893180 | 423623329 423473332 | 21 |
| 10 | 462492748 | 452312889 | 442393033 | 432733182 | 423313335 | 20 |
| 11 | 462322750 462152752 | 452142891 451982893 | 442233036 442073038 | 432573185 432413187 | 423163337 423003340 | 19 |
| | 461982755 | 451812896 | 441903041 | 432253190 | 422853342 | |
| 12 | 461812757 | 451642898 45147 2001 | 441743043 | 432103192 | 422693345 | 18 |
| 13 | 461632759 461462761 | 451472901 451312903 | 441583046 441423048 | 431943195 431783197 | 422543347 422383350 | 17 |
| | 461292764 | 451142905 | 441253051 | 431623200 | 422233353 | |
| 14 | 461122766 460952768 | 450972908 450812910 | 441093053 440933056 | 431463202 431303205 | 422073355 421923358 | 16 |
| 15 | 460782771 460612773 | 450642913 450472915 | 440773058 440603060 | 431143207 430993210 | 421763360 | 15 |
| 16 | 460432775 | 450312917 | 440443063 | 430833212 | 421613363 421453366 | 14 |
| | 460262778 | 450142920 | 440283065 | 430673215 | 421303368 | |
| 17 | 460092780 459922782 | 449972922 449812924 | 440123068 439953070 | 430513217 430353220 | 421153371 420993373 | 13 |
| 18 | 459752785 | 449642927 | 439793073 | 430203222 | 420843376 | 12 |
| 19 | 459582787 459412789 | 449472929 449312932 | 439633075 439473078 | 430043225 429883227 | 420683379 420533381 | 11 |
| | 459242792 | 449142934 | 439313080 | 429723230 | 420383384 | |
| 20 | 459072794 458902797 | 448982936 448812939 | 439143083 438983085 | 429563233 429413235 | 420223386 420073389 | 10 |
| 21 | 458732799 | 448642941 | 438823088 | 429253238 | 419913391 | 9 |
| | 458562801 | 448482944 | 438663090 | 429093240 | 419763394 | <u> </u> |
| 22 | 458392804 458222806 | 448312946 448152949 | 438503092 438343095 | 428933243 428783245 | 419613387 419453399 | 8 |
| 23 | 458052808 457882811 | 447982951 447822953 | 438183097 438013100 | 428623248 428463250 | 419303402 419153404 | 7 |
| 24 | 457712813 | 447652956 | 437853102 | 428303253 | 418993407 | 6 |
| 25 | 457542815 457372818 | 447482958 | 437693105 | 428153255 | 418843410 | _ |
| | 457202820 | 447322961 447152963 | 437533107 437373110 | 427993258 427833260 | 418693412 418533415 | 5 |
| 26 | 457032822 | 446992965 | 437213112 | 427683263 | 418383418 | 4 |
| 27 | 456862825 456692827 | 446822968 446662970 | 437053115 436893117 | 427523266 427363268 | 418233420 418083423 | 3 |
| | 456522829 | 446492973 | 436733120 | 427213271 | 417923425 | |
| 28 | 456352832 456182834 | 446332975 446162978 | 436573122 436413125 | 427053273 426893276 | 417773428 417623431 | 2 |
| 29 | 456012836 | 446002980 | 436243127 | 426743278 | 417463433 | 1 |
| 30 | 455842839 455672841 | 445832982 445672985 | 439083130 435923132 | 436583281 426423283 | 417313436 | <u> </u> |
| | A B | A B | 435923132 A B | A B | 417163438 A B | - |
| | 159°30' | 159°00' | 158°30′ | 158°00' | 157°30' | l |
| | 132 33 | 139 00 | 150 30 | 158 00 | 15/ 30 | J |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 22°30' | 23°00' | 23°30' | 24°00' | 24 ⁰ 30' | 1 |
|----|------------------------|------------------------|------------------------|------------------------|------------------------|----------|
| | A B | A B | 23 30 A B | A B | A B | ł |
| | 417163438 | | | | | |
| U | 417103441 | 408123597 407973600 | 399303760 399153763 | 390693927 390543930 | 382274098 382134101 | 30 |
| 1 | 416853444 | 407823603 | 399013766 | 390403932 | 382004103 | 29 |
| | 416703446 | 407683605 | 398863768 | 390263935 | 381864106 | Ь |
| 2 | 416553449 416403452 | 407533608 407383611 | 398723771 398573774 | 390123938 389983941 | 381724109 381584112 | 28 |
| 3 | 416253454 | 407233613 | 398433777 | 389843944 | 381444115 | 27 |
| | 416093457 | 407083616 | 398283779 | 389693947 | 381304118 | <u></u> |
| 4 | 415943459 | 406933619 | 398143782 | 389553949 | 381174121 | 26 |
| 5 | 415793462 415643465 | 406783622 406643624 | 397993785 397853788 | 389413952 389273955 | 381034124 380894127 | 25 |
| | 415493467 | 406493627 | 397713790 | 389133958 | 380754129 | |
| 6 | 415333470 | 406343630 | 397563793 | 388993961 | 380614132 | 24 |
| 7 | 415183473 | 406193632 | 397423796 | 388853964 | 380484135 | |
| , | 415033475 414883478 | 406043635 405903638 | 397273799 397133801 | 388713966 388563969 | 380344138 380204141 | 23 |
| 8 | 414733480 | 405753640 | 396983804 | 388423972 | 380064144 | 22 |
| | 414583483 | 405603643 | 396843807 | 388283975 | 379924147 | |
| 9 | 414433486 414273488 | 405453646 405303648 | 396693810 396553813 | 388143978 388003981 | 379794150 379654153 | 21 |
| 10 | 414123491 | 405163651 | 396413815 | 387863983 | 379514155 | 20 |
| .0 | 413973494 | 405013654 | 396263818 | 387723986 | 379374158 | 20 |
| 11 | 413823496 | 404863657 | 396123821 | 387583989 | 379244161 | 19 |
| | 413673499 | 404713659 | 395973824 | 387443992 | 379104164 | <u> </u> |
| 12 | 413523502 413373504 | 404573662 404423665 | 395833826 395693829 | 387303995 387163998 | 378964167 378824170 | 18 |
| 13 | 413223507 | 404273667 | 395543832 | 387024000 | 378694173 | 17 |
| | 413073509 | 404133670 | 395403835 | 386884003 | 378554176 | |
| 14 | 412913512 412763515 | 403983673 403833676 | 395253838 | 386744006 | 378414179 | 16 |
| 15 | 412613517 | 403683678 | 395113840 394973843 | 386604009 386454012 | 378284182 378144185 | 15 |
| | 412463520 | 403543681 | 394823846 | 386314015 | 378004187 | |
| 16 | 412313523 | 403393684 | 394683849 | 386174017 | 377864190 | 14 |
| 17 | 412163525 412013528 | 403243686 403103689 | 394543851 394393854 | 386034020 385894023 | 377734193 377594196 | 13 |
| | 411863531 | 402953692 | 394253857 | 385754026 | 377454199 | |
| 18 | 411713533 | 402803695 | 394113860 | 385614029 | 377324202 | 12 |
| 19 | 411563536 411413539 | 402663697 402513700 | 393963863 393823865 | 385474032 385334035 | 377184235 | ١., |
| ,, | 411263541 | 402363703 | 393683868 | 385204037 | 377044208 376914211 | 11 |
| 20 | 411113544 | 402223705 | 393533871 | 385064040 | 376774214 | 10 |
| | 410963547 | 402073708 | 393393874 | 384924043 | 376634217 | |
| 21 | 410813549 410663552 | 401923711 401783714 | 393253876 393113879 | 384784046 384644049 | 376504220 376364222 | 9 |
| 22 | 410513555 | 401633716 | 392963882 | 384504052 | 376234225 | 8 |
| | 410363557 | 401493719 | 392823885 | 384364055 | 376094228 | |
| 23 | 410213560 410063563 | 401343722 401193725 | 392683888 392543890 | 384224057 384084060 | 375954231 375824234 | 7 |
| 24 | 409913565 | 401053727 | 392393893 | 383944063 | 375684237 | 6 |
| | 409763568 | 400903730 | 392253896 | 383804066 | 375544240 | ľ |
| 25 | 409613571 | 400763733 | 392113899 | 383664069 | 375414243 | 5 |
| | 409463573 | 400613735 | 391973902 | 383524072 | 375274246 | <u> </u> |
| 26 | 409313576 409163579 | 400463738 400323741 | 391823904 391683907 | 383384075 383244078 | 375144249 375004252 | 4 |
| 27 | 409023581 | 400173744 | 391543910 | 383114080 | 374864255 | 3 |
| | 408873584 | 400033746 | 391403913 | 382974083 | 374734258 | |
| 28 | 408723587 408573589 | 399883749 399743752 | 391253916 | 382834086 | 374594261 | 2 |
| 29 | 408423592 | 399743752 399593755 | 391113918 390973921 | 382694089 382554092 | 374464264 374324266 | 1 |
| | 408273595 | 399453757 | 390833924 | 382414095 | 374194269 | , |
| 30 | 408123597 | 399303760 | 390693927 | 382274098 | 374054272 | 0 |
| | A B | A B | АВ | A B | А В | |
| | 157 [°] 00' | 156 ⁰ 30' | 156 ⁰ 00' | 155 [°] 30′ | 155 ⁰ 00' | |
| l | | | | | .30 00 | J |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 1 | | 26°00' | - 0 | 27°00' | |
|-----|------------------------|-------------------------|------------------------|----------------------------------|-------------------------|----------|
| | 25 [°] 00' | 25 [°] 30' | | 26 [°] 30' | | |
| 0 | A B 374054272 | A B 366024451 | A B 358164634 | A B 350474821 | A B 342955012 | 30 |
| U | 373924275 | 365884454 | 358034637 | 350354824 | 342835015 | 30 |
| 1 | 373784278 373654281 | 365754457 365624460 | 357904640 357774643 | 350224827 350094830 | 342705018 342585022 | 29 |
| - 2 | 373514284 | 365494463 | 357644646 | 349974833 | 342465025 | 28 |
| | 373374287 | 365354466 | 357514649 | 349844837 | 342335028 | |
| 3 | 373244290 373104293 | 365224469 365094472 | 357384651 357254656 | 349714840 349594843 | 342215031 342095034 | 27 |
| 4 | 372974296 | 364964475 | 357124659 | 349464846 | 341965038 | 26 |
| 5 | 372834299 372704302 | 364834478 364694481 | 356994662 356864665 | 349334849 349214852 | 341845041 341725044 | 25 |
| | 372584305 | 364564484 | 356744668 | 349084856 | 341595047 | |
| 6 | 372434308 | 364434487 | 356614671 | 348964859 | 341475051 | 24 |
| 7 | 372294311 372164314 | 364304490 364174493 | 356484674 358354877 | 348834862 348704865 | 341345054 341225057 | 23 |
| | 372034317 | 364034496 | 356224680 | 348584868 | 341105060 | |
| 8 | 371894320 371764323 | 363904499 363774503 | 356094683 355964686 | 348454871 348324875 | 340975064 340855067 | 22 |
| 9 | 371624326 | 363644506 | 355834690 | 348204878 | 340735070 | 21 |
| | 371494329 | 363514509 | 355714693 | 348074881 | 340615073 | <u> </u> |
| 10 | 371354332 371224334 | 363384512 363254515 | 355584696 355454699 | 347954884 347824887 | 340485076 340385080 | 20 |
| 11 | 371084337 370954340 | 363114518 362984521 | 355324702 355194705 | 347704890 347574894 | 340245083 34011,5086 | 19 |
| 12 | 370814343 | 362854524 | 355064708 | 347444897 | 339995089 | 18 |
| | 370684346 | 362724527 | 354934711 | 347324900 | 339875093 | |
| 13 | 370554349 370414352 | 362594530 362464533 | 354814714 354684718 | 347194903 347074908 | 339745096 339625099 | 17 |
| 14 | 370284355 | 362334536 | 354554721 | 346944910 | 339505102 | 16 |
| 15 | 370144358 370014361 | 362204539 362064542 | 354424724 354294727 | 346824913 346694916 | 339385106 33925,5109 | 15 |
| | 369884364 | 361934545 | 354174730 | 346574919 | 339135112 | |
| 16 | 369744367 | 361804548 | 354044733 | 346444922 | 339015115 | 14 |
| 17 | 369614370 369484373 | 361674551 361544554 | 353914736 353784739 | 346324925 346194929 | 338895119 338765122 | 13 |
| | 369344376 | 361414557 | 353654742 | 346074932 | 338645125 | |
| 18 | 369214379 369074382 | 361284560 361154563 | 353534746 353404749 | 345944935 345824938 | 338525128 338405132 | 12 |
| 19 | 368944385 | 361024566 | 353274752 | 345694941 | 338275135 | 11 |
| | 368814388 | 360894569 | 353144755 | 345574945 | 338155138 | |
| 20 | 368674391 368544394 | 360764573 360634576 | 353024758 352894761 | 345444948 345324951 | 338035142 337915145 | 10 |
| 21 | 368414397 368274400 | 360504579 360374582 | 352764764 352634769 | 345194954 345074957 | 337795148 337665151 | 9 |
| 22 | 368144403 | 360244585 | 352514771 | 344944961 | 337545155 | |
| | 368014406 | 360114588 | 352384774 | 344824964 | 337425158 | |
| 23 | 367874409 367744412 | 359984591 359854594 | 352254/// 352124780 | 344694967 344574970 | 337305161 337175164 | ' |
| 24 | 367614415 | 359724597 | 352004783 | 344454973 | 337055168 | 6 |
| 25 | 367474418 367344421 | 359594600 359464603 | 351874786 351744789 | 344324977 344204980 | 336935171 336815174 | 5 |
| | 367214424 | 359334606 | 351614793 | 344074983 | 336695178 | Ľ |
| 26 | 367084427 | 359204609 | 351494796 | 343954986 | 336575181 | 4 |
| 27 | 366944430 366814433 | 359074612 358944615 | 351364799 351234802 | 343824989 343704993 | 336445184 336325187 | 3 |
| | 366684436 | 358814619 | 35111,4805 | 343574996 | 336205191 | |
| 28 | 366554439 366414442 | 358684622 358554625 | 350984808 350854811 | 343454999 343325002 | 336085194 335965197 | 2 |
| 29 | 366284445 | 358424628 | 350734815 | 343205005 | 335845200 | 1 |
| 30 | 366154448 | 358294631 35816 4634 | 350604818 | 343085009 | 335725204 | |
| 30 | 366024451 A B | 358164634 A B | 350474821 A B | 342955012 A B | 335595207 A B | <u> </u> |
| | | | | | | |
| | 154 [°] 30' | 154 ⁰ 00' | 153 ⁰ 30' | 153 ⁰ 00 [,] | 152 ⁰ 30' | |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 1 | 1 . | 1 . | 1 . | 1 . | ı |
|----|------------------------|------------------------|------------------------|------------------------|-------------------------|-------------|
| | 27 [°] 30' | 28 ⁰ 00' | 28 ⁰ 30' | 29 ⁰ 00' | 29°30' | 1 |
| | A B | A B | A B | A B | A B | <u> </u> |
| 0 | 335595207 335475210 | 328395406 328275410 | 321345610 321225614 | 314435818 | 307666030 | 30 |
| 1 | 335355214 | 328155413 | 321225617 | 314315822 314205825 | 307556034 307446038 | 29 |
| | 335235217 | 328035417 | 320995620 | 314095829 | 307336041 | |
| 2 | 335115220 | 327925420 | 320875624 | 313975832 | 307216045 | 28 |
| 3 | 334995224 334875227 | 327805423 327685426 | 320765627 320645631 | 313865836 313755839 | 307106048 306996052 | 27 |
| | 334755230 | 327565430 | 320525634 | 313635843 | 306886055 | <u> </u> |
| 4 | 334625233 | 327445433 | 320415638 | 313525846 | 306776059 | 26 |
| 5 | 334505237 334385240 | 327325437 327205440 | 320295641 320185645 | 313405850 313295853 | 306666062 306556066 | 25 |
| | 334265243 | 327095443 | 320065648 | 313185857 | 306436070 | L |
| 6 | 334145247 | 326975447 | 319945651 | 313065860 | 306326073 | 24 |
| 7 | 334025250 333905253 | 326855450 326735454 | 319835655 319715658 | 312955864 312845867 | 306216077 306106080 | 23 |
| | 333785257 | 326615457 | 319605662 | 312725871 | 305996084 | |
| 8 | 333665260 | 326495460 | 319485665 | 312615874 | 305886088 | 22 |
| 9 | 333545263 333425266 | 326385464 326255467 | 319365669 319255672 | 312505878 312385881 | 305778091 305666095 | 21 |
| | 333305270 | 326145470 | 319135675 | 312275885 | 305556098 | 1 2' |
| 10 | 333185273 | 326025474 | 319025679 | 312165888 | 305446102 | 20 |
| 11 | 333065277 332935280 | 325905477 325795481 | 318905682 318795686 | 312045892 311935895 | 305326106 | 19 |
| | 332815283 | 325675484 | 318675689 | 311825899 | 305216109 305106113 | '* |
| 12 | 332695287 | 325555487 | 318565693 | 311705902 | 304996116 | 18 |
| 13 | 332575290 332455293 | 325435491 325325494 | 318445696 318335700 | 311595906 311485909 | 304886120 304776124 | 17 |
| | 332335296 | 325205498 | 318215703 | 311375913 | 304666127 | l " |
| 14 | 332215300 | 325085501 | 318095707 | 311255917 | 304556131 | 16 |
| 15 | 332095303 331975306 | 324965504 324845508 | 317985710 317865714 | 311145920 | 304446134 | ٠., |
| | 331855310 | 324735511 | 317755717 | 311035924 310915927 | 304336138 304226142 | 15 |
| 16 | 331735313 | 324615515 | 317635720 | 310805931 | 304116145 | 14 |
| 17 | 331615316 331495320 | 324495518 324385521 | 317525724 317405727 | 310695934 310585938 | 304006149 303896153 | 13 |
| | 331375323 | 324265525 | 317295731 | 310465941 | 303786156 | 13 |
| 18 | 331255326 | 324145528 | 317175734 | 310355945 | 303676160 | 12 |
| 19 | 331135330 331015333 | 324025532 323915535 | 317065738 316945741 | 310245948 310135952 | 303566163 303456167 | 11 |
| | 330895336 | 323795538 | 316835745 | 310015955 | 303346171 | |
| 20 | 330775340 | 323675542 | 316725748 | 309905959 | 303226174 | 10 |
| 21 | 330655343 330545346 | 323555545 323445549 | 316605752 316485755 | 309795963 309685966 | 303116178 | |
| | 330425350 | 323325552 | 316375759 | 309565970 | 303006181 302896185 | 9 |
| 22 | 330305353 | 323205555 | 316265762 | 309455973 | 302786189 | 8 |
| 23 | 330185356 330065360 | 323095559 322975562 | 316145766 316035769 | 309345977 309235980 | 302676192 302566196 | 7 |
| | 329945363 | 322855566 | 315915773 | 309125984 | 302456200 | , |
| 24 | 329825366 | 322745569 | 315805776 | 309005988 | 302356203 | 6 |
| 25 | 329705370 329585373 | 322625572 322505576 | 315695780 315575783 | 308895991 308785995 | 302246207 302136210 | 5 |
| - | 329465376 | 322395579 | 315465787 | 308675998 | 302026214 | |
| 26 | 329345380 | 322275583 | 315345790 | 308566002 | 301916218 | 4 |
| 27 | 329225383 329105386 | 322155586 322045590 | 315235794 315115797 | 308446005 308336009 | 301806221 301696225 | 3 |
| | 328985390 | 321925593 | 315005801 | 308226012 | 301586229 | |
| 28 | 328875393 | 321805596 | 314885804 | 308116016 | 301476232 | 2 |
| 29 | 328755396 328635400 | 321695600 321575603 | 314775808 314665811 | 308006020 307886023 | 301366236 30125 6240 | . |
| | 328515403 | 321455607 | 314545815 | 307776027 | 301256240 301146243 | 1 |
| 30 | 328395406 | 321345610 | 314435818 | 307666030 | 301036247 | 0 |
| | А В | A B | A B | A B | A B | |
| | 152 ⁰ 00' | 151 ⁰ 30' | 151°00' | 150°30' | 150°00' | |
| 1 | ı (| l l | i l | | | l |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 30°00' | 30°30' | 31°00′ | 31°30' | 32°00' | 1 |
|----|------------------------|------------------------|------------------------|------------------------|-------------------------------------|----------|
| | A B | A B | АВ | A B | A B | 1 |
| 0 | 301036247 300926251 | 294536468 294426472 | 288166693 288066697 | 281916923 281816927 | 275797158 | 30 |
| 1 | 300816254 300706258 | 294326475 294216479 | 287956701 287856705 | 281716931 281616935 | 275697162 275597166 275497170 | 29 |
| 2 | 300596262 | 294106483 | 287746709 | 281506939 | 275397174 | 28 |
| 3 | 300486265 300376269 | 293996487 293896490 | 287636712 287536716 | 281406943 281306947 | 275287178 275187182 | 27 |
| | 300266273 | 293786494 | 287436720 | 281196951 | 275087186 | <u> </u> |
| 4 | 300166276 300056280 | 293676498 293576501 | 287326724 287226728 | 281096954 280996958 | 274987190 274887193 | 26 |
| 5 | 299946284 | 293466505 | 287116731 | 280896962 | 274787197 | 25 |
| | 299836287 | 293356509 | 287016735 | 280786966 | 274687201 | — |
| 6 | 299726291 299616294 | 293256513 293146516 | 286906739 286806743 | 280686970 280586974 | 274587205 274487209 | 24 |
| 7 | 299506298 299396302 | 293036520 | 286696747 | 280476978 | 274387213 | 23 |
| 8 | 299286305 | 292936524 292826528 | 286596750 | 280376982 | 274287217 | - |
| | 299176309 | 292716531 | 286486754 286386758 | 280276985 280176989 | 274187221 274087225 | 22 |
| 9 | 299076313 298966316 | 292616535 292506539 | 286276762 286176766 | 280066993 279966997 | 273987229 273877233 | 21 |
| 10 | 298856320 | 292396543 | 286066770 | 279867001 | 273777237 | 20 |
| 11 | 298746324 | 292296546 | 285966773 | 279767005 | 273677241 | |
| ** | 298636328 298526331 | 292186550 292076554 | 285866777 285756781 | 279657009 279557013 | 273577245 273477249 | 19 |
| 12 | 298416335 | 291976558 | 285656785 | 279457017 | 273377253 | 18 |
| 13 | 298316339 298206342 | 291866561 291756565 | 285546789 285446793 | 279357021 279257024 | 273277257 | ., |
| | 298096346 | 291656569 | 285336798 | 279147028 | 273177261 273077265 | 17 |
| 14 | 297986350 | 291546573 | 285236800 | 279047032 | 272977269 | 16 |
| 15 | 297876353 297766357 | 291446576 291336580 | 285136804 285026808 | 278947036 278847040 | 272877273 272777277 | 15 |
| | 297666361 | 291226584 | 284926812 | 278747044 | 272677281 | |
| 16 | 297556364 297446368 | 291126588 291016591 | 284816815 284716819 | 278637048 | 272577285 | 14 |
| 17 | 297336372 | 290916595 | 284616823 | 278537052 278437056 | 272477289 272377293 | 13 |
| | 297226375 | 290806599 | 284506827 | 278337060 | 272277297 | |
| 18 | 297116379 297016383 | 290696603 290596606 | 284406831 284296835 | 278237064 278127067 | 272177301 272077305 | 12 |
| 19 | 296906386 296796390 | 290486610 290386614 | 284196839 | 278027071 | 271977309 | 11 |
| 20 | 296686394 | 290276618 | 284096842 283986846 | 277927075 | 271877313 | - |
| | 296576398 | 290166622 | 283886850 | 277827079 277727083 | 271777317 271677321 | 10 |
| 21 | 296476401 296366405 | 290066625 289956629 | 283786854 283676858 | 277617087 277517091 | 271577325 271477329 | 9 |
| 22 | 296256409 | 289856633 | 283576862 | 277417095 | 271377333 | 8 |
| 23 | 296146412 | 289746637 | 283466865 | 277317099 | 271277337 | |
| | 296046416 295936420 | 289646640 289536644 | 283366869 283266873 | 277217103 277117107 | 271177341 271077345 | 7 |
| 24 | 295826423 | 289426648 | 283156877 | 277017111 | 270987349 | 6 |
| 25 | 295716427 295606431 | 289326652 289216655 | 283056881 282956885 | 276907115 276807118 | 270887353 270787357 | 5 |
| | 295506435 | 289116659 | 282846889 | 276707122 | 270687361 | ľ |
| 26 | 295396438 295286442 | 289006663 288906667 | 282746893 282646896 | 276607126 | 270587365 | 4 |
| 27 | 295176446 | 288796671 | 282536900 | 276507130 276407134 | 270487369 270387373 | з |
| | 295076449 | 288696674 | 282436904 | 276307138 | 270287377 | |
| 28 | 294966453 294856457 | 288586678 288486682 | 282336908 282226912 | 276197142 276097146 | 270187381 270087385 | 2 |
| 29 | 294756461 | 288376686 | 282126916 | 275997150 | 269987389 | 1 |
| 30 | 294646464 294536468 | 288276690 | 282026920 | 275897154 | 269887393 | |
| | A B | 288166693 A B | 281916923 A B | 275797158 A B | 269787397 | 0 |
| | | | | | A B | 1 |
| | 149 [°] 30' | 149 ⁰ 00' | 148 ⁰ 30' | 148 ⁰ 00′ | 147 [°] 30' | |
| | - | • | • | • | | • |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | | 1 . | 1 | 1 , | 1 . | 1 |
|------|------------------------|------------------------|------------------------|------------------------|------------------------|-------------|
| | 32 [°] 30' | 33°00, | 33°30' | 34 ⁰ 00' | 34 [°] 30' | 4 |
| | A B | A B | АВ | A B | A B | |
| 0 | 269787397 | 263897641 | 258117889 | 252448143 | 246878401 | 30 |
| 1 | 269687401 269587405 | 263797645 263707649 | 258017893 257927898 | 252358147 252258151 | 246788405 246698409 | 29 |
| | 269497409 | 263607653 | 257827902 | 252168155 | 246608414 | |
| 2 | 269397413 | 263507657 | 257737906 | 252068160 | 246508418 | 28 |
| 3 | 269297417 269197421 | 263407661 263317665 | 257637910 257547914 | 251978164 251888168 | 246418422 | 27 |
| | 269097425 | 263217670 | 257447919 | 251788172 | 246328427 246238431 | 27 |
| 4 | 268997429 | 263117674 | 257357923 | 251698177 | 246148435 | 26 |
| 5 | 268897433 268797437 | 263027678 262927682 | 257257927 | 251608181 | 246058440 | 25 |
| | 268697441 | 262827686 | 257167931 257067935 | 251508185 251418189 | 245958444 245868448 | 25 |
| 6 | 268607445 | 262737690 | 256977940 | 251328194 | 245778453 | 24 |
| 7 | 268507449 | 262637694 | 256877944 | 251228198 | 245688457 | |
| , | 268407453 268307458 | 262537698 262447702 | 256787948 256687952 | 251138202 251048207 | 245598461 245508466 | 23 |
| 8 | 268207462 | 262347707 | 256597956 | 250948211 | 245408470 | 22 |
| • | 268107466 | 262247711 | 256497961 | 250858215 | 245318475 | |
| 9 | 268007470 267907474 | 262147715 262057719 | 256407965 256307969 | 250768219 250668224 | 245228479 245138483 | 21 |
| 10 | 267817478 | 261957723 | 256217973 | 250578228 | 245048488 | 20 |
| | 267717482 | 261857727 | 256117977 | 250488232 | 244958492 | |
| 11 | 267617486 267517490 | 261757731 261667736 | 256027982 255927986 | 250388237 250298241 | 244868496 244778501 | 19 |
| 12 | 267417494 | 261577740 | 255837990 | 250208245 | 244678505 | 18 |
| | 267317498 | 261477744 | 255737994 | 250118249 | 244588510 | |
| 13 | 267227502 267127506 | 261377748 261287752 | 255647998 255548003 | 250018254 249928258 | 244498514 | 17 |
| 14 | 267027510 | 261187756 | 255458007 | 249838262 | 244408518 244318523 | 16 |
| | 266927514 | 261087760 | 255368011 | 249738267 | 244228527 | 16 |
| 15 | 266827518 266727522 | 260997764 | 255268015 | 249648271 | 244138531 | 15 |
| 16 | 266637526 | 260897769 260797773 | 255178020 | 249558275 | 244048536 | |
| | 266537531 | 260707777 | 255078024 254988028 | 249468280 249368284 | 243958540 243858545 | 14 |
| 17 | 266437535 266337539 | 260607781 | 254888032 | 249278288 | 243768549 | 13 |
| 18 | 266237543 | 260517785 | 254798037 | 249188292 | 243678553 | |
| 10 | 266147547 | 260417789 260317793 | 254698041 254608045 | 249098297 248998301 | 243588558 243498562 | 12 |
| 19 | 266047551 | 260227798 | 254518049 | 248908305 | 243408567 | 11, |
| | 265947555 | 260127802 | 254418053 | 248818310 | 243318571 | |
| 20 | 265847559 265747563 | 260027806 259937810 | 254328058 254228062 | 248728314 248628318 | 243228575 243138580 | 10 |
| 21 | 265657567 | 259837814 | 254138066 | 248538323 | 243048584 | 9 |
| | 265557571 | 259747818 | 254038070 | 248448327 | 242958589 | |
| 22 | 265457575 265357579 | 259647823 259547827 | 253948075 253858079 | 248358331 248258336 | 242868593 242768597 | 8 |
| 23 | 265267584 | 259457831 | 253758083 | 248168340 | 242678602 | 7 |
| | 265167588 | 259357835 | 253668087 | 248078344 | 242588606 | <u> </u> |
| . 24 | 265067592 264967596 | 259267839 259167843 | 253568091 253478096 | 247988349 247888353 | 242498611 242408615 | 6 |
| 25 | 264867600 | 259077848 | 253388100 | 247798357 | 242318619 | 5 |
| | 264777604 | 258977852 | 253288104 | 247708362 | 242228624 | <u> </u> |
| 26 | 264677608 264577612 | 258877856 258787860 | 253198108 253098113 | 247618366 247528370 | 242138628 242048633 | 4 |
| 27 | 264477616 | 258687864 | 253008117 | 247428375 | 241958637 | 3 |
| | 264387620 | 258597868 | 252918121 | 247338379 | 241868641 | |
| 28 | 264287625 264187629 | 258497873 258407877 | 252818125 252728130 | 247248383 247158388 | 241778646 | 2 |
| 29 | 264097633 | 258307881 | 252638134 | 247158388 | 241688650 241598655 | 1 |
| | 263997637 | 258217885 | 252538138 | 246968396 | 241508659 | |
| 30 | 263897641 | 258117889 | 252448143 | 246878401 | 241418663 | 0 |
| | A B | A B | АВ | A B | A B | |
| | 147 ⁰ 00' | 146 [°] 30' | 146 ⁰ 00' | 145 ^O 30' | 145 [°] 00' | |
| Į. | l l | l | | l | | J |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | ı | | 1 | ARE R PROMISOT | 1 ABEE | • |
|----|------------------------|------------------------|------------------------|------------------------|--------------------------|--------------|
| | 35°00' | 35°30′ | 36°00' | 36°30′ | 37 ⁰ 00' | |
| | A B | A B | A B | A B | A B | |
| 0 | 241418663 241328668 | 236058931 235968936 | 230789204 | 225619482 225539487 | 220549765 | 30 |
| 1 | 241238672 | 235878940 | 230699209 230619213 | 225539487 225449492 | 220459770 220379775 | 29 |
| | 241148677 | 235788945 | 230529218 | 225369496 | 220299779 | |
| 2 | 241058681 240968686 | 235698949 235608954 | 230439223 230359227 | 225279501 225199505 | 220209784 220129789 | 28 |
| 3 | 240878690 240788694 | 235518958 | 230269232 | 255109510 | 220039794 | 27 |
| 4 | 240698699 | 235438963 235348967 | 230179236 230099241 | 225019515 224939520 | 219959798 | |
| | 240608703 | 235258972 | 230009246 | 224849524 | 219879803 219789808 | 26 |
| 5 | 240518708 240428712 | 235168976 235078981 | 229919250 229839255 | 224769529 224679534 | 219709813 219629818 | 25 |
| 6 | 240338717 | 234988986 | 229749259 | 224599538 | 219539822 | 24 |
| 7 | 240248721 240158726 | 234908990 234818995 | 229659264 299579269 | 224509543 | 219459827 | |
| | 240068730 | 234728999 | 229489273 | 224429548 224339552 | 219379832 219289837 | 23 |
| 8 | 239978734 | 234639004 | 229399278 | 224259557 | 219209841 | 22 |
| 9 | 239888739 239798743 | 234549008 234469013 | 229319282 229229287 | 224169562 224089566 | 219129846 219039851 | 21 |
| | 239708748 | 234379017 | 229139292 | 223999571 | 218959856 | |
| 10 | 239618752 239528757 | 234289022 234199026 | 229059296 228969301 | 223919576 223829581 | 218879861 218789865 | 20 |
| 11 | 239438761 | 234109031 | 228879305 | 223749585 | 218709870 | 19 |
| 12 | 239348766 239258770 | 234029035 233939040 | 228799310 228709315 | 223669590 | 218629875 | |
| | 239168775 | 233849044 | 228629319 | 223579595 223499599 | 218539880 218459885 | 18 |
| 13 | 239078779 238988783 | 233759049 233669054 | 228539324 228449329 | 223409604 223329609 | 218379889 218289894 | 17 |
| 14 | 238898788 | 233589058 | 228369333 | 223239614 | 218209899 | 16 |
| 15 | 238808792 238718797 | 233499063 233409067 | 228279338 | 223159618 | 218129904 | |
| | 238638801 | 233319072 | 228189342 228109347 | 223069623 222989628 | 218039909 217959913 | 15 |
| 16 | 238548806 | 233239076 | 228019352 | 222899632 | 217879918 | 14 |
| 17 | 238458810 238368815 | 233149081 233059085 | 227939356 227849361 | 222819637 222729642 | 217789923 217709928 | 13 |
| | 238278819 | 232969090 | 227759366 | 222649647 | 217629933 | |
| 18 | 238188824 238098828 | 232889094 232799099 | 227679370 227589375 | 222569651 222479656 | 217549937 217459942 | 12 |
| 19 | 238008833 | 232709104 | 227509380 | 222399661 | 217379947 | 11 |
| 20 | 237918837 237828842 | 232619108 232529113 | 227419384 227329389 | 222309665 | 217299952 | |
| | 237738846 | 232449117 | 227249394 | 222229670 222139675 | 217209957 217129962 | 10 |
| 21 | 237648850 237558855 | 232359122 232269126 | 227159398 227079403 | 222059680 221979684 | 217049966 216969971 | 9 |
| 22 | 237478859 | 232189131 | 226989407 | 221889689 | 216879976 | 8 |
| 23 | 237388864 237298868 | 232099136 232009140 | 226909412 | 221809694 | 216799981 | _ |
| | 237208873 | 231919145 | 226819417 226729421 | 221719699 221689703 | 216719986 216629990 | ' |
| 24 | 237118877 | 231839149 | 226649426 | 221549708 | 216549995 | 6 |
| 25 | 237028882 236938886 | 231749154 231659158 | 226559431 226479435 | 221469713 221389718 | 2164610000 2163810005 | 5 |
| | 236848891 | 231569163 | 226389440 | 221299722 | 2162910010 | |
| 26 | 236758895 236678900 | 231489168 231399172 | 226309445 226219449 | 221219727 221129732 | 2162110015 2161310019 | 4 |
| 27 | 236588904 | 231309177 | 226129454 | 221049737 | 2160510024 | 3 |
| 28 | 236498909 236408913 | 231229181 231139186 | 226049459 | 220969741 | 2159610029 | |
| | 236318918 | 231049190 | 225959463 225879468 | 220879746 220799751 | 2158810034 2158010039 | 2 |
| 29 | 236228922 236138927 | 230959195 230879200 | 225789473 225709477 | 220709756 220629760 | 2157210044 2156310049 | 1 |
| 30 | 236058931 | 230789204 | 225619482 | 220549765 | 2155510049 | 0 |
| | A B | А В | A B | A B | A B | - |
| | 144°30' | 144 [°] 00' | 143 ⁰ 30' | 143 ⁰ 00' | 142 [°] 30' | |
| | | | | | 142 00 | |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 37 [°] 30' | 38 ⁰ 00' | 38°30' | 39°00' | 39°30' | 1 |
|----|--------------------------|--------------------------|--------------------------|-----------------------------------|--------------------------|-------------|
| | A B | A B | A B | A B | A B | |
| -0 | 2155510053 | 2106610347 | 2058510646 | 2011310950 | 1964911259 | 30 |
| | 2154710058 | 2105810352 | 2057710651 | 2010510955 | 1964111265 | |
| 1 | 2153910063 2153110068 | 2105010357 2104210362 | 2056910656 2056110661 | 2009710960 2008910965 | 1963411270 1962611275 | 29 |
| 2 | 2152210073 | 2103310367 | 2055310666 | 2008210970 | 1961811280 | 28 |
| 3 | 2151410078 215061008≥ | 2102510372 2101710376 | 2054510671 2053710676 | 2007410975 | 1961111285 1960311291 | 27 |
| | 2149810087 | 2100910381 | 2052910681 | 2006610980 2005810986 | 1959511296 | |
| 4 | 2148910092 | 2100110386 | 2052210686 | 2005010991 | 1958811301 | 26 |
| 5 | 2148110097 2147310102 | 2099310391 2098510396 | 2051410691 2050610696 | 2004310996 2003511001 | 1958011306 1957211311 | 25 |
| | 2146510107 | 2097710401 | 2049810701 | 2002711006 | 1956511317 | |
| 6 | 2145710112 | 2096910406 | 2049010706 | 2001911011 | 1955711322 | 24 |
| 7 | 2144810116 2144010121 | 2096110411 2095310416 | 2048210711 2047410716 | 2001211016 2000411021 | 1954911327 1954111332 | 23 |
| | 2143210126 | 2094510421 | 2046610721 | 1999611027 | 1953411338 | |
| 8 | 2142410131 2141610136 | 2093710426 2092910431 | 2045810726 2045010731 | 1998811032 1998011037 | 1952711343 1951911348 | 22 |
| 9 | 2140710141 | 2092110436 | 2044210736 | 1997311042 | 1951111353 | 21 |
| | 2139910146 | 2091310441 | 2043510741 | 1996511047 | 1950411359 | |
| 10 | 2139110151 2138310155 | 2090510446 2089710451 | 2042710746 2041910751 | 1995711052 1994911057 | 1949611364 1948811369 | 20 |
| 11 | 2137510160 2136710165 | 2088810456 2088010461 | 2041110756 2040310761 | 1994211063 1993411068 | 1948111374 1947311380 | 19 |
| 12 | 2135810170 | 2087210466 | 2039510767 | 1992611073 | 1946611385 | 18 |
| | 2135010175 | 2086410471 | 2038710772 | 1991911078 | 1945811390 | |
| 13 | 2134210180 2133410185 | 2085610476 2084810481 | 2037910777 2037110782 | 1991111083 1990311088 | 1945011395 1944311400 | 17 |
| 14 | 2132610190 | 2084010486 | 2036410787 | 1989511094 | 1943511406 | 16 |
| 15 | 2131810195 2130910199 | 2083210491 2082410496 | 2035610792 2034810797 | 1988811099 1988011104 | 1942811411 1942011416 | 15 |
| | 2130110204 | 2081610500 | 2034010802 | 1987211109 | 1941211422 | |
| 16 | 2129310209 | 2080810505 | 2033210807 | 1986411114 | 1940511427 | 14 |
| 17 | 2128510214 2127710219 | 2080010510 2079210515 | 2032410812 2031610817 | 1985711119 1984911124 | 1939711432 1939011437 | 13 |
| | 2126910224 | 2078410520 | 2030910822 | 1984111130 | 1938211443 | |
| 18 | 2126010229 2125210234 | 2077610525 2076810530 | 2030110827 2029310832 | 1983411135 1982611140 | 1937511448 1936711453 | 12 |
| 19 | 2124410239 | 2076010535 | 2028510838 | 1981811145 | 1935911458 | 11 |
| | 2123610243 | 2075210540 | 2027710843 | 1981011150 | 1935211464 | |
| 20 | 2122810248 2122010253 | 2074410545 2073610550 | 2026910848 2026110853 | 19803111 <i>5</i> 6 1979511161 | 1934411469 1933711474 | 10 |
| 21 | 2121210258 2120410263 | 2072810555 2072010560 | 2025410858 2024610863 | 1978711166 1977911171 | 1932911479 1932111485 | 9 |
| 22 | 2119510268 | 2071210565 | 2023810868 | 1977211176 | 1931411490 | |
| 23 | 2118710273 | 2070410570 | 2023010873 | 1976411181 | 1930611495 | |
| | 2117910278 2117110283 | 2069610575 2068810580 | 2022210878 | 1975611187 1974911192 | 1929911501 1929111506 | i ' |
| 24 | 2116310288 | 2068010585 | 2020710888 | 1974111197 | 1928411511 | 6 |
| 25 | 2115510293 2114710298 | 2067210590 2066510595 | 2019910894 2019110899 | 1973311202 1972611207 | 1927611516 1926911522 | 5 |
| | 2113910302 | 2065710600 | 2018310904 | 1971811213 | 1926111527 | <u> </u> |
| 26 | 2113110307 2112210312 | 2064910605 2064110610 | 2017510909 | 1971011218 | 1925311532 | 4 |
| 27 | 2111410317 | 2063310615 | 2016710914 2016010919 | 1970311223 1969511228 | 1924611537 1923811543 | 3 |
| | 2110610322 | 2062510620 | 2015210924 | 1968711233 | 1923111548 | |
| 28 | 2109810327 2109010332 | 2061710625 2060910630 | 2014410929 2013610934 | 1968011239 1967211244 | 1922311553 1921611559 | 2 |
| 29 | 2108210337 | 2060110635 | 2012810939 | 1966411249 | 1920811564 | 1 |
| 20 | 2107410342 | 2059310640 | 2012110945 | 1965711254 | 1920111569 | |
| 30 | 2106610347 A B | 2058510646 A B | 2011310950 A B | 1964911259 A B | 1919311575 | |
| | | | | | A B | |
| | 142 ⁰ 00' | 141 ⁰ 30′ | 141 ⁰ 00' | 140 [°] 30′ | 140 ⁰ 00' | |
| | - ' | - | • | • | - | • |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | | | | | ۰ | 1 |
|------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------|
| | 40°00' | 40 [°] 30' | 41 ⁰ 00' | 41 [°] 30′ | 42 ⁰ 00' | |
| | A B | A B | A B | A B | A B | |
| 0 | 1919311575 1918611580 | 1874611895 1873811901 | 1830612222 1829812228 | 1787312554 1786612560 | 1744912893 1744212898 | 30 |
| 1 | 1917811585 1917111590 | 1873111906 1872311912 | 1829112233 1828412238 | 1785912566 1785212571 | 1743512904 1742812910 | 29 |
| 2 | 1916311596 | 1871611917 | 1827712244 | 1784512577 | 1742112915 | 28 |
| 2 | 1915611601 | 1870911922 | 1826912249 | 1783812582 | 1742112915 | 20 |
| 3 | 1914811606 1914111612 | 1870111928 1869411933 | 1826212255 1825512260 | 1783112588 1782412593 | 1740712927 1740012932 | 27 |
| 4 | 1913311617 | 1868611939 | 1824812266 | 1781612599 | 1739312938 | 26 |
| | 1912611622 | 1867911944 | 1924012271 | 1780912605 | 1728612944 | |
| 5 | 1911811628 1911111633 | 1867211949 1866411955 | 1823312277 1822612282 | 1780212610 1779512616 | 1737912950 1737212955 | 25 |
| | 1910311638 | 1865711960 | 1821912288 | 1778812622 | 1736512961 | 24 |
| 7 | 1909611644 1908811649 | 1865011966 1864211971 | 1821112293 | 1778112627 | 1735812967 1735112972 | 23 |
| , | 1908111654 | 1863511977 | 1820412299 1819712305 | 1777412633 1776712638 | 1734412978 | 23 |
| 8 | 1907311660 | 1862711982 | 1819012310 | 1776012644 | 1733712984 | 22 |
| 9 | 1906611665 1905811670 | 1862011987 1861311993 | 1818212316 1817512321 | 1775212650 1774512655 | 1733012990 1732312995 | 21 |
| | 1905111676 | 1860511998 | 1816812327 | 1773812661 | 1731613001 | |
| 10 | 1904311681 | 1859812004 | 1816112332 | 1773112667 | 1730913007 | 20 |
| 11 | 1903611686 1902811692 | 1859112009 1858312014 | 1815412338 1814612343 | 1772412672 1771712678 | 1730213012 1729513018 | 19 |
| | 1902111697 | 1857612020 | 1813912349 | 1771012683 | 1728813024 | |
| 12 | 1901311702 1900611708 | 1856912025 1856112031 | 1813212354 1812512360 | 1770312689 1769612695 | 1728113030 1727413035 | 18 |
| 13 | 1899811713 | 1855412036 | 1811712365 | 1768912700 | 1726713041 | 17 |
| | 1899111718 | 1854712042 | 1811012371 | 1768112706 | 1726013047 | |
| 14 | 1898311724 1897611729 | 1853912047 1853212053 | 1810312376 1809612382 | 1767412711 1766712717 | 1725313053 1724613058 | 16 |
| 15 | 1896811734 | 1852512058 | 1808912387 | 1766012723 | 1723913064 | 15 |
| -10 | 1896111740 | 1851712063 | 1808112393 | 1765312728 | 1723213070 | |
| 16 | 1895311745 1894611750 | 1851012069 1850312074 | 1807412398 1806712404 | 1764612734 1763912740 | 1722513075 1721813081 | 14 |
| 17 | 1893911756 1893111761 | 1849512080 1848812085 | 1806012410 1805312415 | 1763212745 1762512751 | 1721213087 1720513093 | 13 |
| 18 | 1892411766 | 1848112091 | 1804512421 | 1761812757 | 1719813098 | 12 |
| | 1891611772 | 1847312096 | 1803812426 | 1761112762 | 1719113104 | |
| . 19 | 1890911777 1890111782 | 1846612102 1845912107 | 1803112432 1802412437 | 1760412768 1759712774 | 1718413110 1717713116 | 11 |
| 20 | 1889411788 | 1845112112 | 1801712443 | 1759012779 | 1717013121 | 10 |
| 0.1 | 1888611793 | 1844412118 | 1801012448 | 1758312785 | 1716313127 | |
| 21 | 1887911799 1887211804 | 1843712123 1842912129 | 1800212454 1799512460 | 1757512790 1756812796 | 1715613133 1714913139 | 9 |
| 22 | 1886411809 | 1842212134 | 1798812465 | 1756112802 | 1714213144 | 8 |
| 23 | 1885711815 1884911820 | 1841512140 1840812145 | 1798112471 1797412476 | 1755412807 1754712813 | 1713513150 1712813156 | 7 |
| | 1884211825 | 1840012151 | 1796612482 | 1754012819 | 1712113162 | |
| 24 | 1883411831 | 1839312156 | 1795912487 | 1753312824 | 1711413168 | 6 |
| 25 | 1882711836 1882011842 | 1838612162 1837812167 | 1795212493 1794512499 | 1752612830 1751912836 | 1710813173 1710713179 | 5 |
| | 1881211847 | 1837112173 | 1793812504 | 1751212841 | 1709413185 | |
| 26 | 1880511852 1879711858 | 1836412178 1835712184 | 1793112510 1792412515 | 1750512847 1749812853 | 1708713191 1708013196 | 4 |
| 27 | 1879011863 | 1834912189 | 1791612511 | 1749112859 | 1707313202 | 3 |
| | 1878311868 | 1834212195 | 1790912526 | 1748412864 | 1706613208 | |
| 28 | 1877511874 1876811879 | 1833512200 1832712205 | 1790212532 1789512538 | 1747712870 1747012876 | 1705913214 1705213220 | 2 |
| 29 | 1876011885 | 1832012211 | 1788812543 | 1746312881 | 1704613225 | 1 |
| | 1875311890 | 1831312216 | 1788112549 | 1745612887 | 1703913231 | <u> </u> |
| | 1874611895 A B | 1830612222 | 1787312554 | 1744912893 | 1703213237 | - |
| | | A B | A B | A B | A B | |
| | 139 [°] 30' | 139 ⁰ 00' | 138 ⁰ 30' | 138 ⁰ 00' | 137 ⁰ 30′ | |
| ' | • | , | • | • | • | • |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | • | IAN LATTODE, IN V | MICH CASE TAKE | 2 PROWITOF OF | IADLE | |
|-------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|----|
| | 42 [°] 30′ | 43 [°] 00' | 43°30' | 44 ⁰ 00' | 44 [°] 30' | |
| | А В | A B | A B | A B | A B | |
| 0 | 1703213237 | 1662213587 | 1621913944 | 1582314307 | 1543414676 | 30 |
| 1 | 1702513243 1701813248 | 1661513593 1660813599 | 1621213950 1620513956 | 1581614313 1581014319 | 1542714682 1542114688 | 29 |
| | 1701113254 | 1660113605 | 1619913962 | 1580314325 | 1541414694 | |
| 2 | 1700413260 1699713266 | 1659513611 1658813617 | 1619213968 1618613974 | 1579714331 1579014337 | 1540814701 1540214707 | 28 |
| 3 | 1699013272 | 1658113623 | 1617913980 | 1578414343 | 1539514713 | 27 |
| | 1698313277 | 1657413628 | 1617213986 | 1577714349 | 1538914719 | |
| 4 | 1697713283 1697013289 | 1656713634 1656113640 | 1616613992 1615913998 | 1577114355 1576414362 | 1538214726 1537614732 | 26 |
| 5 | 1696313295 1695613301 | 1655413646 1654713652 | 1615214004 1614614010 | 1575814368 1575114374 | 1537014738 1536314744 | 25 |
| 6 | 1694913306 | 1654013658 | 1613914016 | 1574414380 | 1535714750 | 24 |
| ' | 1694213312 | 1653413664 | 1613214022 | 1573814386 | 1535014757 | |
| 7 | 1693513318 1692813324 | 1652713670 1652013676 | 1612614028 1611914034 | 1573114392 1572514398 | 1534414763 1533814769 | 23 |
| 8 | 1692213330 | 1651313682 | 1611214040 | 1571814404 | 1533114775 | 22 |
| 9 | 1691513336 1690813341 | 1650713688 1650013694 | 1610614046 1609914052 | 1571214411 1570514417 | 1532514782 1531814788 | 21 |
| | 1690113347 | 1649313700 | 1609314058 | 1569914423 | 1531214794 | |
| 10 | 1689413353 | 1648713705 | 1608614064 | 1569214429 | 1530614800 | 20 |
| 11 | 1688713359 1688013365 | 1648013711 1647313717 | 1607914070 1607314076 | 1568614435 1567914441 | 1529914807 1529314813 | 19 |
| | 1687413370 | 1646613723 | 1606614082 | 1567314447 | 1528614819 | |
| 12 | 1686713376 1686013382 | 1646013729 1645313735 | 1606014088 1605314094 | 1566614453 1566014460 | 1528014825 1527414831 | 18 |
| 13 | 1685313388 | 1644613741 | 1604614100 | 1565314466 | 1526714838 | 17 |
| | 1684613394 | 1643913747 | 1604014106 | 1564714472 | 1526114844 | 10 |
| 14 | 1683913400 1683313405 | 1643313753 1642613759 | 1603314112 1602714118 | 1564014478 1563414484 | 1525514850 1524814857 | 16 |
| 15 | 1682613411 1681913417 | 1641913765 1641313771 | 1602014124 1601314130 | 1562714490 1562114496 | 1524214863 1523514869 | 15 |
| 16 | 1681213423 | 1640613777 | 1600714136 | 1561414503 | 1522914875 | 14 |
| | 1680513429 | 1639913783 | 1600014142 | 1560814509 | 1522314882 | |
| 17 | 1679813435 1679213440 | 1639213789 1638613794 | 1599414149 1598714155 | 1560214515 1559514521 | 1521614888 1521014894 | 13 |
| 18 | 1678513446 | 1637913800 | 1598014161 | 1558914527 | 1520414900 | 12 |
| 19 | 1677813452 1677113458 | 1637213806 1636613812 | 1597414167 1596714173 | 1558214533 1557614540 | 1519714907 1519114913 | 11 |
| | 1676413464 | 1635913818 | 1596114179 | 1556914546 | 1518414919 | |
| 20 | 1675713470 | 1635213824 1634613830 | 1595414185 | 1556314552 | 1517814925 | 10 |
| 21 | 1675113476 1674413481 | 1633913836 | 1594714191 1594114197 | 1555614558 1555014564 | 1517214932 1516514938 | 9 |
| | 1673713487 | 1633213842 | 1593414203 | 1554314570 | 1515914944 | |
| 22 | 1673013493 1672313499 | 1632513848 1631913854 | 1592814209 1592114215 | 1553714577 1553014583 | 1515314951 1514814957 | 8 |
| 23 | 1671713505 | 1631213860 | 1591514221 | 1552414589 | 1514014963 | 7 |
| 24 | 1671013511 1670313517 | 1630513866 1629913872 | 1590814227 1590114233 | 1551714595 1551114601 | 1513414969 1512714976 | 6 |
| | 1669613523 | 1629213878 | 1589514240 | 1550514608 | 1512114982 | ů |
| 25 | 1668913528 1668313534 | 1628513884 1627913890 | 1588814246 1588214252 | 1549814614 1549214620 | 1511514988 1510814995 | 5 |
| 26 | 1667613540 | 1627213896 | 1587514258 | 1548514626 | 1510215001 | 4 |
| 27 | 1666913546 1666213552 | 1626513902 1625913908 | 1586914264 1586214270 | 1547914632 1547214639 | 1509615007 1508915014 | 3 |
| | 1665613558 | 1625213914 | 1585614276 | 1546614645 | 1508315020 | 3 |
| 28 | 1664913564 | 1624513920 | 1584914282 | 1545914651 | 1507715026 | 2 |
| 29 | 1664213570 1663513575 | 1623913926 1623213932 | 1584214288 1583614294 | 1545314657 1544714663 | 1507015033 1506415039 | 1 |
| | 1662813581 | 1622513938 | 1582914300 | 1544014670 | 1505815045 | |
| 30 | 1662213587 | 1621913944 | 1582314307 | 1543414676 | 1505115051 | 0 |
| | A B | A B | A B | A B | A B | |
| | 137 [°] 00′ | 136 ⁰ 30' | 136 ⁰ 00' | 135 ⁰ 30' | 135 ⁰ 00' | |
| | " | • | • | | • | - |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| A B A B A B A B A B A B A B A B A B A B | | 45 [°] 00' | 45 [°] 30' | 46 [°] 00' | 46 [°] 30' | 47 ⁰ 00' | 1 |
|--|----|---------------------|---------------------|---------------------|---------------------|---------------------|--------------|
| 15051_15051 | | | | | | | 1 |
| 1 15039 | 0 | | | | | 1358716622 | 30 |
| 2 1500615077 1445115499 1420215846 1300016245 1305616246 22 1305016245 1305616246 1305616259 1305616269 1305616269 1305616269 1305616269 1305616269 1305616269 1305616269 1305616269 1305616269 1305616269 1305616269 1305616269 1305616269 1305616269 1305616269 1305616269 1305616279 13056 | 1 | | | | | | 29 |
| 15003_15008_1 14646_15466_1 14676_15666_2 13961_16266_2 27 1307_15066_2 14630_15676_2 14626_15666_2 13060_16266_3 13060_16266_2 27 15007_15006_3 14630_15676_3 14620_15666_2 14620_15666_2 14620_15666_2 14620_15666_2 14620_15666_2 14620_15666_2 14620_15666_3 14620_15666_2 14620_15666_3 14620_1566_3 14620_156 | | | 1465715453 | | | | |
| \$\begin{array}{cccccccccccccccccccccccccccccccccccc | 2 | | | | | | 28 |
| 4 1500115102 1462615485 1425215862 1389616272 1385416875 26 1498515108 1442615495 1425215862 1399016279 1353416863 25 1498215118 1446415696 1424615698 1386416287 1385416863 25 1386416287 1385416863 25 1498215121 1449615698 1386416282 1385416863 25 1386416282 1385416863 25 1386416282 1385416863 25 1386416282 1385416863 1386416282 1386516698 1386616305 1381116710 1498916134 1469816524 142716916 1386616305 1381116710 1498316524 142716916 1386616305 1381116710 1498715146 1469816524 142716916 1386616305 1381116710 1498715146 1459816527 1427816915 1386416332 1348916723 1449816529 1449715543 1429315924 1385416319 1348916723 1429315924 1385416319 13849816723 1449816550 1419716941 13848416322 1348916730 1429816165 1419716941 13836316339 1348116744 21 1498215178 1455215659 1419715643 1382416329 1349416744 21 1491815181 1491815181 1491815181 1491815181 1491815181 1491815181 1491815181 1391816359 134841674 147815994 1380816359 1348416771 19 1469415676 1477315994 1380816357 1348416771 19 1469415676 1478915994 1380816372 1345216787 1478915994 1380816372 1345216787 1478915994 1380816372 1345216787 1468815927 1467815994 1391816372 1345216787 1468815927 1467815996 1391816372 1345216787 1468815927 1467815999 1379416389 1346416782 1346816927 1467815999 1379416389 134681675 18 1498815927 1467815999 13794816382 134981678 17 1467815999 13794816382 134981678 17 1467815999 134581678 17 1467815999 134581678 17 1467815999 134581678 17 147815999 134581678 17 147815999 134581678 17 147815999 134581678 17 147815999 134581678 17 147815999 134581678 1349815927 1467815999 134581698 133981688 13 1347716999 134581698 133981 | 3 | 1501415089 | 1463915472 | 1427015862 | 1390816259 | 1355216662 | 27 |
| 1498615108 1482615492 1428215121 1498815151 1461415498 1426615888 1398416282 1352816689 25 6 1497615127 1489115151 1420015985 1387816292 1351718703 24 7 149815144 1458615517 1422715906 1386016319 1351718703 24 7 149815146 1458815524 142715916 1386016319 135181871 23 8 1495115163 1447715537 1420915928 1348416319 1349916723 22 8 1495115163 1447715557 1420915928 1348216325 1348316730 22 1498315165 1445615550 1419715941 1360616323 1348116744 21 10 1492615172 1445515563 1419715941 1362016325 1347016737 20 14921512 1445615560 1417315997 1381216366 1347816794 19 11 149131516 1445615570 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> | | | | | | | |
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| 6 1497615127 1460115511 1423315901 1387216299 1351716703 24 1469615134 1469615154 1422715908 1398616312 1351116710 23 1469615153 1469615524 1422715915 1398616312 1351116717 23 1487715146 1459815525 1421515217 1385616312 1399816717 23 1498415159 1457715537 1420915928 1394816325 1349816730 22 1449415159 1457015543 1420315934 1394216332 1349816730 22 1449815159 1459615550 1419115947 1383616339 1344616734 21 1452215172 1455615556 1419115947 1383616339 1344616744 21 1491815184 1454615596 1417915961 1381816352 1347016737 20 1491915184 1454615596 1417915961 1381816336 1345616771 19 1400715197 1453315555 1416715974 1380616372 1345216778 1489415210 1462115595 1416115980 1380016379 1344616786 18 1468615216 1462115595 1416115980 1380016379 1344616786 18 1468615216 1462115595 1416215980 1380016379 1344616786 18 1468615216 1462115595 1416215098 1379816398 1342816798 17 1468615216 1469815600 1414616000 1377816398 1342816798 17 1468615224 1449015627 1412416000 1377816398 1342816898 1344916898 17 1468515284 1448415281 1448415281 1448415281 1448615280 1448615680 1414816007 1377716406 1342316886 1448415281 1448415281 1448415281 1448415281 1448415281 1448415281 1448415281 1448415281 1448415281 1448415281 1448415281 1448415281 1448415281 1448415281 1448815289 1448815680 1448815680 1378816483 1338816880 1348816880 1348816880 1348816880 13488816880 13488816880 13488816880 13488816880 13488816880 13488 | 5 | | | | | | 25 |
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| 14 1487515229 1450315614 1413616007 1377716406 1342316812 16 15 1486915235 1449615621 1413016013 1377116413 1341716819 1341716819 1341716819 1341716819 1341716819 1341716819 1341716819 1341716819 1341716819 1340516833 15 16 1485015256 1447615640 1411816027 1375916426 1340516833 15 16 1485015256 1447815640 1411216033 1375316433 1340016839 14 17 1483815287 1446615683 1410016046 1374116446 1338816853 13 18 1482515280 1445315686 1409416053 1375316453 1337516880 13 1337516880 13 1337516480 1337616880 11 1481915282 1444715673 1408216066 1372316466 1337016874 1408216066 1372316493 14476915680 11 1477616473 1337116493 1336516894 10 1 | 13 | | | | | | 17 |
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| 17 | 16 | 1485015255 | 1447815640 | 1411216033 | 1375316433 | 1340016839 | 14 |
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| 19 1481915286 1444715673 1408216066 1372316486 1337016874 1336516880 11 19 1481315293 1444115679 1407616073 1371716473 1338516880 11 20 1480015306 1442915692 1406416086 1370516487 1335316894 10 21 1478815312 1442315699 1405816093 1369916493 1334716901 9 21 1478815318 1441715705 1405216099 1369416500 1334116908 9 1478215331 1440415718 1404016112 1368816507 1333616928 8 22 1477515331 1440415718 1404016112 1368216513 1333016922 8 23 1478315344 1439215731 1402816126 1367016527 1331816935 7 24 1475015357 1438015744 1401616139 1365816540 1330016949 6 25 1473815370 14368 | | В | | | | | |
| 19 1481315293 1444115679 1407616073 1371716473 1336516880 11 20 1480015306 1442815692 1406416086 1370516487 1335316894 10 20 1480015306 1442815692 1406416086 1370516487 1335316894 10 21 1478815318 1441715705 1405216099 1369416500 1334116908 9 21 1477515325 1441115712 1404616105 1368816507 1333616915 22 1477515331 1440415718 1404016112 1368216513 1333016922 8 23 1476915338 1439815725 1403416119 1367016527 1331816938 7 24 1475015357 1438615738 1402216132 1366416534 1331216942 7 24 1475015357 1438815754 1401616139 1365816540 1330616949 6 1473815376 1438815758 1400416152 | 18 | | | | | | 12 |
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| 1478215325 1441115712 1404616105 1368816507 1333616915 22 1477515331 1440415718 1404016112 1368216513 1333016922 8 1476915338 1439815725 1403416119 1367616520 1332416928 1 23 1476315344 1439215731 1402816126 1367016527 1331816935 7 1475715350 1438615738 1402216132 1366416534 1331216942 24 1475015357 1438015744 1401616139 1365816540 1330616949 6 1474415363 1437415751 1401016146 1365216547 1330116956 1 25 1473815376 1436815764 1399816159 1364016561 1328916970 5 26 1472515382 1435515771 1399216166 1363416567 1328316977 4 1471915395 1434915777 1398616172 1362816574 1327716983 | 20 | | | | | | 10 |
| 22 1477515331 1440415718 1404016112 1368216513 1333016922 8 23 1476915338 1439815725 1403416119 1367616520 1332416928 7 23 1476315344 1439215731 1402816126 1367016527 1331816935 7 1475715350 1438615738 1402216132 1366416534 1331216942 7 24 1475015357 1438015744 1401616139 1365816540 1330616949 6 1474415363 1437415751 1401016146 1365216547 1330116956 1329516963 5 25 1473815370 1436815758 1400416152 1364616554 1329516963 5 1473215396 1436215764 1399816159 1364016561 1328916970 4 26 1472515382 1435515771 1399216166 1363416567 1328316977 4 27 1471315395 1434315784 1398016179 1362816581 | 21 | | | | | | 9 |
| 23 1476915338 1439815725 1403416119 1367616520 1332416928 7 24 1475715350 1438615738 1402216132 1366416534 1331216942 6 24 1475015357 1438015744 1401616139 1365816540 1330616949 6 1474415363 1437415751 1401016146 1365816547 1330116956 136956 25 1473815370 1436815764 1399816159 1364616554 1329516963 5 26 1472515382 1435515771 1399216166 1363416567 1328316977 4 1471915389 1434915777 1398616172 1362816574 1327716983 1 27 1471315395 1434315784 1398016179 1362316581 1327216990 3 28 1470115408 1433115797 1396816192 1361116595 1326017004 2 28 1470115408 1433115797 1396816192 1361116595 < | 22 | | - | | | | - |
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| 25 1474415363 1437415751 1401016146 1365216547 1330116956 1329516963 5 1473815370 1436815758 1400416152 1364616554 1329516963 5 1473215376 1436215764 1399816159 1364016561 1328916970 5 26 1472515382 1435515771 1399816162 1363416567 1328316977 4 1471915389 1434915777 1398616172 1362816574 1327716983 3 27 1471315395 1434315784 1398016179 1362316581 1327716983 1327716990 3 1470715402 1433715790 1397416185 1361716588 1326616997 28 1470115408 1433115797 1396816192 1361116595 1326017004 2 29 1468815421 1431915810 1398616192 1359916601 1325417011 1 29 1468815427 1431315816 1395016212 </td <td>23</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>7</td> | 23 | | | | | | 7 |
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| 27 1471915389 1434915777 1398616172 1362816574 1327716983 1471315395 1434315784 1398016179 1362316581 1327216990 3 28 1470115408 1433115797 1396816192 1361116595 1326017004 2 1469415414 1432515803 1396216199 1365116601 1325417011 1325417011 29 1468815421 1431915810 1395616205 1359916608 1324817018 1 1468215427 1431315816 1395016212 1359316615 1324317025 1 30 1467615434 1430715823 1394416219 1358716622 1323717032 0 A B A B A B A B A B | | | | | | | |
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ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 47°30' | 48 [°] 00' | 48 ⁰ 30' | 49 [°] 00' | 49 ^O 30' | 1 |
|----|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|----------|
| | | | | | | |
| | A B 1323717032 | A B 1289317449 | A B 1255417873 | A B | A B 1189518746 | 30 |
| 1 | 1323117039 1322517045 | 1288717456 1288117463 | 1254917881 1254317888 | 1221618313 1221118320 | 1189018753 1188518760 | 29 |
| | 1322017052 | 1287617470 | 1253817895 | 1220518327 | 1187918768 | |
| 2 | 1321417059 1320817066 | 1287017477 1286417484 | 1253217902 1252617909 | 1220018335 1219518342 | 1187418775 1186818783 | 28 |
| 3 | 1320217073 1319617080 | 1285917491 1285317498 | 1252117916 1251517924 | 1218918349 1218418357 | 1186318790 1185818797 | 27 |
| 4 | 1319117087 | 1284717505 | 1251017921 | 1217818364 | 1185218805 | 26 |
| 5 | 1318517094 1317917101 | 1284117512 1283617519 | 1250417938 1249917945 | 1217318371 1216718378 | 1184718812 1184218820 | 25 |
| | 1317317108 | 1283017526 | 1249317952 | 1216218386 | 1183618827 | |
| 6 | 1316817114 1316217121 | 1282417533 1281917540 | 1248717959 1248217966 | 1215618393 1215118400 | 1183118834 1182518842 | 24 |
| 7 | 1315617128 | 1281317547 | 1247617974 | 1214518408 | 1182018849 | 23 |
| 8 | 1315017135 1314417142 | 1280717554 1280217561 | 1247117981 1246517988 | 1214018415 1213418422 | 1181518857 1180918864 | 22 |
| 9 | 1313917149 1313317156 | 1279617568 1279017576 | 1246017995 1245418002 | 1212918429 1212318437 | 1180418872 1179918879 | 21 |
| | 1312717163 | 1278517583 | 1244818010 | 1211818444 | 1179318886 | |
| 10 | 1312117170 1311617177 | 1277917590 1277417597 | 1244318017 1243718024 | 1211218451 1210718459 | 1178818894 1178218901 | 20 |
| 11 | 1311017184 | 1276817604 | 1243218031 | 1210218466 | 1177718909 | 19 |
| 12 | 1310417191 1309817198 | 1276217611 1275717618 | 1242618038 1242118045 | 1209618473 1209118481 | 1177218916 1176618924 | 18 |
| 13 | 1309317205 1308717212 | 1275117625 1274517632 | 1241518053 1241018060 | 1208518488 1208018495 | 1176118931 1175618939 | 17 |
| | 1308117218 | 1274017639 | 1240418067 | 1207418503 | 1175018946 | <u> </u> |
| 14 | 1307517225 1307017232 | 1273417646 1272817653 | 1239818074 1239318081 | 1206918510 1206318517 | 1174518953 1174018961 | 16 |
| 15 | 1306417239 1305817246 | 1272317660 1271717667 | 1238718089 1238218096 | 1205818525 1205318532 | 1173418968 1172918976 | 15 |
| 16 | 1305317253 | 1271117674 | 1237618103 | 1204718539 | 1172418983 | 14 |
| 17 | 1304717260 1304117267 | 1270617681 1270017689 | 1237118110 1236518117 | 1204218547 1203618554 | 1171818991 1171318998 | 13 |
| | 1303517274 | 1269517696 | 1236018125 | 1203118561 | 1170819006 | |
| 18 | 1303017281 1302417288 | 1268917703 1268317710 | 1235418132 1234918139 | 1202518569 1202018576 | 1170219013 1169719021 | 12 |
| 19 | 1301817295 1301217302 | 1267817717 1267217724 | 1234318146 1233818154 | 1201418583 1200918591 | 1169219028 1168619036 | 11 |
| 20 | 1300717309 | 1266617731 | 1233218161 | 1200418598 | 1168119043 | 10 |
| 21 | 1300117316 1299517323 | 1266117738 1265517745 | 1232718168 1232118175 | 1199818605 1199318613 | 1167619051 1167019058 | 9 |
| | 1299017330 | 1265017752 | 1231618182 | 1198718620 | 1166519066 | <u> </u> |
| 22 | 1298417337 1297817344 | 1264417760 1263817767 | 1231018190 1230518197 | 1198218627 1197618635 | 1166019073 1165419081 | 8 |
| 23 | 1297217351 1296717358 | 1263317774 1262717781 | 1229918204 1229318211 | 1197118642 1196618650 | 1164919088 1164419096 | 7 |
| 24 | 1296117365 | 1262217788 | 1228818219 | 1196018657 | 1163819103 | 6 |
| 25 | 1295517372 1295017379 | 1261617795 1261017802 | 1228218226 1227718233 | 1195518664 1194918672 | 1163319111 1162819118 | 5 |
| | 1294417386 | 1260517809 | 1227118240 | 1194418679 | 1162219126 | <u> </u> |
| 26 | 1293817393 1293217400 | 1259917816 1259317824 | 1226618248 1226018255 | 1193918686 1193318694 | 1161719133 1161219141 | 4 |
| 27 | 1292717407 1292117414 | 1258817831 1258217838 | 1225518262 1224918269 | 1192818701 1192218709 | 1160619148 1160119156 | 3 |
| 28 | 1291517421 | 1257717845 | 1224418277 | 1191718716 | 1159619163 | 2 |
| 29 | 1291017428 1290417435 | 1257117852 1256617859 | 1223818284 1223318291 | 1191218723 1190618731 | 1159019171 1158519178 | 1 |
| | 1289817442 | 1256017866 | 1222718298 | 1190118738 | 1158019186 | <u> </u> |
| 30 | 1289317449 A B | 1255417873 A B | 1222218306 A B | 1189518746 A B | 1157519193 A B | <u> </u> |
| | 132°00' | 131 [°] 30' | 131°00' | 130°30' | 130 [°] 00' | |
| | 132 00 | 131 30 | 131 00 | 130 30 | 130 00 | |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 1 | 1 . | i | I | 1 | |
|------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|----------|
| | 50°00' | 50°30' | 51°00' | 51 [°] 30' | 52 [°] 00' | |
| | A B | A B | . A B | A B | АВ | |
| 0 | 1157519193 1156919201 | 1125919649 1125419657 | 1095020113 | 1064620585 | 1034721066 | 30 |
| 1 | 1156419208 | 1124919664 | 1094520121 1093920128 | 1064020593 1063520601 | 1034221074 1033721082 | 29 |
| | 1155919216 | 1124419672 | 1093420136 | 1063020609 | 1033221090 | |
| 2 | 1155319223 1154819231 | 1123919680 1123319687 | 1092920144 | 1062520617 | 1032721098 | 28 |
| 3 | 1154310238 | 1122819695 | 1092420152 1091920160 | 1062020625 1061520633 | 1032221106 1031721114 | 27 |
| | 1153719246 | 1122319703 | 1091420167 | 1061020641 | 1031221122 | |
| 4 | 1153219253 1152719261 | 1121819710 1121319718 | 1090920175 1090420183 | 1060520649 1060020657 | 1030721131 1030221139 | 26 |
| 5 | 1152219269 | 1120719726 | 1089920191 | 1059520665 | 1029821147 | 25 |
| | 1151619276 | 1120219733 | 1089420199 | 1059020672 | 1029321155 | <u> </u> |
| 6 | 1151119284 1150619291 | 1119719741 1119219749 | 1088820207 1088320214 | 1058520680 1058020688 | 1028821163 1028321171 | 24 |
| 7 | 1150119299 | 1118719756 | 1087820222 | 1057520696 | 1027821179 | 23 |
| | 1149519306 | 1118119764 | 1087320230 | 1057020704 | 1027321187 | <u> </u> |
| 8 | 1149019314 1148519321 | 1117619772 1117119779 | 1086820238 1086320246 | 1056520712 1056020720 | 1026821195 1026321204 | 22 |
| 9 | 1147919329 | 1116619787 | 1085820254 | 1055520728 | 1025821212 | 21 |
| 10 | 1147419337 1146919344 | 1116119795 1115619803 | 1085320261 | 1055020736 | 1025321220 | |
| 10 | 1146419352 | 1115019810 | 1084820269 1084320277 | 1054520744 1054020752 | 1024821228 1024321236 | 20 |
| 11 | 1145819359 1145319367 | 1114519818 1114019826 | 1083820285 1083220293 | 1053520760 1053020768 | 1023921244 1023421252 | 19 |
| 12 | 1144819375 | 1113519834 | 1082720301 | 1052520776 | 1022921260 | 18 |
| 40 | 1144319382 | 1113019841 | 1082220308 | 1052020784 | 1022421269 | |
| 13 | 1143719390 1143219397 | 1112419849 1111919857 | 1081720316 1081220324 | 1051520792 1051020800 | 1021921277 1021421285 | 17 |
| 14 | 1142719405 | 1111419864 | 1080720332 | 1050520808 | 1020921293 | 16 |
| 15 | 1142119412 1141619420 | 1110919872 | 1080220340 | 1050020816 | 1020421301 | |
| 10 | 1141119428 | 1110419880 1109919888 | 1079720348 1079220356 | 1049620824 1049120832 | 1019921309 1019521318 | 15 |
| 16 | 1140619435 | 1109419895 | 1078720364 | 1048620840 | 1019021326 | 14 |
| 17 | 1140019443 1139519450 | 1108819903 1108319911 | 1078220371 1077720379 | 1048120848 1047620856 | 1018521334 1018021342 | 13 |
| | 1139019458 | 1107819918 | 1077220387 | 1047120864 | 1017521350 | |
| 18 | 1138519466 1138019473 | 1107319926 | 1076720395 | 1046620872 | 1017021358 | 12 |
| 19 | 1137419481 | 1106819934 1106319942 | 1076120403 1075620411 | 1046120880 1045620888 | 1016521367 1016021375 | 11 |
| | 1136919488 | 1105719949 | 1075120419 | 1045120897 | 1015521383 | |
| 20 | 1136419496 1135919504 | 1105219957 1104719965 | 1074620427 1074120435 | 1044620905 1044120913 | 1015121391 | 10 |
| 21 | 1135319511 | 1104219973 | 1073620442 | 1043620913 | 1014621399 1014121407 | 9 |
| | 1134819519 | 1103719980 | 1073120450 | 1043120929 | 1013621416 | |
| 22 | 1134319527 1133819534 | 1103219988 1102719996 | 1072620458 1072120466 | 1042620937 1042120945 | 1013121424 1012621432 | 8 |
| 23 | 1133219542 | 1102120004 | 1071620474 | 1041620953 | 1012121440 | 7 |
| - 24 | 1132719549 | 1101620012 | 1071120482 | 1041120961 | 1011621448 | |
| 24 | 1132219557 1131719565 | 1101120019 1100620027 | 1070620490 1070120498 | 1040620969 1040120977 | 1011221457 1010721465 | 6 |
| 25 | 1131119572 1130619580 | 1100120035 1099620043 | 1069620506 1069120514 | 1039620985 | 1010221473 | 5 |
| 26 | 1130119588 | 1099120050 | 1068620522 | 1039120993 1038621001 | 1009721481 | |
| | 1129619595 | 1098620058 | 1068120529 | 1038121009 | 1009221489 1008721498 | 4 |
| 27 | 1129119603 1128519611 | 1098020066 1097520074 | 1067620537 1067120545 | 1037621017 1037221025 | 1008221506 1007821514 | 3 |
| 28 | 1128019618 | 1097020082 | 1066620553 | 1036721033 | 1007321522 | 2 |
| | 1127519626 | 1096520089 | 1066120561 | 1036221042 | 1006821531 | |
| 29 | 1127019634 1126519641 | 1096020097 1095520105 | 1065620569 1065120577 | 1035721050 1035221058 | 1006321539 1005821547 | 1 |
| 30 | 1125919649 | 1095020113 | 1064620585 | 1034721066 | 1005321555 | 0 |
| | A B | A B | A B | А В | A B | _ |
| | 129°30' | 129 [°] 00' | 128 [°] 30' | 128 ⁰ 00' | 127°30' | |
| |] | , | | .25 00 | 127 30 | |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| S2 300 | | 0 | 0 | l . | 1 . | 1 , | 1 |
|--|----|----------------------|---------------------|---------------------|---------------------|---------------------|------------|
| 0 10063, 21655 | | 52 ⁰ 30′ | 53 ⁰ 00' | 53 [°] 30′ | 54 ⁰ 00' | 54 ⁰ 30' | l |
| 1 10049, 21653 976, 22079 9473, 22578 9195, 22095 8927, 22913 2010039, 21690 9776, 22079 9468, 22589 9195, 22095 8918, 22861 2010039, 21696 9741, 22096 9459, 22696 9181, 22123 8990, 22864 2010039, 21696 9774, 22096 9459, 22696 9181, 22123 8990, 22864 2010039, 21696 9772, 22112 9448, 22612 9177, 22130 9900, 22866 27 201015, 21611 9727, 22112 9449, 22632 9172, 22139 9000, 22866 27 201015, 21611 9727, 22129 9440, 22830 9163, 23146 8991, 22884 916010, 21629 9722, 22129 9440, 22830 9163, 23146 8991, 22884 9163, 23165 8991, 22884 91600, 21689 9772, 22120 9440, 22883 9163, 23165 8991, 22884 916000, 21689 9773, 22146 9431, 22865 9164, 23174 8882, 23702 24884 91690, 21682 9773, 22143 9445, 22884 91690, 21682 9773, 22143 9445, 22884 91690, 21682 9773, 22143 9445, 22884 91690, 21682 9773, 22143 9447, 22881 9160, 23193 8877, 22712 24 9900, 21682 9773, 22143 9447, 22881 9160, 23193 8877, 22712 24 9900, 21682 9773, 22143 9447, 22881 9140, 23200 8864, 22738 23 9888, 22775 9886, 22784 9906, 22163 9447, 22888 9193, 23200 8864, 22738 23 9906, 22760 9906, 22203 9864, 22738 9906, 22760 9906, 22060 9906, 22203 9864, 22734 9168, 23203 8865, 22756 9906, 22760 9906, 22203 9868, 22774 9906, 22774 9975, 22213 9994, 22744 9174, 2277 9875, 22213 9994, 22744 9174, 2277 9875, 22213 9994, 22744 9174, 22888 8977, 22771 9875, 22213 9994, 22744 9174, 22884 9174, 22888 9174, 22885 9174, 22888 9174, 22888 9174, 22888 9174, 22888 9174, 22888 9187, 22779 9864, 22779 9864, 22779 9864, 22779 9864, 22779 9865, 22276 9865, 22776 9867, 22283 9867, 22786 9867, 22283 9868, 22775 9864, 22784 9868, 22779 9864, 22784 9868, 22779 9868, 22779 9868, 22779 98694, 22784 9868, 22779 98694, 22888 9877, 22871 9879, 22888 9877, 22871 9879, 22888 9877, 22871 9879, 22888 987 | - | | | | | A B | <u> </u> |
| 1 10044_21572 9758_22070 947325587 919623095 8822_22822 29 10034_21586 975122097 946825587 919623113 8818_22840 28 10029_21596 974122098 9458_22585 919623113 8818_22840 28 10024_21505 97372104 94542812 917723130 880023646 27 10019_21613 97372104 94542812 917723130 880023646 27 10019_21613 97322112 9449_252821 917223130 880023646 27 10010_21629 97322112 944525830 918623146 889623647 26 10010_21629 972221219 944525830 918623146 889623647 26 10010_21629 972221219 944525830 918623146 889623647 26 10000_21646 97182138 945525638 918623146 889623647 26 10000_21646 97382138 945525647 919623145 888623693 25 10000_21646 97382138 94552565 916423174 888223790 27 10019_21612 977322141 944525830 918623156 888623693 25 10000_21646 973821246 943625654 914923133 8877_23711 947 998621672 98892171 941725891 914023330 886423720 98862172 98842180 941725890 918623200 886623729 23 8997821627 989822171 941725891 914023320 886622738 23 8997821627 989822179 945722219 945725280 918623228 885023774 99682172 99682172 968622727 945823277 918623228 885622775 99682172 9967522213 939422770 918623228 885623774 99682172 996822729 986822772 986822774 986822279 986822773 986822774 986822279 986822779 986822779 986822779 986822779 986822779 986822779 986822779 986822779 986822779 986822779 986822779 986822779 987922879 987922779 986822779 986822779 987922879 987922779 987922899 987922899 987922899 9879822899 987922899 98798 | 0 | | | | | | 30 |
| 2 | 1 | | | | | | 29 |
| 3 1002921966 97422069 494928061 911123122 880023645 27 1001921613 973222112 944828261 917223139 880023655 27 1001921613 973222112 944828261 917223139 880023655 27 1001921613 973222119 944528380 916823166 8891228275 26 1000021639 972222129 944025380 916323166 889122863 971822139 945824247 918623165 889222893 25 1000021646 971322146 94312655 915423174 882823893 25 1000021646 971322146 94312655 915423174 882823993 25 1000021646 971322146 94312655 915423174 882823993 25 1000021647 99802162 970322149 94512672 914523191 94722270 989021679 989021671 9417226894 914623191 94722270 989021679 989021679 98942180 941226890 913823299 88942273 22 98942719 997121696 98942189 941226890 913823299 889622747 9771 | | 1003921580 | 975122079 | 946822587 | 919023104 | 891823631 | |
| 3 1002421605 107322104 945422621 917723130 89042265 27 1001921613 973222112 944922621 917223139 890022656 27 1001521621 972222129 944026539 916323146 89812264 27 1001021628 972222129 944026539 916323146 89812264 97 1000021646 973122188 94552647 915423155 988222647 9703 | 2 | | | | | | 28 |
| 10019_1613 9732_22121 9449_22821 9172_22139 8900_22867 26 | 3 | | | | | | 27 |
| 5 1001021629 97222129 97402538 914523156 888123689 25 1000021646 971322146 94312565 915423174 888223702 25 1000021646 971322146 94312565 915423174 888223702 25 1000021646 971322163 94212872 9154523183 887723711 24 992021692 970322163 94212872 915523702 989321692 916922169 94122872 914523181 887723712 24 989321679 989322160 94122890 914033300 989323728 23 989321679 98942160 94122890 915622290 98942773 22 989522179 940728988 913132318 889923747 22 989522179 968522209 989422177 94072724 917132346 98642373 21 957522213 939427724 911732345 98652373 987522213 939427724 911732345 98652373 98652274 93752724 911923252 884223732 20 98952774 966522249 93892274 910632307 883323800 19 99472174 996522247 93752758 996923729 885823739 19 99472174 996522247 93752758 996923739 885823810 19 99472174 996522247 93752758 996923739 885823810 19 99472174 996522264 93662275 909923279 885823810 19 99472174 996522264 93662275 909923279 885823810 10 993721754 986722264 93662275 909923279 885823810 10 993721754 986722264 93662275 90992325 88592381 10 993721754 996722264 93662275 90992325 88592381 10 993721754 996722264 93662276 909923275 88592381 10 993721754 996922269 93682775 909423288 88592381 10 99372180 993722288 93592276 90992329 88592381 10 99372381 10 99372381 10 99372381 10 99372381 10 99372381 10 99372381 10 99372381 10 99372381 10 99372381 10 99372381 10 99372381 10 99382382 93882382 93882381 938 | | 1001921613 | 973222112 | 944922621 | | | |
| 5 1000521638 971822146 9491822816 888623802 25 | 4 | | | | 916823148 | | 26 |
| 1000021646 971322166 943122865 915423174 888223702 1 | 5 | | | | | | 25 |
| 7 999021662 970322163 94212872 914523191 887323720 23 989621679 999921679 999422100 941222880 915823200 888623728 23 997521687 998922170 941222880 915823209 888623728 23 997721686 986422197 940322707 912523226 885823725 998521729 980522205 939822715 912523226 885823725 21 998521729 987522121 959822724 911723244 884623773 91262321 9126 | | | | | | | |
| 7 996621671 969922171 941722681 91402200 686423738 23 96942180 941222690 915823209 686423738 25 96942180 941222690 915823209 686423738 25 9772180 94032707 912632268 685823747 22 957121666 969422197 94032707 912632268 85523754 21 99722180 96962213 94032707 912632258 85523764 21 998221712 9665222213 959822724 911723244 88462373 85523764 21 998221712 967022222 938922724 911323252 884223782 20 985221729 966522239 938422741 910823261 883723761 19 947221737 966122239 938922759 910423270 833323800 19 933421745 965522239 938922759 909823279 8282823809 19 993321762 965722247 937522767 909432288 862423818 18 993321770 964222272 936522767 909632331 861823827 963323775 964722264 938622775 909632314 861823827 963722258 937622784 906833314 861823826 17 993321776 963222288 935222801 907823331 860823845 16 990421819 9682822239 934422818 906823314 861823845 16 990421819 968822215 933822826 907823331 860823845 16 990421819 968822215 933822826 907823340 679723881 15 990421819 968822315 933822826 907823340 679723880 17 989821819 968822315 933822826 905823340 879823880 17 989821819 968823257 935822826 905823340 879823880 18 989921829 969023240 932422818 906823340 879823880 17 989821829 9699 | 6 | 999521654 | 970822154 | 942622664 | 914923183 | 887723711 | 24 |
| 996121679 969422180 941222800 913823209 886423738 997721687 996922188 940722888 913123218 865823747 22 997721686 969422197 940322705 912632226 865823755 996821714 968022205 939822715 912632226 865823753 912632226 865823753 912632226 836923734 21 969521729 967522121 959722722 938922732 911323222 884223721 10 996721720 967022220 938922732 911323222 884223729 948223737 946122339 938023750 910423270 823323809 19 947221737 966122239 938922750 910423270 823323809 19 9978233323809 19 9978233323809 19 9978233323809 19 9978233323809 19 9978233323809 19 997823333 80802375 808323305 818123827 13 992321752 964722264 936822757 90942288 861923826 17 997833333 80802384 16 997833333 80802384 16 997833333 80802384 16 997833333 80802384 16 997833334 861023845 17 996322289 934722810 907623331 860023844 16 999921829 962322289 934722810 90763333 860023845 16 999921829 969921829 969921829 969922886 878323889 14 968922888 96892388 878823888 17 989921829 969922881 969923888 878823888 18 98892384 969923888 9789 | 7 | | | | | | 22 |
| 997121696 968422197 940322707 912823226 865523755 2912822219 966621719 967522219 939422714 911723244 884623773 210 996521720 967522213 939422724 911723244 884623773 210 996521729 966522230 938422741 910823265 884223782 20 93642271 906521737 966122230 938422750 910423261 833723782 21 9942 | | | | | | | 23 |
| 9 996621704 968022213 993822715 912223234 884623773 10 995721720 967022212 993822732 911323252 884223782 20 985221729 96652239 938422741 910823251 883723761 995521729 96652239 938422781 910823261 883723761 994221745 965622239 938922788 90992279 882823809 19 984221745 96562247 937522788 90992279 882823809 19 984221745 96562247 937522788 90992279 882823809 19 994221762 964722264 936822775 900032386 88192387 17 983321762 964722264 936822775 900032396 88192387 17 982321778 963722281 935622781 900032396 88192387 17 982321778 963722281 935622781 900032393 881623836 17 995321787 963222289 935222801 907523331 880623845 17 995921803 996921803 962322306 934222816 900723331 880023845 16 990021803 962322306 934222816 900723331 800023845 16 990021803 962322306 934222816 900723340 879723817 15 990421802 961422323 933322807 90032349 879223810 17 986921803 960922340 932422816 900723340 879723817 15 990421803 960922340 932422816 900523354 879823898 11 987022845 900922340 932422816 900523355 878823889 11 987022845 900922340 932422816 900523965 900523965 900923965 900923965 900923965 900923965 900923965 900923965 900923965 900923965 900923965 90092396 900923965 90092396 90092399 90092399 90092399 90092399 90092399 90092399 90092399 900923 | 8 | 997621687 | 968922188 | 940722698 | 913123218 | 885923747 | 22 |
| 99622172 | 9 | | | | | | 21 |
| 11 994721729 966522290 9394227750 10423270 8833233900 19 994721745 965622247 937522758 909923279 8833233900 19 994721745 965622247 937522758 909923279 882823390 19 993721754 965622256 937022767 909423286 882423818 18 933321705 99472264 994722775 909923296 881923827 13 992821770 964222224 935622775 909623314 881023845 17 992821767 963722281 935622793 906123314 881023845 17 992821795 962822289 935222801 907623331 880123845 16 991321795 962822288 934722810 907723331 880123863 890923863 990421812 961822315 933822827 906323349 679223871 15 990421812 961822315 933822827 906323349 678223880 16 996921820 961422323 933322836 905623356 678823880 17 986821837 960422340 932422813 904423384 677823897 988921827 960422340 932422815 904423384 677923907 13 985821845 959922349 931922862 904423393 877023925 12 986521878 959922366 931022879 903523400 676623943 11 987021878 959922367 931522879 903523400 676623943 11 986521878 959922361 930122879 903523419 875723952 12 996521878 95812391 9292 | | | | | | | - ' |
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| 12 993721754 965622247 937522758 909923279 882823809 12 993721754 965122266 937022767 909423288 862423818 18 993321770 964222272 936122775 9099232305 881523837 992821770 964222272 936122784 908523305 881523836 17 993021787 963722281 9356227801 907623323 880623854 16 991321795 962822298 934722810 907623331 880123863 15 990921801 962822306 934222818 906723331 880123863 15 990421812 961822315 933822867 906323349 879223871 15 990421812 961822315 933822844 905423386 878823889 14 988921820 961422323 93332286 905423358 878823899 14 988921837 960422340 93242285 9044233375 877923907 13 988921837 960422340 932422885 9044233375 877923907 13 987021853 959522357 931522870 904023393 877023916 18 988021863 959922385 931922886 904423393 877023925 12 98702187 958522357 931522870 904023393 877023925 12 986521878 9595122391 929622995 902823419 875723943 11 987021879 958122382 930122886 902823419 875723943 11 988021895 957522391 929622993 900423348 875823970 986521895 957522391 929622993 900423428 875823997 986521895 957522391 929622993 900423428 875823997 986521895 955222391 900823446 874323970 986521895 955222391 929622993 900423483 873823970 986521895 955322455 922822931 900423483 873823997 9 986521895 955822455 922822931 900423483 873823 | 11 | | | | | | 10 |
| 993321762 996422284 936622775 990923965 881923827 1770 996221770 964222872 936122793 9008123315 881523836 17 992321778 963222281 935622793 9008123315 881523836 17 991321787 963222280 935222801 907623322 880623854 16 991321787 963222280 935222801 907623322 880623854 16 991321787 963222306 934222810 907623340 879723871 15 990921812 961822315 933022826 906523349 879723871 15 990921812 961822315 933322836 905823349 879723871 15 980921828 96192332 932922844 905423395 878823898 14 988921828 96092332 932922844 905423395 878323898 14 988921828 960922332 932922844 905423395 877823896 13 988521845 959922367 931522802 904423337 877923916 13 975721862 95092356 950522357 931522807 904423338 877023916 19 987021870 956522374 930522879 903523402 878623934 11 987521878 959122382 930122879 903523419 877523965 11 986521878 956122382 930122897 903523419 875723961 10 966521878 956122390 929922913 901723419 875223961 10 966621895 955722396 922822913 901723419 875823979 984621912 9566222416 928222331 900023446 874823979 984621912 9566222416 92822231 901323446 874823979 9851 | | | | | | | '" |
| 13 992821770 964222272 936122794 908523305 881523895 17 992321778 963722281 935622793 908123314 861023845 16 991821787 962822298 934722810 907623323 880023845 16 990921803 962322298 934722810 907223331 880123863 15 990921803 962322306 934222810 907223331 860123863 15 990921812 961822315 933822827 906323349 679723871 15 990921812 961422323 933322836 906823358 678823889 14 989921828 960922332 932922844 905423365 878323888 989421828 960922349 932922843 904923375 877923907 13 988521845 959022349 931922862 904423384 877523916 987521802 959022349 931922862 904423384 877523916 987521870 98582374 930522877 903123400 876623934 11 9886 | 12 | 993721754 | 965122256 | 937022767 | 909423288 | 882423818 | 18 |
| 992321778 963722281 935622793 908123314 881023845 16 991821787 963222288 395222810 907623323 880623854 16 991321795 962822296 934722810 907223331 880623854 16 991321795 962822296 934722810 907223331 880623851 15 990921803 962322306 934222817 906323340 879723871 15 990921802 961822315 933822827 906323349 879223880 14 989421828 960922323 932822895 906823356 878823889 14 989421828 960922340 932422833 904923375 877823888 179 988921837 980422340 932422833 904923375 877923907 13 985821857 980922346 931922862 904423338 477523916 18 988021853 959522366 93102879 903523402 876623934 19 987521862 959022366 93102879 903523402 876623934 11 98672187 98652187 986522374 930522887 903523402 876623943 11 986521878 957822382 930122889 902623419 875723965 12 986521878 957822391 929622905 90222348 975723965 10 986823174 930522889 902623419 875723916 10 986521879 956222391 929622905 902223428 875823911 10 986521903 956622319 929222905 902823446 875823979 986521903 956622408 9267 | 13 | | | | | | |
| 15 990321795 96282298 934722810 907223331 880123863 990821812 961822315 951822315 951822315 990823184 879223861 15 990821812 961822315 933822827 906323349 879223861 16 989921820 961422323 933322836 905823358 878823888 14 9894 | | | | | | | 17 |
| 15 9904 21802 9618 22315 9338 22827 9653 23349 8797 23871 15 | 14 | 991821787 | 963222289 | 935222801 | 907623323 | 880623854 | 16 |
| 990421812 961822315 933822827 906323349 879223880 | 15 | | | | | | 45 |
| 17 9894 21828 9609 22332 9329 22844 9054 23366 8783 23898 9889 21837 9604 22340 9324 22853 9049 23375 8779 23907 13 9885 21845 9599 22349 9319 22865 9044 23384 8775 23916 18 9880 21853 9595 22357 9315 22870 9040 23393 8770 23925 12 9875 21862 9590 22366 9310 22879 9035 23402 8766 23934 11 9870 21870 9585 22382 9301 22887 9031 23410 8761 23943 11 9870 21878 9581 22382 9301 22889 9026 23419 8755 23961 10 9865 21878 9581 22382 9301 22896 9026 23419 8757 23952 20 9961 21887 9576 22391 9296 22905 9022 23428 8752 23961 10 9656 21895 9571 22399 9292 22913 9017 23437 8748 23970 9846 21912 9562 22416 9282 22931 9008 23446 8733 23988 23982 21912 9562 22445 9262 22931 9008 23446 8733 23988 23982 21937 9548 22442 9269 22957 8995 23446 8733 23988 23982 21937 9544 22442 9269 22957 8995 23446 8730 24006 23832 21937 9544 22442 9269 22957 8995 23441 8726 24015 79827 21945 9543 22450 9264 22965 8990 23490 8721 24024 24042 24042 24042 22665 8990 23490 8721 24024 24042 2404 | 13 | | | | | | 15 |
| 17 | 16 | 989921820 | 961422323 | 933322836 | 905823358 | 878823889 | 14 |
| 9885 21845 9599 22349 9319 22882 9044 23384 8775 23916 | 17 | | | | | | 40 |
| 987521862 959022366 931022879 903523402 876623934 19 987021870 958522374 930522887 903123410 875123943 11 986521878 958122382 930122896 902623419 875723952 12 986121887 957622391 929622905 902223428 875223961 10 985621895 957122399 929222913 901723437 874823970 936521893 956622408 928722922 901323446 874323979 9364621912 956222416 928222931 900823454 873923988 984621912 956222416 928222931 900823454 873923988 983721928 955222433 927322948 899923472 873024006 898321937 954822442 9269 | '' | | | | | | 13 |
| 19 987021870 958522374 930522887 903123410 876123943 11 986521878 958122382 930122896 902623419 875723952 1 929623419 875723952 1 929623419 875723952 1 929623419 875723952 1 986121887 957622391 929622905 902223428 875223961 10 986521895 957122399 929222913 901723437 874823970 986621903 956622408 926722922 901332446 874323979 9 9 929222913 900823446 874323979 9 9 924621912 956222416 928222931 900823454 873923988 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 | 18 | 988021853 | 959522357 | 931522870 | 904023393 | 877023925 | 12 |
| 986521878 958122382 930122896 902623419 875723952 20 986121887 957622391 929622905 902223428 875223961 10 986521895 957122399 928222913 901723437 874823970 985621903 956622408 928722922 901333446 874323979 9 984621912 956222416 928222931 900823454 873923988 | 10 | | | | | | |
| 21 985621895 957122399 929222913 901723437 874823970 985823970 98562408 928722922 901323446 874323979 9 22 984121920 955722425 927822939 900423463 873423997 8 23 983721928 955222433 927822936 899523472 873024006 7 24 982721945 954422450 926422965 899023490 872124024 872624015 7 24 982221953 953822450 926422965 899023490 877124033 6 25 981321970 952922467 925522983 898123507 871224024 26 980321970 952922476 925522991 897623516 870824051 5 25 981321970 952922476 9250 | | | | | | | 11 |
| 21 985121903 956622408 928722922 901323446 874323979 9 22 984421920 955722425 927822939 900423463 873423997 8 23 983721928 955222433 927322948 899923461 872624015 7 982721945 954322450 926422955 899923490 872124024 24 9822 | 20 | 986121887 | 957622391 | 929622905 | 902223428 | 875223961 | 10 |
| 984621912 956222416 928222931 900823454 873923988 22 984121920 955722425 927822939 900423463 873423997 8 983721928 955222433 9273 | 21 | | | | | | |
| 22 984121920 955722425 927822939 900423463 873423997 8 983721928 955222433 927322948 899923472 873024006 7 983721945 954822442 926922957 899523481 872624015 7 982721945 9543 | | | | | | | 9 |
| 23 983721928 955222433 927322948 899923472 873024006 983221937 954822442 926922957 899523481 872624015 7 982721945 9954322450 926422965 899023490 872124024 24 982221953 953822459 925922974 898523498 871724033 6 981821962 953422467 925522983 898123507 871224042 25 981321970 952922476 925522981 897623516 870824051 5 980821978 952422484 924623000 897223525 870324060 26 980321987 952022493 924123009 896723524 869924069 4 979821995 951522501 923623017 896323543 869424078 979422003 951022510 923623017 896323543 869924087 3 976922012 950522519 922723035 895423560 866624086 28 976422020 950522519 922723035 895423560 866624096 29 977522029 949622507 922323052 894523569 866124105 2 977922029 949622536 921823052 894523569 866124105 2 977922045 948722553 920923061 894023587 867724114 977022045 948722553 920923069 893623596 866824132 30 976522054 948222561 920423078 893123605 866324141 0 | 22 | 984121920 | 955722425 | 927822939 | 900423463 | | 8 |
| 982721945 954322450 92642265 899023490 872124024 24 982221953 953822459 925922974 898523498 871724033 6 981821962 953422467 925522983 8981123507 871224042 25 981321970 952922476 925022991 897623516 870824051 5 980821978 952422484 924623000 897223525 870324060 26 980321987 952022493 924123009 896723534 869924069 4 979821995 951522501 923623017 896323543 869424078 27 979422003 951022510 923223026 895823551 869024087 3 978922012 950522519 922723035 895423560 868624096 28 978422020 950122527 922323043 894923569 868124105 2 977922029 949622536 921823052 894523578 867724114 29 977522037 949122544 921323061 894023587 867724114 29 977522037 949122544 921323061 894023587 867724114 29 977522037 949122544 921323061 894023587 867224123 1 977022045 948722553 920923069 893623596 866824132 30 976522054 948222561 920423078 893123605 866324141 0 | 23 | | | | | | - |
| 24 982221953 953822459 925922974 898523498 871724033 6 981821962 953422467 925522983 898123507 871224042 871224042 6 25 981321970 952922476 925022991 897623516 870824051 5 980821978 952422484 924623000 897223525 870324060 870824060 26 980321987 952022493 924123009 896723534 869924069 4 27 979821995 951522501 923623017 896323551 869024078 3 9789 | | | | | | | ′ |
| 25 981821962 953422467 925522983 898123507 871224042 981821970 952922476 925022991 897623516 870824051 5 980821978 952422484 924623000 897223525 870324060 5 26 980321987 952022493 924123009 896723534 869924069 4 9798 | 24 | 982221953 | 953822459 | 925922974 | | | 6 |
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| 26 980321987 952022493 924123009 896723534 869924069 4 979821995 951522501 923623017 896323543 869424078 3 27 979422003 951022510 923223026 895823551 869024087 3 978922012 950522519 922723035 895423560 868624096 868624096 28 978422020 950122527 922323043 894923569 868124105 2 977922029 949622536 921823052 894523578 867724114 2 29 977522037 949122544 921323061 894023587 867224123 1 977022045 948722553 920923069 893623596 866824132 1 30 9765 | 20 | | | | | | l ° |
| 27 979821995 951522501 923623017 896323543 869424078 3 979422003 951022510 923223026 895823551 869024087 3 978922012 950522519 922723035 895423560 868624096 28 978422020 95012527 922323043 894923569 868124105 2 9779 | 26 | 980321987 | 952022493 | 924123009 | | | 4 |
| 978922012 950522519 922723035 895423560 866624096 28 978422020 950122527 922323043 894923569 868124105 2 977922029 949622536 921823052 894523578 867724114 29 977522037 949122544 921323061 894023587 867224123 1 977022045 948722553 920923069 893623596 866824132 30 976522054 948222561 920423078 893123605 866324141 0 A B A B A B A B A B A B A B | 27 | | 951522501 | 923623017 | 896323543 | 869424078 | |
| 28 978422020 950122527 922323043 894923569 868124105 2 977922029 949622536 921823052 894523578 867724114 921323061 894023587 867224123 1 29 977522037 949122544 921323061 894023587 867224123 1 977022045 948722553 920923069 893623596 866824132 30 976522054 948222561 920423078 893123605 866324141 0 A B A B A B A B A B | 21 | | | | | | 3 |
| 29 977922029 977522037 977022045 949622536 949122544 949122544 921323061 921323061 894023587 893623596 867724114 867224123 893623596 1 30 976522054 948222561 948222561 920423078 920423078 893123605 893123605 866324141 866324141 0 A B A B A B A B | 28 | | | | | | 2 |
| 977022045 948722553 920923069 893623596 866824132 30 976522054 948222561 920423078 893123605 866324141 0 A B A B A B A B A B | | | 949622536 | 921823052 | 894523578 | 867724114 | |
| 30 976522054 948222561 920423078 893123605 866324141 0 A B A B A B A B A B A B | 29 | | | | | | 1 |
| A B A B A B A B | 30 | | | | | - | 0 |
| | | | | | | | Ť |
| 125 00' | | 127 ⁰ 00' | | | | | |
| | | 127 00 | 120 30 | 120 00 | 125 30" | 125 00' | |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 55°00' | 55°30' | 56°00' | 56°30' | 57 [°] 00' | 1 |
|----|-------------------------|------------------------|------------------------|------------------------|------------------------|----|
| | А В | А В | A B | A B | A B | |
| 0 | 866324141 865924150 | 840124687 839624696 | 814325244 813825253 | 788925811 788525821 | 764126389 763726399 | 30 |
| 1 | 865524159 865024168 | 839224706 838824715 | 813425263 813025272 | 788125830 787725840 | 763326409 762926418 | 29 |
| 2 | 864624177 | 838324724 | 812525281 | 787325849 | 762426428 | 28 |
| 3 | 864124186 863724195 | 837924733 837524742 | 812125291 811725300 | 786825859 786425868 | 762026438 761626447 | 27 |
| | 863324204 | 837024752 | 811325309 | 786025878 | 761226457 | |
| 4 | 862824213 862424222 | 836624761 836224770 | 810825319 810425328 | 785625887 785225897 | 760826467 760426477 | 26 |
| 5 | 861924231 861524240 | 835724779 835324788 | 810025338 809625347 | 784825907 784325916 | 760026486 759626496 | 25 |
| 6 | 861124249 860624258 | 834924798 834424807 | 809225356 808725366 | 783925926 783525935 | 759226506 758826516 | 24 |
| 7 | 860224267 859724276 | 834024816 833624825 | 808325375 807925385 | 783125945 782725954 | 758426526 | 23 |
| 8 | 859324286 | 833124835 | 807525394 | 782325964 | 757926535 757526545 | 22 |
| 9 | 858924295 858424304 | 832724844 832324853 | 807025403 806625413 | 781825974 781425983 | 757126555 756726565 | 21 |
| | 858024313 | 831824862 | 806225422 | 781025993 | 756326574 | |
| 10 | 857524322 857124331 | 831424872 831024881 | 805825432 805325441 | 780626002 780226012 | 755926584 755526594 | 20 |
| 11 | 856724340 856224349 | 830524890 830124899 | 804925451 804525460 | 779826022 779326031 | 755126604 754726614 | 19 |
| 12 | 855824358 | 829724909 | 804125469 | 778926041 | 754326623 | 18 |
| 13 | 855324367 854924376 | 829224918 828824927 | 803625479 803225488 | 778526051 778126060 | 753926633 753526643 | 17 |
| 14 | 854524385 854024395 | 828424936 828024946 | 802825498 802425507 | 777726070 777326079 | 753126653 752626663 | 16 |
| 15 | 853624404 853124413 | 827524955 827124964 | 802025517 | 776926089 | 752226672 | |
| | 852724422 | 826724973 | 801525526 801125536 | 776426099 776026108 | 751826682 751426692 | 15 |
| 16 | 852324431 851824440 | 826224983 825824992 | 800725545 800325554 | 775626118 775226128 | 751026702 750626712 | 14 |
| 17 | 851424449 851024458 | 825425001 824925011 | 799825564 799425573 | 774826137 774426147 | 750226722 749826731 | 13 |
| 18 | 850524467 | 824525020 | 799025583 | 774026157 | 749426741 | 12 |
| 19 | 850124477 849624486 | 824125029 823725038 | 798625592 798225602 | 773626166 773126176 | 749026751 748626761 | 11 |
| | 849224495 | 823225048 | 797725611 | 772726185 | 748226771 | |
| 20 | 848824504 848324513 | 822825057 822425066 | 797325621 796925630 | 772326195 771926205 | 747826781 747426790 | 10 |
| 21 | 847924522 847524531 | 821925076 821525085 | 796525640 796125649 | 771526214 771126224 | 747026800 746626810 | 9 |
| 22 | 847024540 8466 24550 | 821125094 | 795625659 | 770726234 | 746226820 | 8 |
| 23 | 846624550 846124559 | 820725104 820225113 | 795225668 794825678 | 770226244 769826253 | 745826830 745326840 | 7 |
| 24 | 845724568 845324577 | 819825122 819425132 | 794425687 794025697 | 769426263 769026273 | 744926850 744526860 | 6 |
| 25 | 844824586 844424595 | 818925141 818525150 | 793525706 793125716 | 768626282 | 744126869 | |
| | 844024605 | 818125160 | 792725725 | 768226292 767826302 | 743726879 743326889 | 5 |
| 26 | 843524614 843124623 | 817725169 817225178 | 792325735 791925744 | 767426311 767026321 | 742926899 742526909 | 4 |
| 27 | 842724632 842224641 | 816825188 816425197 | 791425754 791025763 | 766526331 766126340 | 742126919 741726929 | 3 |
| 28 | 841824650 | 816025206 | 790625773 | 765726350 | 741326939 | 2 |
| 29 | 841424660 840924669 | 815525216 815125225 | 790225782 789825792 | 765326360 764926370 | 740926949 740526958 | 1 |
| | 840524678 | 814725234 | 789325801 | 764526379 | 740126968 | |
| | 840124687 A B | 814325244 A B | 788925811 A B | 764126389 | 739726978 | 0 |
| | 124°30' | | | A B | A B | |
| | 124 30 | 124 ⁰ 00' | 123 [°] 30′ | 123 ⁰ 00' | 122 ⁰ 30′ | |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 57 [°] 30′ | 58 [°] 00' | 58°30' | 59 [°] 00' | 59°30' | 1 |
|----|------------------------|------------------------|------------------------|------------------------|------------------------|----------------|
| | A B | А В | A B | A B | A B | 1 |
| 0 | 739726978 739326988 | 715827579 715427589 | 692328191 692028202 | 669328816 669028827 | 646829453 646429464 | 30 |
| 1 | 738926998 738527008 | 715027599 714627609 | 691628212 691228222 | 668628837 668228848 | 646029475 645729485 | 29 |
| 2 | 738127018 | 714227619 | 690828233 | 667828858 | 645329496 | 28 |
| 3 | 737727028 737327038 | 713827630 713427640 | 690428243 690028253 | 667428869 667128879 | 644929507 644629517 | 27 |
| | 736927048 | 713027650 | 689628264 | 666728890 | 644229528 | |
| 4 | 736527058 736127068 | 712627660 712227670 | 689228274 688928284 | 666328900 665928911 | 643829539 643429550 | 26 |
| 5 | 735727078 | 711827680 | 688528295 | 665528921 | 643129560 | 25 |
| | 735327088 | 711527690 | 688128305 | 665228932 | 642729571 | <u> </u> |
| 6 | 734927098 734527107 | 711127701 710727711 | 687728315 687328326 | 664828942 664428953 | 642329582 642029593 | 24 |
| 7 | 734127117 | 710327721 | 686928336 | 664028964 | 641629604 | 23 |
| 8 | 733727127 733327137 | 709927731 709527741 | 686528346 | 663728974 | 641229614 640929625 | 22 |
| 0 | 732927147 | 709127751 | 686228357 685828367 | 663328985 662928995 | 640529636 | 1 |
| 9 | 732527157 732127167 | 708727761 708327772 | 685428378 685028388 | 662529006 662229016 | 640129647 639729657 | 21 |
| 10 | 731727177 | 707927782 | 684628398 | 661829027 | 639429668 | 20 |
| | 731327187 | 707527792 | 684228409 | 661429038 | 639029679 | |
| 11 | 730927197 730527207 | 707127802 706827812 | 683928419 683528429 | 661029048 660729059 | 638629690 638329701 | 19 |
| 12 | 730127217 | 706427823 | 683128440 | 660329069 | 637929711 | 18 |
| 13 | 729727227 729327237 | 706027833 705627843 | 682728450 682328461 | 659929080 659529091 | 637529722 637229733 | 17 |
| | 728927247 | 705227853 | 681928471 | 659129101 | 636829744 | |
| 14 | 728527257 728127267 | 704827863 704427874 | 681528481 681228492 | 658829112 658429122 | 636429755 636129766 | 16 |
| 15 | 727727277 | 704027884 | 680828502 | 658029133 | 635729776 | 15 |
| | 727327287 | 703627894 | 680428513 | 657629144 | 635329787 | _ |
| 16 | 726927297 726527307 | 703227904 702827914 | 680028523 679628533 | 657329154 656929165 | 634929798 634629809 | 14 |
| 17 | 726127317 | 702427925 | 679228544 | 656529175 | 634229820 | 13 |
| 18 | 725727327 725327337 | 702127935 701727945 | 678928554 678528565 | 656129186 655829197 | 633829831 633529841 | 12 |
| | 724927347 | 701327955 | 678128575 | 655429207 | 633129852 | |
| 19 | 724527357 724127367 | 700927965 700527976 | 677728586 677328596 | 655029218 654629229 | 632729863 632429874 | 11 |
| 20 | 723727377 | 700127986 | 677028607 | 654329239 | 632029885 | 10 |
| 21 | 723327387 722927398 | 699727996 699328006 | 676628617 676228627 | 653929250 653529261 | 631629896 631329907 | 9 |
| | 722527408 | 698928017 | 675828638 | 653129271 | 630929917 | L |
| 22 | 722127418 | 698528027 | 675428648 | 652829282 | 630529929 | 8 |
| 23 | 721727428 721327438 | 698228037 697828047 | 675028659 674728669 | 652429293 652029303 | 630229939 629829950 | 7 |
| | 720927448 | 697428058 | 674328680 | 651629314 | 629429961 | |
| 24 | 720527458 720127468 | 697028068 696628078 | 673928690 673528701 | 651329325 650929335 | 629129972 628729983 | 6 |
| 25 | 719727478 | 696228089 | 673128711 | 650529346 | 628329994 | 5 |
| | 719327488 | 695828099 | 672828722 | 650229357 | 628030005 | |
| 26 | 719027498 718627508 | 695428109 695128119 | 672428732 672028743 | 649829367 649429378 | 627630015 627230026 | 4 |
| 27 | 718227518 717827528 | 694728130 694328140 | 671628753 671228763 | 649029389 648729399 | 626930037 626530048 | 3 |
| 28 | 717427539 | 693928150 | 670928774 | 648329410 | 626130059 | 2 |
| | 717027549 | 693528161 | 670528784 | 647929421 | 625830070 | |
| 29 | 716627559 716227569 | 693128171 692728181 | 670128795 669728806 | 647529432 647229442 | 625430081 625130092 | 1 |
| 30 | 715827579 | 692328191 | 669328816 | 646829453 | 624730103 | 0 |
| | A B | A B | A B | А В | A B | |
| | 122 ⁰ 00' | 121°30' | 121 ⁰ 00' | 120°30' | 120°00' | 1 |
| | | | | | 1 | I |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 1 | 1 | | 1 | • | 1 |
|----|------------------------|------------------------|------------------------|-------------------------|------------------------------------|---------------|
| | 60°00. | 60°30' | 61 [°] 00' | 61 °30' | 62 ⁰ 00' | |
| | A B | A B | - A B | АВ | A B | <u> </u> |
| 0 | 624730103 | 603030766 | 581831443 | 561032134 | 540632839 | 30 |
| 1 | 624330114 624030125 | 602730777 602330788 | 581531454 581131466 | 560732145 560332157 | 540332851 540032863 | 29 |
| • | 623630136 | 602030800 | 580831477 | 560032169 | 539632875 | 1 " |
| 2 | 623230147 | 601630811 | 580431488 | 559632180 | 539332887 | 28 |
| 3 | 622930158 622530169 | 601230822 600930833 | 580131500 579731511 | 559332192 559032204 | 539032898 538632910 | 27 |
| J | 622130180 | 600530844 | 579431523 | 558632215 | 538332922 | 1 |
| 4 | 621830191 | 600230856 | 5790,31534 | 558332227 | 538032934 | 26 |
| 5 | 621430202 | 599830867 | 578731546 | 557932239 | 537632946 | 05 |
| 3 | 621030213 620730224 | 599530878 599130889 | 578331557 578031569 | 557532250 557232262 | 537332958 537032970 | 25 |
| 6 | 620330235 | 598730900 | 577631580 | 556932274 | 536632982 | 24 |
| _ | 620030245 | 598430912 | 577331591 | 556632285 | 536332994 | |
| 7 | 619630256 619230267 | 598030923 597730934 | 576931603 576631614 | 556232297 555932309 | 536033006 535633018 | 23 |
| 8 | 618930278 | 597330945 | 576231626 | 555532320 | 535333030 | 22 |
| _ | 618530289 | 597030956 | 575931637 | 555232332 | 535033042 | Į. |
| 9 | 618130300 617830311 | 596630968 596330979 | 575531649 575231660 | 554932344 554532355 | 534633054 534333065 | 21 |
| 10 | 617430322 | 595930990 | 574831672 | 554232367 | 534033077 | 20 |
| | 617130334 | 595531001 | 574531683 | 553832379 | 533633089 | ~ |
| 11 | 616730345 616330355 | 595231013 594831024 | 574131694 573831706 | 553532391 553232402 | 533333101 533033113 | 19 |
| 12 | 616030367 | 594531035 | 573431717 | 552832414 | 532633125 | 18 |
| | 615630378 | 594131046 | 573131729 | 552532426 | 532333137 | '` |
| 13 | 615230389 614930400 | 593831058 593431069 | 572731740 572431752 | 552132438 551832449 | 532033149 531633161 | 17 |
| 14 | 614530411 | 593131080 | 572031763 | | | 16 |
| 17 | 614230422 | 592731091 | 571731775 | 551532461 551132473 | 531333173 531033185 | , '° |
| 15 | 613830433 | 592431103 | 571431786 | 550832484 | 530633197 | 15 |
| 16 | 613430444 | 592031114 | 571031798 | 550432496 | 530333209 | - |
| 16 | 613130455 612730466 | 591731125 591331137 | 570731809 570331821 | 550132508 549832520 | 530033221 529633233 | 14 |
| 17 | 612430477 | 560931148 | 570031833 | 549432532 | 529333245 | 13 |
| | 612030488 | 590631159 | 569631844 | 549132543 | 529033257 | |
| 18 | 611630499 611330510 | 590231170 589931182 | 569331856 568931867 | 548732555 548432567 | 52863326 9 528333281 | 12 |
| 19 | 610930521 | 589531193 | 568631879 | 548132579 | 528033293 | 11 |
| | 610630532 | 589231204 | 568231890 | 547732590 | 527633306 | <u> </u> |
| 20 | 610230544 609830555 | 588831216 588531227 | 567931902 567531913 | 547432602 547032614 | 527333318 527033330 | 10 |
| 21 | 609530566 | 588131238 | 567231925 | 546732625 | 526633342 | 9 |
| | 609130577 | 587831250 | 566931936 | 546432638 | 526333354 | |
| 22 | 608830588 608430599 | 587431261 587131272 | 566531948 566231960 | 546032649 545732661 | 526033366 525733378 | 8 |
| 23 | 608030610 | 586731284 | 565831971 | 545432673 | 525333390 | 7 |
| | 607730621 | 586431295 | 565531983 | 545032685 | 525033402 | |
| 24 | 607330632 607030643 | 586031306 585731318 | 565131994 564832006 | 544732697 5443 33709 | 524733414 5243 33436 | 6 |
| 25 | 606630655 | 585331329 | 564432018 | 544332709 544032720 | 524333426 524033438 | 5 |
| | 606230666 | 585031340 | 564132029 | 543732732 | 523733450 | |
| 26 | 605930677 | 584631352 | 563832041 | 543332744 | 523333462 | 4 |
| 27 | 605530688 605230699 | 584331363 583931375 | 563432052 563132064 | 543032756 542732768 | 523033475 522733487 | 3 |
| | 604830710 | 583631386 | 562732076 | 542332780 | 522433499 | <u> </u> |
| 28 | 604530721 | 583231397 | 562432087 | 542032792 | 522033511 | 2 |
| 29 | 604130733 693730744 | 582931409 582531420 | 562032099 561732110 | 541732803 541332815 | 521733523 521433535 | 1 |
| | 603430755 | 582231431 | 561432122 | 541032827 | 521033547 | • |
| 30 | 603030766 | 581831443 | 561032134 | 540632839 | 520733559 | 0 |
| | A B | А В | А В | А В | A B | |
| | 119 ⁰ 30' | 119 ⁰ 00' | 118 ⁰ 30' | 118 ⁰ 00' | 117°30' | |
| | | | | | 55 | |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 62°30' | 63°00' | 63°30' | 64 ⁰ 00' | 64 [°] 30' | ı |
|-----------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|----|
| | A B | A B | 63 30 A B | A B | 64 30 A B | 1 |
| 0 | 520733559 | 501234295 | 482135047 | 463435816 | 445136602 | 30 |
| 1 | 520433572 520033584 519733596 | 500934308 500534320 500234332 | 481835060 481535073 481135085 | 463135829 462835842 462535855 | 444836615 444536628 444236641 | 29 |
| 2 | 519433608 | 499934345 | 480835098 | 462235868 | 443936655 | 28 |
| 3 | 519133620 518733632 | 499634357 499334370 | 480535111 480235123 | 461935881 461535894 | 443636668 443336681 | 27 |
| | 518433644 | 498934382 | 479935136 | 461235907 | 443036694 | |
| 4 | 518133657 517833669 | 498634395 498334407 | 479635149 479335161 | 460935920 460635933 | 442736708 442436721 | 26 |
| 5 | 517433681 517133693 | 498034420 497734432 | 478935174 478635187 | 460335946 460035959 | 442136734 441836747 | 25 |
| 6 | 516833705 | 497334444 | 478335200 | 459735972 | 441536761 | 24 |
| 7 | 516433717 516133730 | 497034457 496734469 | 478035212 477735225 | 459435985 459135998 | 441236774 440936787 | 23 |
| | 515833742 | 496434482 | 477435238 | 458836011 | 440636801 | L~ |
| 8 | 515533754 515233766 | 496134494 495734507 | 477135251 476735263 | 458536024 458236037 | 440336814 440036827 | 22 |
| 9 | 514833779 514533791 | 495434519 495134532 | 476435276 476135289 | 457936050 457636063 | 439736841 439436854 | 21 |
| 10 | 514233803 | 494834544 | 475835302 | 457336076 | 439136867 | 20 |
| 11 | 513833815 513533827 | 494534557 494134569 | 475535314 475235327 | 456936089 456636102 | 438836881 438536894 | 19 |
| | 513233840 | 493834582 | 474935340 | 456336115 | 438236907 | |
| 12 | 512833852 512533864 | 493534594 493234607 | 474635353 474235365 | 456036128 455736141 | 437936921 437636934 | 18 |
| 13 | 512233876 511933889 | 492934619 492534632 | 273935378 473635391 | 455436154 455136167 | 437336948 437036961 | 17 |
| 14 | 511533901 | 492234644 | 473335404 | 454836180 | 436736974 | 16 |
| 15 | 511233913 510933925 | 491934657 491634669 | 473035417 472735429 | 454536193 454236206 | 436436988 436137001 | 15 |
| | 510639938 | 491334682 | 472435442 | 452936220 | 435837014 | |
| [*] 16 | 510233950 509933962 | 491034694 490634707 | 472135455 471835468 | 453636233 453336246 | 435537028 435237041 | 14 |
| 17 | 509633974 509333987 | 490334719 490034732 | 471435481 471135493 | 453036259 452736272 | 434937055 434637068 | 13 |
| 18 | 508933999 | 489734744 | 470835506 | 452436285 | 434337081 | 12 |
| 19 | 508634011 508334024 | 489434757 489034770 | 470535519 470235532 | 452136298 451836311 | 434037095 433737108 | 11 |
| | 508034036 | 488734782 | 469935545 | 451536325 | 433437122 | - |
| 20 | 507634048 507334061 | 488434795 488134807 | 469635558 469335571 | 451236338 450936351 | 433237135 432937149 | 10 |
| 21 | 507034073 506734085 | 487834820 487534832 | 469035583 468635596 | 450636364 450336377 | 432637162 432337176 | 9 |
| 22 | 506434097 | 487134845 | 468335609 | 450036390 | 432037189 | 8 |
| 23 | 506034110 505734122 | 496834858 486534870 | 468035622 467735635 | 449736403 449336417 | 431737203 431437216 | 7 |
| 24 | 505434134 505134147 | 486234883 485934896 | 467435648 467135661 | 449036430 448736443 | 431137229 430837243 | 6 |
| 25 | 504734159 504434172 | 485634908 485234921 | 466835674 | 448436456 | 430537256 | |
| | 504134184 | 484934933 | 466535686 466235699 | 448136469 447836483 | 430237270 429937283 | 5 |
| 26 | 503834196 503434209 | 484634946 484334959 | 465935712 465635725 | 447536496 447236509 | 429637297 429337310 | 4 |
| 27 | 503134221 | 484034971 | 465235738 | 446936522 | 429037324 | 3 |
| 28 | 502834233 502534246 | 483734984 483334997 | 464935751 464635764 | 446636535 446336549 | 428737337 428437351 | 2 |
| 29 | 502234258 501834270 | 483035009 482735022 | 464335777 464035790 | 446036562 | 428137365 | |
| 2.5 | 501534283 | 482435035 | 463735803 | 445736575 445436588 | 427837378 427537392 | |
| 30 | 501234295 | 482135047 | 463435816 | 445136602 | 427237405 | 0 |
| | A B | A B | A B | А В | A B | 1 |
| | 117 ⁰ 00' | 116 ⁰ 30' | 116 ⁰ 00' | 115 ⁰ 30' | 115 ⁰ 00' | İ |
| | | • | • | • | • | - |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| - | 65 [°] 00' | 65°30' | 66°00' | 66°30' | 67 ⁰ 00' | |
|----|------------------------|------------------------|------------------------|------------------------|------------------------|-------------|
| | A B | A B | A B | A B | A B | |
| - | 427237405 | 409838227 | 392739069 | 376039930 | 359740812 | 30 |
| | 426937419 | 409538241 | 392439083 | 375739945 | 359540827 | 20 |
| 1 | 426637432 426437446 | 409238255 408938269 | 392139097 391839111 | 375539959 375239974 | 359240842 358940857 | 29 |
| 2 | 426137459 | 408638283 | 391639125 | 374939988 | 358740872 | 28 |
| 3 | 425837473 425537487 | 408338297 408038311 | 391339140 391039154 | 374640003 374440017 | 358440887 358140902 | 27 |
| | 425237500 | 407838324 | 390739168 | 374140032 | 357940916 | <u> </u> |
| 4 | 424937514 | 407538338 | 390439182 | 373840046 | 357640931 | 26 |
| 5 | 424637527 424337541 | 407238352 406938366 | 390239197 389939211 | 373540061 373340076 | 357340946 357140961 | 25 |
| | 424037554 | 406638380 | 389639225 | 373040090 | 356840976 | |
| 6 | 423737568 | 406338394 | 389339239 | 372740105 | 356540991 | 24 |
| 7 | 423437582 423137595 | 406038408 405738422 | 389039254 388839268 | 372540119 372240134 | 356341006 356041021 | 23 |
| | 422837609 | 305538436 | 388539282 | 371940149 | 355741036 | |
| 8 | 422537623 422237636 | 405238450 404938464 | 388239296 387939311 | 371640163 371440178 | 355541051 355241066 | 22 |
| 9 | 422037650 | 404638478 | 387639325 | 371140178 | 354941081 | 21 |
| | 421737663 | 404338492 | 387439339 | 370840207 | 354741096 | |
| 10 | 421437677 421137691 | 404038506 403738520 | 387139353 386839368 | 370540222 370340236 | 354441111 354141126 | 20 |
| 11 | 420837704 | 403538533 | 386539382 | 370040251 | 353941141 | 19 |
| | 420537718 | 403238547 | 386339396 | 369740266 | 353641156 | <u> </u> |
| 12 | 420237732 419937745 | 402938561 402638575 | 386039411 385739425 | 369540280 369240295 | 353341171 353141186 | 18 |
| 13 | 419637759 | 402338589 | 385439439 | 368940310 | 352841201 | 17 |
| | 419337773 | 402038603 | 385139454 | 368640324 | 352541216 | L |
| 14 | 419037786 418737800 | 401738617 401538631 | 384939468 384639482 | 368440339 368140354 | 352341231 352041246 | 16 |
| 15 | 418537814 | 401238645 | 384339497 | 367840368 | 351741261 | 15 |
| | 418237828 | 400938660 | 384039511 | 367640383 | 351541276 | |
| 16 | 417937841 417637855 | 400638674 400338688 | 383839525 383539540 | 367340398 367040413 | 351241291 350941307 | 14 |
| 17 | 417337869 | 400038702 | 383239554 | 366740427 | 350741322 | 13 |
| | 417037882 | 399838716 | 382939569 | 366540442 | 350441337 | |
| 18 | 416737896 416437910 | 399538730 399238744 | 382639583 382439597 | 366240457 365940471 | 350241352 349941367 | 12 |
| 19 | 416137924 | 398938758 | 382139612 | 365740486 | 349641382 | 11 |
| | 415837937 | 398638772 | 381839626 | 365440501 | 349441397 | <u> </u> |
| 20 | 415537951 415337965 | 398338786 398138800 | 381539641 381339655 | 365140516 364840530 | 349141412 348841427 | 10 |
| 21 | 415037979 | 397838814 | 381039669 | 364640545 | 348641443 | 9 |
| | 414737992 | 397538828 | 380739684 | 364340560 | 348341458 | <u> </u> |
| 22 | 414438006 414138020 | 397238842 396938856 | 380439698 380139713 | 364040575 363840590 | 348041473 347841488 | 8 |
| 23 | 413838034 413538048 | 396638871 396438885 | 379939727 379639742 | 363540604 363240619 | 347541503 | 7 |
| 24 | 413238048 | 396138899 | 379339756 | | 347341518 | |
| | 412938075 | 395838913 | 379339756 379039771 | 363040634 362740649 | 347041533 346741549 | 6 |
| 25 | 412738089 412438103 | 395538927 395238941 | 378839785 378539799 | 362440664 362240678 | 346541564 346241579 | 5 |
| 26 | 412138117 | 394938955 | 378239814 | 361940693 | 345941594 | 4 |
| | 411838130 | 394738969 | 377939828 | 361640708 | 345741609 |] |
| 27 | 411538144 411238158 | 394438984 394138998 | 377739843 377439857 | 361340723 361140738 | 345441625 345241640 | 3 |
| 28 | 410938172 | 393839012 | 377139872 | 360840753 | 344941655 | |
| | 410638186 | 393539026 | 376839886 | 360540768 | 344641670 | 1 |
| 29 | 410338200 410138213 | 393339040 393039054 | 376639901 376339915 | 360340782 360040797 | 344441685 344141701 | 1 |
| 30 | 409838227 | 392739069 | 376039930 | 359740812 | 343841716 | 0 |
| | АВ | A B | A B | A B | A B | |
| | | | | | | |
| | 114 ⁰ 30' | 114 ⁰ 00' | 113 ⁰ 30' | 113 ⁰ 00' | 112 ⁰ 30' | |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 67°30' | 68 [°] 00' | 68°30' | 69°00' | 69°30' | ı |
|-----|------------------------|------------------------|------------------------|------------------------|-------------------------|--------------|
| | A B | A B | A B | A B | A B | 1 |
| 0 | 343841716 | 328342642 | 313243592 | 298544567 | 284145567 | 30 |
| | 343641731 | 328142658 | 313043608 | 298244583 | 283945584 | |
| 1 | 343341746 343141762 | 327842674 327642689 | 312743624 312543641 | 298044600 297844616 | 283645601 283445618 | 29 |
| 2 | 342841777 | 327342705 | 312243657 | 297544633 | 283245635 | 28 |
| 3 | 342541792 342341808 | 327142721 326842736 | 312043673 311743689 | 297344649 297044666 | 282945652 282745669 | 27 |
| | 342041823 | 326642752 | 311543705 | 296844682 | 282545686 | l "' |
| 4 | 341841838 | 326342768 | 311243721 | 296544699 | 282245703 | 26 |
| 5 | 341541853 341241869 | 326042783 325842799 | 311043737 310743753 | 296344715 296144732 | 282045720 281845737 | 25 |
| | 341041884 | 325542815 | 310543769 | 295844748 | 281545754 | |
| 6 | 340741899 | 325342830 | 310243785 | 295644765 | 281345771 | 24 |
| 7 | 340441915 340241930 | 325042846 324842862 | 310043801 309743818 | 295344782 295144798 | 281145788 280845805 | 23 |
| | 339941945 | 324542878 | 309543834 | 294944815 | 280645822 | |
| 8 | 339741961 339441976 | 324342893 324042909 | 309243850 309043866 | 294644831 294444848 | 280445839 280145856 | 22 |
| 9 | 339141991 | 323742925 | 308843882 | 294144864 | 279945873 | 21 |
| | 338942007 | 323542941 | 308543898 | 293944881 | 279745890 | |
| 10 | 338642022 338442038 | 323342956 323042972 | 308343914 308043931 | 293644898 293444914 | 279445907 279245924 | 20 |
| 11 | 338142053 | 322742988 | 307843947 | 293244931 | 278945941 | 19 |
| -10 | 337942068 | 322543004 | 307543963 | 292944947 | 278745958 | 120 |
| 12 | 337642084 337342099 | 322243020 322043035 | 307343979 307043995 | 292744964 292444981 | 278545975 278245992 | 18 |
| 13 | 337142115 336842130 | 321743051 321543067 | 306844012 | 292244997 | 278046009 277846026 | 17 |
| 14 | 336642145 | 321243083 | 306544028 306344044 | 292045014 291745031 | 277546043 | 16 |
| 1-7 | 336342161 | 321043099 | 306044060 | 291545047 | 277346061 | l '° |
| 15 | 336042176 335842192 | 320743114 320543130 | 305844077 305644093 | 291345064 291045081 | 277146078 276846095 | 15 |
| 16 | 335542207 | 320243146 | 305344109 | 290845097 | 276646112 | 14 |
| 47 | 335342223 | 320043162 | 305144125 | 290545114 | 276446129 | |
| 17 | 335042238 334842254 | 319743178 319543194 | 304844142 304644158 | 290345131 290145147 | 276146146 275946163 | 13 |
| 18 | 334542269 | 319243210 | 304344174 | 289845164 | 275746181 | 12 |
| 19 | 334242285 334042300 | 319043225 318743241 | 304144190 303844207 | 289645181 289345198 | 275546198 275246215 | 11 |
| | 333742316 | 318543257 | 303644223 | 289145214 | 275046232 | L¨. |
| 20 | 333542331 | 318243273 | 303344239 | 288945231 | 274846249 | 10 |
| 21 | 333242347 332942362 | 318043289 317743305 | 303144256 302944272 | 288645248 288445265 | 274546266 274346284 | 9 |
| | 332742378 | 317543321 | 302644288 | 288145281 | 274146301 | |
| 22 | 332442393 332242409 | 317243337 317043353 | 302444305 302144321 | 287945298 287745315 | 273846318 273646335 | 8 |
| 23 | 331942424 | 316743369 | 301944337 | 287445332 | 273446353 | 7 |
| | 331742440 | 316543385 | 301644354 | 287245348 | 273146370 | |
| 24 | 331442455 331242471 | 316243400 316043416 | 301444370 301244386 | 287045365 286745382 | 272946387 272746404 | 6 |
| 25 | 330942486 | 315743432 | 300944403 | 286545399 | 272446422 | 5 |
| | 330642502 | 315543448 | 300744419 | 286245416 | 272246439 | |
| 26 | 330442518 330142533 | 315243464 315043480 | 300444436 300244452 | 286045433 285845449 | 272046456 271746473 | 4 |
| 27 | 329942549 329642564 | 314743496 314543512 | 299944468 299744485 | 285545466 285345483 | 271546491 2713 46508 | 3 |
| 28 | 329442580 | 314243528 | 299444501 | 285145500 | 271346508 271146525 | 2 |
| | 329142596 | 314043544 | 299244518 | 284845517 | 270846543 | I |
| 29 | 328942611 328642627 | 313743560 313543576 | 299044534 298744551 | 284645534 284445551 | 270646560 270446577 | 1 |
| 30 | 328342642 | 313243592 | 298544567 | 284145567 | 270146595 | 0 |
| | A B | A B | A B | A B | A B | i |
| | 112 ⁰ 00' | 111 °30' | 111 ⁰ 00' | 110 [°] 30' | 110 [°] 00' | 1 |
| | 112 00 | 111 30 | 111 00 | 110 30 | 110 00 | l |
| | | | | | | |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 70°00' | 70°30' | 71 [°] 00' | 71 ⁰ 30' | 72 [°] 00' | ı |
|-----|-------------------------|-------------------------|------------------------|------------------------|------------------------|----------------|
| | 70 00° | 70 30° | 71 00° | 71 30 B | 72 00° | - |
| - | 270146595 | 256547650 | 243348736 | 230449852 | 217951002 | 30 |
| • | 269946612 | 256347668 | 243148754 | 230249871 | 217551002 | 30 |
| 1 | 269746630 269446647 | 256147686 255947704 | 242948772 242748791 | 230049890 229849909 | 217551041 217351060 | 29 |
| | 269246664 | 255647722 | 242448809 | 229649928 | 217151080 | 28 |
| | 269046682 | 255447740 | 242248828 | 229449947 | 216951099 | 20 |
| 3 | 268846699 268546716 | 255247758 255047775 | 242048846 241848864 | 229249966 229049985 | 216751119 216551138 | 27 |
| 4 | 268346734 | 254747793 | 241648883 | 228750004 | 216351158 | 26 |
| | 268146751 | 254547811 | 241348901 | 228550023 | 216151177 | - |
| 5 | 267846769 267646786 | 254347829 254147847 | 241148920 240948938 | 228350042 228150061 | 215951197 215751216 | 25 |
| 6 | 267446804 | 253947865 | 240748957 | 227950080 | 215551236 | 24 |
| | 267246821 | 253647883 | 240548975 | 227750098 | 215351255 | ŀ |
| 7 | 266946839 266746856 | 253447901 253247919 | 240348993 240049012 | 227550117 227350137 | 215151275 214951294 | 23 |
| 8 | 266546873 | 253047937 | 239849030 | 227150156 | 214751314 | 22 |
| , | 266246891 | 252847955 | 239649049 | 226950175 | 214551334 | İ |
| 9 | 266046908 265846926 | 252547973 252347991 | 239449067 239249086 | 226650194 226450213 | 214351353 214151373 | 21 |
| 10 | 265646943 | 252148009 | 239049104 | 226250232 | 213851392 | 20 |
| 11 | 265346961 265146978 | 251948027 251648045 | 238749123 238549141 | 226050251 225850270 | 213651412 213451432 | 10 |
| ., | 264946996 | 251448063 | 238349160 | 225650270 | 213251451 | 19 |
| 12 | 264647014 | 251248081 | 238149179 | 225450308 | 213051471 | 18 |
| 13 | 264447031 264247049 | 251048099 250748117 | 237949197 237749216 | 225250327 225050346 | 212851491 212651510 | 17 |
| ,,, | 264047066 | 250548135 | 237549234 | 224850365 | 212451530 | [" |
| 14 | 263747084 | 250348153 | 237249253 | 224650385 | 212251550 | 16 |
| 15 | 263547101 263347119 | 250148171 249948189 | 237049271 236849290 | 224350404 224150423 | 212051570 211851589 | 15 |
| | 263147137 | 249648207 | 236649309 | 223950442 | 211651609 | 1 |
| 16 | 262847154 | 249448226 | 236449327 | 223750461 | 211451629 | 14 |
| 17 | 262647172 262447189 | 249248244 249048262 | 236249346 236049365 | 223550480 223350499 | 211251649 211051668 | 13 |
| | 262247207 | 248848280 | 235849383 | 223150519 | 210851688 | |
| 18 | 261947225 261747242 | 248548298 248348316 | 235549402 235349421 | 222950538 222750557 | 210651708 | 12 |
| 19 | 261547269 | 248148334 | 235149439 | 222550576 | 210451728 210251747 | 11 |
| | 261347278 | 247948352 | 234949458 | 222350596 | 210051767 | |
| 20 | 261047295 260847313 | 247748371 247448389 | 234749477 234549495 | 222150615 221850634 | 209851787 209651807 | 10 |
| 21 | 260647331 | 247248407 | 234349514 | 221650653 | 209451827 | 9 |
| | 260447348 | 247048425 | 234049533 | 221450673 | 209251847 | <u> </u> |
| 22 | 260147366 259947384 | 246848443 246648462 | 233849551 233649570 | 221250692 221050711 | 209051867 208851886 | 8 |
| 23 | 259747402 | 246348480 | 233449589 | 220850730 | 208651906 | 7 |
| | 259447419 | 246148498 | 233249608 | 220650750 | 208451926 | <u> </u> |
| 24 | 259247437 259047455 | 245948516 245748534 | 233049626 232849645 | 220450769 220250788 | 208251946 208051966 | 6 |
| 25 | 258847472 | 245548553 | 232549664 | 220050808 | 207851986 | 5 |
| 26 | 258547490 258347508 | 245348571 | 232349683 | 219850827 | 207652006 | - |
| 20 | 258147526 | 245048589 244848608 | 232149702 231949720 | 219650846 219450866 | 207452026 207252046 | 4 |
| 27 | 257947544 2576 47561 | 244648626 2444 48644 | 231749739 | 219250885 | 207052066 | 3 |
| 28 | 257647561 257447579 | 244448644 244248662 | 231549758 | 219050905 | 206852086 | |
| | 257247597 | 244248681 243948681 | 231349777 231149796 | 218850924 218550943 | 206652106 206452126 | 2 |
| 29 | 257047615 2568 47633 | 243748699 2435 48717 | 230949815 | 218350963 | 206252146 | 1 |
| 30 | 256847633 256547650 | 243548717 243348736 | 230649833 230449852 | 218150982 217951002 | 206052166 | 1 |
| | A B | A B | A B | A B | 205852186 A B | <u> </u> |
| | | | | | | 4 |
| | 109 [°] 30' | 109 ⁰ 00' | 108 ⁰ 30' | 108 ⁰ 00' | 107 [°] 30′ | 1 |
| | - 1 | - | • | • | • | • |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 72°30' | 73°00' | 73°30' | 74°00′ | 74°30' | 1 |
|----|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|----------|
| | A B | A B | 73 30 A B | A B | 74 30 A B | |
| 0 | 205852186 | 194053406 | 182654666 | 171655966 | 160957310 | 30 |
| 1 | 205652206 205452226 205252246 | 193853427 193653448 193553468 | 182454687 182354708 182154730 | 171455988 171256010 171056032 | 160757333 160557356 160457378 | 29 |
| 2 | 205052266 | 193353489 | 181954751 | 170956054 | 160257401 | 28 |
| 3 | 204852286 204652306 | 193153510 | 181754773 | 170756076 | 160057424 | 27 |
| | 204452326 | 192953531 192753551 | 181554794 181354815 | 170556099 170356121 | 159857447 159757470 | 27 |
| 4 | 204252346 204052366 | 192553572 192353593 | 181154837 180954858 | 170156143 170056165 | 159557493 159357516 | 26 |
| 5 | 203852387 | 192153614 | 180854880 | 169856187 | 159157538 | 25 |
| | 203652407 | 191953634 191753655 | 180654901 180454922 | 169656209 169456231 | 159057561 158857584 | 24 |
| | 203252447 | 191553676 | 180254944 | 169256254 | 158657607 | |
| 7 | 203052467 202852487 | 191353697 191153718 | 180054965 179854987 | 169156276 168956298 | 158457630 158357653 | 23 |
| 8 | 202652508 | 191053738 | 179655008 | 168756320 | 158157676 | 22 |
| 9 | 202452528 202252548 | 190853759 190653780 | 179555030 179355051 | 168556342 168356365 | 157957699 157857722 | 21 |
| | 202052568 | 190453801 | 179155073 | 168256387 | 157657745 | |
| 10 | 201852588 201652609 | 190253822 190053843 | 178955095 178755116 | 168056409 167856431 | 157457768 157257791 | 20 |
| 11 | 201452629 201252649 | 189853864 189653884 | 178555138 178355159 | 167656454 167456476 | 157157814 156957837 | 19 |
| 12 | 201052670 | 189453905 | 178255181 | 167356498 | 156757860 | 18 |
| 13 | 200952690 200752710 | 189253926 189053947 | 178055202 177855224 | 167156521 166956543 | 156557884 156457907 | 17 |
| | 200552730 | 188953968 | 177655246 | 166756565 | 156257930 | |
| 14 | 200352751 200152771 | 188753989 188554010 | 177455267 177255289 | 166556588 166456610 | 156057953 155957976 | 16 |
| 15 | 199952791 | 188354031 | 177155311 | 166256632 | 155757999 | 15 |
| 10 | 199752812 | 188154052 | 176955332 | 166056655 | 155558022 | <u> </u> |
| 16 | 199552832 199352852 | 187954073 187754094 | 176755354 176555376 | 165856677 165756700 | 155358046 155258069 | 14 |
| 17 | 199152873 198952893 | 187554115 187354136 | 176355397 176155419 | 165556722 165356745 | 155058092 154858115 | 13 |
| 18 | 198752914 | 187154157 | 176055441 | 165156767 | 154658138 | 12 |
| 19 | 198552934 198352954 | 187054178 186854199 | 175855463 175655484 | 165056790 164856812 | 154558162 154358185 | 11 |
| | 198152975 | 186654220 | 175455506 | 164656835 | 154158208 | |
| 20 | 197952995 197753016 | 186454242 186254263 | 175255528 175055550 | 164456857 164256880 | 154058232 153858255 | 10 |
| 21 | 197553036 | 186054284 | 174955572 | 164156902 | 153658278 | 9 |
| 22 | 197353057 | 185854305 | 174755593 | 163956925 | 153458302 153358325 | |
| | 197153077 196953098 | 185654326 185454347 | 174555615 174355637 | 163756947 163556970 | 153158348 | 8 |
| 23 | 196753118 196653139 | 185354368 185154390 | 174155659 173955681 | 163456992 163257015 | 152958372 152858395 | 7 |
| 24 | 196453159 196253180 | 184954411 | 173855703 | 163057038 | 152658418 | 6 |
| 25 | 196053200 | 184754432 184554453 | 173655725 173455746 | 162857060 162757083 | 152458442 152358465 | 5 |
| | 195853221 | 184354474 | 173255768 | 162557106 | 152158489 | |
| 26 | 195653241 195453262 | 184154496 183954517 | 173055790 172855812 | 162357128 162157151 | 151958512 151758536 | 4 |
| 27 | 195253283 195053303 | 183754538 183654559 | 172755834 172555856 | 161957174 161857196 | 151658559 151458583 | 3 |
| 28 | 194853324 | 183454581 | 172355878 | 161657219 | 151258606 | 2 |
| 29 | 194653344 194453365 | 183254602 183054623 | 172155900 171955922 | 161457242 161257265 | 151158630 150958653 | 1 |
| | 194453365 | 182854644 | 171855944 | 161157287 | 150758677 | 1 |
| 30 | 194053406 | 182654666 | 171655966 | 160957310 | 150658700 | 0 |
| | А В | А В | A B | A B | А В | |
| | 107 ⁰ 00' | 106 [°] 30' | 106 ⁰ 00' | 105 ⁰ 30 [,] | 105 ⁰ 00' | |
| | • ' | • | , | | • | • |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 75°00' | 75 [°] 30' | 76 ⁰ 00' | 76°30' | 77 [°] 00' | |
|----|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|----|
| | A B | A B | A B | А В | A B | |
| 0 | 150658700 | 140660140 | 131061632 | 121763181 | 112864791 112664819 | 30 |
| 1 | 150458724 150258748 150058771 | 140460164 140360189 140160213 | 130861658 130661683 130561709 | 121563208 121463234 121263260 | 112564846 112364873 | 29 |
| 2 | 149958795 | 139960238 | 130361734 | 121163287 | 112264901 | 28 |
| 3 | 149758818 149558842 149458866 | 139860262 139660287 139460311 | 130161759 130061785 129961810 | 120963313 120863340 120663366 | 112064928 111964956 111764983 | 27 |
| 4 | 149258889 | 139360336 | 129761836 | 120563392 | 111665011 | 26 |
| 5 | 149058913 148958937 148758960 | 139160360 139060385 138860410 | 129561861 129461887 129261912 | 120363419 120263445 120063472 | 111465038 111365066 111265093 | 25 |
| 6 | 148558984 | 138660434 | 129161938 | 119963498 | 111065121 | 24 |
| 7 | 148459008 148259032 148059055 | 138560459 138360483 138160508 | 128961963 128861989 128662014 | 119763525 119663551 | 110965148 110765176 110665204 | 23 |
| 8 | 147959079 | 138060533 | 128462040 | 119463578 119363605 | 110465231 | 22 |
| 9 | 147759103 147559127 | 137860557 137760582 | 128362065 128162091 | 119163631 119063658 | 110365259 110165287 | 21 |
| 10 | 147459151 147259175 | 137560607 137360631 | 128062117 127862142 | 118863684 118763711 | 110065314 | 20 |
| 11 | 147059198 146959222 | 137260656 137060681 | 127762168 127562194 | 118563738 118463764 | 109765370 109665398 | 19 |
| 12 | 146759246 146559270 | 136860706 136760730 | 127462219 127262245 | 118263791 118163818 | 109465425 109365453 | 18 |
| 13 | 146459294 146259318 146059342 | 136560755 136460780 136260805 | 127062271 126962296 126762322 | 117963845 117863871 117663898 | 109165481 109065509 108965537 | 17 |
| 14 | 145959366 | 136060830 | 126662348 | 117563925 | 108765564 | 16 |
| 15 | 145759390 145559414 145459438 | 135960855 135760879 135660904 | 126462374 126362400 126162425 | 117363952 117263978 117064005 | 108665592 108465620 108365648 | 15 |
| 16 | 145259462 145059486 | 135460929 135260954 | 126062451 125862477 | 116964032 116764059 | 108165676 108065704 | 14 |
| 17 | 144959510 144759534 | 135160979 134961004 | 125762503 125562529 | 116664086 116464113 | 107965732 107765760 | 13 |
| 18 | 144559558 144459582 | 134861029 134661054 | 125362555 125262581 | 116364140 116164167 | 107665788 107465816 | 12 |
| 19 | 144259606 144059630 | 134461079 134361104 | 125062607 124962633 | 116064194 115864221 | 107365844 107165872 | 11 |
| 20 | 143959654 143759679 | 134161129 134061154 | 124762659 124662685 | 115764248 115564275 | 107065900 106965928 | 10 |
| 21 | 143559703 143459727 | 133861179 133661204 | 124462711 124362737 | 115464302 115264329 | 106765957 106665985 | 9 |
| 22 | 143259751 143059775 | 133561229 133361254 | 124162763 124062789 | 115164356 115064383 | 106466013 106366041 | 8 |
| 23 | 142959800 142759824 | 133261279 133061304 | 123862815 123762841 | 114864410 114764437 | 106166069 106066098 | 7 |
| 24 | 142559848 142459872 | 132961330 132761355 | 123562867 123462893 | 114564464 114464491 | 105966126 105766154 | 6 |
| 25 | 142259896 142159921 | 132561380 132461405 | 123262919 123062945 | 114264518 114164546 | 105666182 105466211 | 5 |
| 26 | 141959945 141759969 | 132261430 132161456 | 122962971 122762998 | 113964573 113864600 | 105366239 105266267 | 4 |
| 27 | 141659994 141460018 | 131961481 131761506 | 122663024 122463050 | 113664627 113564655 | 105066296 104966324 | 3 |
| 28 | 141260042 141160067 | 131661531 131461556 | 122363076 122163103 | 113364682 113264709 | 104766352 104666381 | 2 |
| 29 | 140960091 140760116 | 131361582 131161607 | 122063129 121863155 | 113064736 112964764 | 104566409 104366438 | 1 |
| 30 | 140660140 | 131061632 | 121763181 | 112864791 | 104266466 | 0 |
| | A B | A B | А В | A B | A B | |
| | 104 ⁰ 30' | 104 ⁰ 00 [,] | 103 ⁰ 30' | 103 [°] 00' | 102 ⁰ 30' | |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 77 ⁰ 30' | | | l . | | 1 |
|------|------------------------|----------------------|-----------------------|-----------------------|-----------------------|----------|
| | | 78 ⁰ 00' | 78 ⁰ 30' | 79 ⁰ 00' | 79 ⁰ 30' | ł |
| | А В | A B | A B | A B | A B | |
| 0 | 104266466 104066495 | 96068212 95868242 | 88170034 87970065 | 80571940 80471973 | 73373937 73273971 | 30 |
| 1 | 103966523 | 95768272 | 87870097 | 80372005 | 73174005 | 29 |
| | 103866552 | 95568301 | 87770128 | 80272038 | 73074039 | _ |
| 2 | 103665580 103566609 | 95468331 95368361 | 87670159 87470190 | 80072070 79972103 | 72974073 72874107 | 28 |
| 3 | 103366638 | 95168391 | 87370221 | 79872136 | 72674142 | 27 |
| | 103266666 | 95068421 | 87270252 | 79772168 | 72574176 | |
| 4 | 103166695 102966724 | 94968450 94768480 | 87070284 86970315 | 79672201 79472234 | 72474210 72374245 | 26 |
| 5 | 102866752 | 94668510 | 86870346 | 79372266 | 72274279 | 25 |
| | 102666781 102566810 | 94568540 | 86770377 | 79272299 | 72174313 | - |
| 6 | 102466838 | 94368570 94268600 | 86570409 86470440 | 79172332 79072365 | 71974348 71874382 | 24 |
| 7 | 102266867 102166896 | 94168630 93968660 | 86370471 86270503 | 78872397 | 71774417 | 23 |
| 8 | 102066925 | 93868690 | 86070534 | 78772430 78672463 | 71674451 71574486 | 22 |
| J | 101866953 | 93768720 | 85970566 | 78572496 | 71474520 | -22 |
| 9 | 101766982 101567011 | 93568750 93468781 | 85870597 85670629 | 78372529 78272562 | 71274555 71174589 | 21 |
| 10 | 101467040 | 93368811 | 85570660 | 78172595 | 71074624 | 20 |
| | 101367069 | 93268841 | 85470692 | 78072628 | 70974659 | - |
| 11 | 101167098 101067127 | 93068871 92968901 | 85370723 85170755 | 77972661 77772694 | 70874693 70774728 | 19 |
| 12 | 100867156 | 92868931 | 85070786 | 77672727 | 70674763 | 18 |
| 40 | 100767185 | 92668962 | 84970818 | 77572760 | 70474797 | |
| 13 | 100667214 100467243 | 92568992 92469022 | 84870850 84670881 | 77472794 77272827 | 70374832 70274867 | 17 |
| 14 | 100367272 | 92269053 | 84570913 | 77172860 | 70174902 | 16 |
| 15 | 100267301 100067330 | 92169083 | 84470945 | 77072893 | 70074937 | 4.5 |
| 13 | 99967359 | 92069113 91869144 | 84370976 84171008 | 76972926 76872960 | 69974972 69875007 | 15 |
| 16 | 99767388 | 91769174 | 84071040 | 76772993 | 69675042 | 14 |
| 17 | 99667417 99567447 | 91669204 91469235 | 83971072 83871104 | 76573026 76473060 | 69575077 69475112 | 13 |
| | 99367476 | 91369265 | 83671135 | 76373093 | 69375147 | ' |
| 18 | 99267505 | 91269296 | 83571167 | 76273127 | 69275182 | 12 |
| 19 | 99167534 98967563 | 91069326 90969357 | 83471199 83371231 | 76173160 75973193 | 69175217 69075252 | 11 |
| | 98867593 | 90869387 | 83171263 | 75873227 | 68875287 | L¨. |
| 20 | 98767622 | 90769418 | 83071295 | 75773260 | 68775322 | 10 |
| 21 | 98567651 98467681 | 90569449 90469479 | 82971327 82871359 | 75673294 75573328 | 68675358 68575393 | 9 |
| | 98267710 | 90369510 | 82671391 | 75373361 | 68475428 | |
| 22 | 98167739 98067769 | 90169541 | 82571423 824 71455 | 75273395 751 73439 | 68375464 683 75400 | 8 |
| 23 | 97867798 | 90069571 89969602 | 82471455 82371488 | 75173429 75073462 | 68275499 68075534 | 7 |
| | 97767828 | 89769633 | 82171520 | 74973496 | 67975570 | |
| 24 | 97667857 97467886 | 89669664 89569694 | 82071552 81971584 | 74773530 74673563 | 67875605 67775641 | 6 |
| 25 | 97367916 | 89469725 | 81871616 | 74573597 | 67675676 | 5 |
| | 97267945 | 89269756 | 81671649 | 74473631 | 67575712 | |
| 26 | 97067975 96968005 | 89169787 89069815 | 81571681 81471713 | 74373665 74273699 | 67475747 67375783 | 4 |
| 27 | 96868034 | 88869849 | 81371746 | 74073733 | 67275819 | 3 |
| - 00 | 96668064 | 88769879 | 81171778 | 73973767 | 67075854 | <u> </u> |
| 28 | 96568093 96468123 | 88669910 88569941 | 81071810 80971843 | 73873801 73773835 | 66975890 66875926 | 2 |
| 29 | 96268153 | 88369972 | 80871875 | 73673869 | 66775961 | 1 |
| -20 | 96168182 | 88270003 | 80771908 | 73573903 | 66675997 | <u> </u> |
| | 96068212 A B | 88170034 A B | 80571940 A B | 73373937 A B | 66576033 | 0 |
| | | | | | A B | 1 |
| | 102 [°] 00' | 101 [°] 30' | 101 ⁰ 00' | 100 ⁰ 30' | 100 ⁰ 00' | |
| ' | - | • | • | • | • | • |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | | | 1 . | | 1 . | 1 |
|-----|----------------------|----------------------|----------------------|----------------------|----------------------|--------------|
| | 80°00' | 80°30' | 81 ⁰ 00' | 81 [°] 30' | 82 ⁰ 00' | ļ |
| | A B | A B | A B | А В | A B | ! |
| 0 | 66576033 66476069 | 60078239 59978277 | 53880567 53780607 | 48083030 47983072 | 42585644 42485689 | 30 |
| 1 | 66376105 | 59878315 | 53680647 | 47883114 | 42385734 | 29 |
| | 66176141 | 59778352 | 53580687 | 47783157 | 42285779 | |
| 2 | 66076176 65976212 | 59578390 59478428 | 53480727 53380767 | 47683199 47583242 | 42185825 42085870 | 28 |
| 3 | 65876248 | 59378466 | 53280807 | 47483284 | 41985915 | 27 |
| | 65776284 | 59278504 | 53180847 | 47383327 | 41885960 | |
| 4 | 65676320 | 59178542 | 53080887 | 47283369 | 41886006 | 26 |
| 5 | 65576357 65476393 | 59078580 58978618 | 52980927 52880967 | 47183412 47083455 | 41786051 41686096 | 25 |
| | 65376429 | 58878656 | 52781008 | 46983497 | 41586142 | |
| 6 | 65276465 | 58778694 | 52681048 | 46883540 | 41486187 | 24 |
| 7 | 65076501 64976537 | 58678733 58578771 | 52581088 52481129 | 46783583 46783626 | 41386233 41286278 | 23 |
| | 64876574 | 58478809 | 52381169 | 46683668 | 41186324 | |
| 8 | 64776610 | 58378847 | 52281210 | 46583711 | 41186370 | 22 |
| 9 | 64676646 64576683 | 58278886 58178924 | 52181250 52081291 | 46483754 46383797 | 41086415 40986461 | 21 |
| | 64476719 | 58078962 | 51981331 | 46283840 | 40886507 | [-' |
| 10 | 64376756 | 57979001 | 51881372 | 46183884 | 40786553 | 20 |
| 11 | 64276792 64176828 | 57879039 57779078 | 51781413 51681453 | 46083927 45983970 | 40686599 40586645 | 10 |
| •• | 63976865 | 57679116 | 51581494 | 45884013 | 40586691 | 19 |
| 12 | 63876902 | 57579155 | 51481535 | 45784056 | 40486737 | 18 |
| 13 | 63776938 63676975 | 57479193 57379232 | 51381576 | 45684100 | 40386783 | |
| | 63577011 | 57179271 | 51281617 51181657 | 45584143 45484186 | 40286829 40186876 | 17 |
| 14 | 63477048 | 57079309 | 51081698 | 45484230 | 40086922 | 16 |
| 15 | 63377085 63277122 | 56979348 56879387 | 50981739 | 45384273 | 39986968 | |
| | 63177158 | 56779426 | 50881780 50781821 | 45284317 45184361 | 39987015 39887061 | 15 |
| 16 | 63077195 | 56679465 | 50681863 | 45084404 | 39787107 | 14 |
| 17 | 62977232 62777269 | 56579503 56479542 | 50581904 | 44984448 | 39687154 | 40 |
| ., | 62677306 | 56379581 | 50481945 50481986 | 44884492 44784535 | 39587201 39487247 | 13 |
| 18 | 62577343 | 56279620 | 50382027 | 44684579 | 39387294 | 12 |
| 19 | 62477380 62377417 | 56179659 56079698 | 50282069 | 44584623 | 39287341 | |
| ,,, | 62277454 | 55979737 | 50182110 50082151 | 44484667 44484711 | 39287387 39187434 | 11 |
| 20 | 62177491 | 55879777 | 49982193 | 44384755 | 39087481 | 10 |
| 21 | 62077528 | 55779816 | 49882234 | 44284799 | 38987528 | |
| 21 | 61977565 61877602 | 55679855 55579894 | 49782276 49682317 | 44184843 44084887 | 38887575 38787622 | 9 |
| 22 | 61777639 | 55479933 | 49582359 | 43984931 | 38787669 | 8 |
| 23 | 61677677 | 55379973 | 49482400 | 43884976 | 38687716 | |
| 23 | 61577714 61477751 | 55280012 55180051 | 49382442 49282484 | 43785020 43685064 | 38587764 38487811 | 7 |
| 24 | 61277788 | 55080091 | 49182526 | 43585109 | 38387858 | 6 |
| 25 | 61177826 | 54980130 | 49082567 | 43485153 | 38287906 | |
| 25 | 61077863 60977901 | 54880170 54780209 | 48982609 48882651 | 43485197 43385242 | 38187953 38188001 | 5 |
| 26 | 60877938 | 54680249 | 48782693 | 43285286 | 38088048 | 4 |
| | 60777976 | 54580288 | 48682735 | 43185331 | 37988096 | |
| 27 | 60678013 60578051 | 54480328 54380368 | 48582777 48482819 | 43085376 42985420 | 37888143 37788191 | 3 |
| 28 | 60478088 | 54280407 | 48382861 | 42885465 | 37688239 | 2 |
| | 60378126 | 54180447 | 48282903 | 42785510 | 37688286 | 1 |
| 29 | 60278164 60178201 | 54080487 53980527 | 48282945 48182987 | 42685555 42685599 | 37588334 37488382 | l ¹ |
| 30 | 60078239 | 53880567 | 48083030 | 42585644 | 37388430 | 0 |
| | А В | A B | A B | A B | A B | - |
| | 99°30' | 99°00, | 98°30' | | | |
| | 99 30 | 99 00' | 98 - 30' | 98 ⁰ 00' | 97 ⁰ 30' | |
| | • | | , ' | • | • | • |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 82 ⁰ 30' | 83°00' | 83°30' | 84 ⁰ 00' | 0 | 1 |
|----|----------------------|---------------------------------|----------------------|---------------------------------|----------------------------|--------------|
| | A B | A B | 83 30 A B | | 84 [°] 30' | |
| 0 | 37388430 | 32591411 | 28094614 | A B 238.698076 | A B 200.4101843 | 30 |
| 1 | 37288478 37188526 | 32491462 32391514 | 27994670 27994725 | 237.998137 237.298197 | 199.8101908 199.2101974 | 29 |
| 2 | 37188574 | 32391565 | 27894781 | 236.698257 | 198.6102040 | <u> </u> |
| 2 | 37088623 36988671 | 32291617 32191668 | 27794836 27694892 | 235.998318 235.398378 | 198.0102106 197.4102172 | 28 |
| 3 | 36888719 36788767 | 32091720 31991772 | 27694948 27595004 | 234.698439 233.998499 | 196.8102238 196.2102304 | 27 |
| 4 | 36688816 | 31991824 | 27495060 | 233.398560 | 195.6102371 | 26 |
| 5 | 36688864 36588913 | 31891876 31791928 | 27495116 27395172 | 232.698621 232.098682 | 195.0102437 194.4102504 | 25 |
| | 36488961 | 31691980 | 27295228 | 231.398743 | 193.8102570 | |
| 6 | 36389010 36289059 | 31692032 31592085 | 27195285 27195341 | 230.798804 230.098865 | 193.2102637 192.6102704 | 24 |
| 7 | 36289107 | 31492137 | 27095397 | 229.498926 | 192.0102771 | 23 |
| | 36189156 36089205 | 31392189 31392242 | 26995454 26995510 | 228.798988 228.199049 | 191.4102838 190.8102905 | 22 |
| | 35989254 | 31292294 | 26895567 | 227.499111 | 190.2102973 | 22 |
| 9 | 35889303 35789352 | 31192347 31092399 | 26795624 26795681 | 226.899172 226.199234 | 189.6103040 189.0103107 | 21 |
| 10 | 35789401 | 31092452 | 26695737 | 225.599296 | 188.4103175 | 20 |
| 11 | 35689450 35589499 | 30992505 30892558 | 26595795 26495851 | 224.899357 224.299419 | 187.8103243 187.2103311 | 19 |
| | 35489548 | 30792610 | 26495909 | 223.599482 | 186.7103379 | |
| 12 | 35389597 35389647 | 30792663 30692716 | 26395966 | 222.999544 | 186.1103447 | 18 |
| 13 | 35289696 | 30592769 | 26296023 26296080 | 222.399606 221.699668 | 185.5103515 184.9103583 | 17 |
| | 35189746 | 30492823 | 26196138 | 221.099731 | 184.3103651 | |
| 14 | 35089795 34989845 | 30492876 30392929 | 26096195 26096253 | 220.399793 219.799856 | 183.7103720 183.2103788 | 16 |
| 15 | 34989894 34889944 | 30292982 | 25996310 | 219.199918 | 182.6103857 | 15 |
| 16 | 34789994 | 30193036 30193089 | 25896368 25796426 | 218.499981 217.8100044 | 182.0103926 181.4103995 | 14 |
| | 34690044 | 30093143 | 25796484 | 217.2100107 | 180.8104064 | |
| 17 | 34590093 34590143 | 29993196 29893250 | 25696542 25596600 | 216.5100170 215.9100233 | 180.3104133 179.7104202 | 13 |
| 18 | 34490193 | 29893304 | 25596658 | 215.3100296 | 179.1104272 | 12 |
| 19 | 34390243 34290293 | 29793358 29693411 | 25496716 25396774 | 214.6100360 214.0100423 | 178.5104341 178.0104411 | 11 |
| | 34190344 | 29593465 | 25396833 | 213.4100487 | 177.4104480 | |
| 20 | 34190394 34090444 | 29593519 29493573 | 25296891 25196950 | 212.8100550 | 176.8104550 | 10 |
| 21 | 33990494 | 29393628 | 25197008 | 212.1100614 211.5100678 | 176.2104620 175.7104690 | 9 |
| | 33890545 | 29293682 | 25097067 | 210.9100742 | 175.1104760 | |
| 22 | 33790595 33790646 | 29293736 29193790 | 24997126 24997184 | 210.3100806 209.6100870 | 174.5104830 174.0104901 | 8 |
| 23 | 33690696 33590747 | 29093845 28993899 | 24897243 24797302 | 209.0100943 208.4100998 | 173.4104971 172.8105042 | 7 |
| 24 | 33490798 | 28993954 | 24797361 | 207.8101063 | 172.3105113 | 6 |
| 25 | 33390848 33390899 | 28894009 28794063 | 24697420 24597480 | 207.1101127 206.5101192 | 171.7105183 | _ |
| | 33290950 | 28794118 | 24597539 | 205.9101192 | 171.1105254 170.6105325 | 5 |
| 26 | 33191001 | 28694173 | 24497598 | 205.3101321 | 170.0105397 | 4 |
| 27 | 33091052 33091103 | 28594228 28494283 | 24397658 24397717 | 204.7101386 204.1101451 | 169.5105468 168.9105539 | 3 |
| | 32991154 | 28494338 | 24297777 | 203.5101516 | 168.4105611 | |
| 28 | 32891205 32791257 | 28394393 28294448 | 24197837 24197897 | 202.8101581 202.2101646 | 167.8105683 167.2105754 | 2 |
| 29 | 32691308 | 28194503 | 24097957 | 201.6101712 | 166.7105826 | 1 |
| | 32691359 | 28194559 | 23998017 | 201.0101777 | 166.0105898 | <u> </u> |
| 30 | 32591411 A B | 28094614 A B | 23998076 A B | 200.4101843 A B | 165.6105970 A B | - |
| | 97°00' | | | | | |
| | 97 00 | 96 ⁰ 30 [,] | 96°00' | 95 ⁰ 30 [,] | 95 ⁰ 00' | |

WHEN LHA (E OR W) IS GREATER THAN 90°, TAKE "K" FROM BOTTOM OF TABLE

| | 1 . | 1 | 1 | 1 . | 1 . | 1 |
|----|----------------------------|----------------------------|----------------------------|--------------------------|---------------------------|----------------|
| | 85 ⁰ 00' | 85 ⁰ 30' | 86°00' | 86 ₀ 30. | 87 ⁰ 00' | |
| | АВ | A B | A B | A B | A B | |
| 0 | 165.6105970 | 134.1110536 | 105.9115641 | 81.1121432 | 59.6128120 | 30 |
| 1 | 165.0106043 164.5106115 | 133.6110616 133.1110696 | 105.5115732 105.0115823 | 80.7121538 80.3121639 | 59.2128241 58.9128362 | 29 |
| | 163.9106187 | 132.6110777 | 104.6115913 | 79.9121743 | 58.6128483 | |
| 2 | 163.4106260 | 132.1110858 | 104.2116004 | 79.5121848 | 58.2128605 | 28 |
| 3 | 162.8106333 162.3106406 | 131.6110939 131.1111020 | 103.7116096 103.3116187 | 79.2121952 78.8122057 | 57.9128727 57.6128849 | 27 |
| | 161.7106479 | 130.6111101 | 102.9116278 | 78.4122161 | 57.3128972 | |
| 4 | 161.2106552 | 130.1111183 | 102.4116370 | 78.0122267 | 56.9129095 | 26 |
| 5 | 160.6106625 160.1106698 | 129.6111264 129.2111346 | 102.0116462 101.6116554 | 77.6122372 77.3122478 | 56.6129218 56.3129342 | 25 |
| | 159.6106772 | 128.7111428 | 101.1116647 | 76.9122584 | 56.0129466 | 1 -3 |
| 6 | 159.0106846 | 128.2111510 | 100.7116739 | 76.5122690 | 55.7129591 | 24 |
| 7 | 158.5106919 157.9106993 | 127.7111592 127.2111674 | 100.3116832 99.8116925 | 76.1122796 75.8122903 | 55.3129716 55.0 120941 | 22 |
| | 157.4107067 | 126.7111757 | 99.4117018 | 75.4123010 | 55.0129841 54.7129967 | 23 |
| 8 | 156.9107141 | 126.2111839 | 99.0117112 | 75.0123117 | 54.4130093 | 22 |
| 9 | 156.3107216 155.8107290 | 125.8111922 125.3112005 | 98.5117205 | 74.6123225 | 54.1130219 | 0.1 |
| 3 | 155.2107364 | 124.8112088 | 98.1117299 97.7117393 | 74.3123332 73.9123441 | 53.7130346 53.4130473 | 21 |
| 10 | 154.7107439 | 124.3112171 | 97.3117487 | 73.5123549 | 53.1130600 | 20 |
| 11 | 154.2107514 | 123.8112255 | 96.8117581 | 73.2123657 | 52.8130728 | |
| " | 153.6107589 153.1107664 | 123.4112338 122.9112422 | 96.4117676 96.0117771 | 72.8123766 72.4123875 | 52.5130856 52.2130985 | 19 |
| 12 | 152.6107739 | 122.4112506 | 95.6117866 | 72.1123985 | 51.9131114 | 18 |
| 40 | 152.1107814 | 121.9112590 | 95.2117961 | 71.7124095 | 51.6131243 | |
| 13 | 151.5107890 151.0107965 | 121.5112674 121.0112759 | 94.7118056 94.3118152 | 71.3124204 71.0124315 | 51.3131373 51.0131503 | 17 |
| 14 | 150.5108041 | 120.5112843 | 93.9118248 | 70.6124425 | 50.7131633 | 16 |
| 4- | 149.9108117 | 120.1112928 | 93.5118344 | 70.3124536 | 50.3131764 | |
| 15 | 149.4108183 148.9108269 | 119.6113013 119.1113098 | 93.1118440 92.7118537 | 69.9124647 69.5124759 | 50.0131896 49.7132027 | 15 |
| 16 | 148.4108345 | 118.7113183 | 92.3118633 | 69.2124870 | 49.4132159 | 14 |
| | 147.8108421 | 118.2113269 | 91.8118730 | 68.8124982 | 49.1132292 | l ' - |
| 17 | 147.3108498 146.8108574 | 117.7113354 117.3113440 | 91.4118827 91.0118925 | 68.5125094 68.1125207 | 48.8132425 48.5132558 | 13 |
| 18 | 146.3108651 | 116.8113526 | 90.6119022 | 67.8125320 | 48.2132692 | 12 |
| | 145.8108728 | 116.3113612 | 90.2119120 | 67.4125433 | 47.9132826 | l '- |
| 19 | 145.2108805 144.7108882 | 115.9113699 115.4113785 | 89.8119218 89.4119316 | 67.1125546 66.7125660 | 47.6132961 47.3133096 | 11 |
| 20 | 144.2108960 | 114.9113872 | 89.0119415 | 66.4125774 | 47.1133231 | 10 |
| | 143.7109037 | 114.5113958 | 88.6119513 | 66.0125888 | 46.8133367 | |
| 21 | 143.2109115 142.7109192 | 114.0114045 113.6114133 | 88.2119612 87.8119711 | 65.7126003 65.3126118 | 46.5133503 46.2133640 | 9 |
| 22 | 142.2109270 | 113.1114220 | 87.4119811 | 65.0126233 | 45.9133777 | 8 |
| | 141.6109348 | 112.7114307 | 87.0119910 | 64.6126349 | 45.6133914 | Ů |
| 23 | 141.1109426 140.6109505 | 112.2114395 111.7114483 | 86.6120010 86.2120110 | 64.3126465 63.9126581 | 45.3134052 45.0134191 | 7 |
| 24 | 140.1109583 | 111.3114571 | 85.8120211 | 63.6126697 | 44.7134330 | 6 |
| | 139.6109662 | 110.8114659 | 85.4120311 | 63.3126814 | 44.4134469 | Ů |
| 25 | 139.1109740 138.6109819 | 110.4114747 109.9114836 | 85.0120412 84.6120513 | 62.9126931 62.6127049 | 44.2134609 43.9134749 | 5 |
| 26 | 138.1109898 | 109.5114925 | 84.2120614 | 62.2127166 | 43.6134890 | 4 |
| | 137.6109978 | 109.0115014 | 83.8120715 | 61.9127284 | 43.3135031 | Ι " |
| 27 | 137.1110057 136.6110136 | 108.6115103 108.1115192 | 83.4120817 83.0120919 | 61.6127403 61.2127521 | 43.0135173 42.7135315 | 3 |
| 28 | 136.1110216 | 107.7115282 | 82.6121021 | 60.9127640 | | - |
| | 135.6110296 | 107.3115371 | 82.2121124 | 60.6127760 | 42.5135457 42.2135600 | 2 |
| 29 | 135.1110375 134.6110455 | 106.8115461 106.4115551 | 81.9121226 81.5 121329 | 60.2127880 | 41.9135744 | 1 |
| 30 | 134.1110536 | | 81.5121329 | 59.9128000 | 41.6135888 | _ |
| | A B | 105.9115641 A B | 81.1121432 A B | 59.6128120 A B | 41.4136032 | - 0 |
| | | | | | A B | |
| | 94 ⁰ 30' | 94 ⁰ 00' | 93°30' | 93 ₀ 00. | 92°30' | |
| , | • 1 | , 1 | ı . | · | l l | j |

ALWAYS TAKE "Z" FROM BOTTOM OF TABLE, EXCEPT WHEN "K" IS SAME NAME AND GREATER THAN LATITUDE, IN WHICH CASE TAKE "Z" FROM TOP OF TABLE

| | 87 [°] 30' | 88°00' | 88°30' | 89°00' | 89°30' | |
|----|--------------------------|--------------------------|--------------------------|-------------------------------------|------------------------|----------|
| | АВ | A B | А В | A B | A B | 1 |
| 0 | 41.4136032 41.1136177 | 26.5145718 26.2145899 | 14.9158208 14.7158450 | 6.6175814 6.5176178 | 1.7205916 1.6206646 | 30 |
| 1 | 40.8136322 40.5136468 | 26.0146081 25.8146264 | 14.6158693 14.4158938 | 6.4176544 6.3176914 | 1.5207388 1.5208143 | 29 |
| 2 | 40.3136615 40.0136761 | 25.6146448 25.4146632 | 14.2159184 14.1159431 | 6.2177287 6.1177663 | 1.4208912 1.4209695 | 28 |
| 3 | 39.7136909 | 25.2146817 | 13.9159680 | 6.0178042 | 1.3210491 | 27 |
| | 39.4137057 | 24.9147003 | 13.7159930 | 5.9178424 | 1.3211303 | _ |
| 4 | 39.2137205 38.9137354 | 24.7147190 24.5147377 | 13.6160182 13.4160435 | 5.8178810 5.7179200 | 1.2212130 1.2212974 | 26 |
| 5 | 38.6137503 38.4137653 | 24.3147566 24.1147755 | 13.3160690 13.1160946 | 5.6179593 5.5179990 | 1.1213834 | 25 |
| 6 | 38.1137804 | 23.9147945 | 13.0161204 | 5.4180390 | 1.1214711 | 24 |
| | 37.8137955 | 23.7148135 | 12.8161463 | 5.3180794 | 1.0216521 | |
| 7 | 37.6138106 37.3138258 | 23.5148327 23.3148520 | 12.7161724 12.5161986 | 5.2181201 5.1181613 | 1.0217455 0.9218409 | 23 |
| 8 | 37.1138411 | 23.1148713 | 12.4162250 | 5.0182029 | 0.9219385 | 22 |
| 9 | 36.8138564 36.5138718 | 22.8148907 22.6149103 | 12.2162516 12.1162783 | 4.9182448 4.8182872 | 0.9220384 0.8221406 | 21 |
| | 36.3138872 | 22.4149299 | 11.9163052 | 4.7183300 | 0.8222452 | |
| 10 | 36.0139027 | 22.2149495 | 11.8163322 | 4.6183732 | 0.7223525 | 20 |
| 11 | 35.8139182 35.5139338 | 22.0149693 21.8149892 | 11.6163594 11.5163868 | 4.5184168 4.4184609 | 0.7224624 0.7225752 | 19 |
| | 35.3139494 | 21.6150092 | 11.3164144 | 4.3185055 | 0.6226910 | |
| 12 | 35.0139651 34.7139809 | 21.4150292 21.2150494 | 11.2164422 11.0164701 | 4.2185505 4.1185959 | 0.6228100 0.6229324 | 18 |
| 13 | 34.5139967 | 21.0150696 | 10.9164982 | 4.1186419 | 0.5230583 | 17 |
| | 34.2140125 34.0140285 | 20.8150899 | 10.8165265 | 4.0186883 | 0.5231879 | |
| 14 | 34.0140285 33.7140445 | 20.6151104 20.5151309 | 10.6165550 10.5165836 | 3.9187353 3.8187827 | 0.5233215 0.4234594 | 16 |
| 15 | 33.5140605 33.2140766 | 20.3151515 20.1151722 | 10.3166125 10.2166415 | 3.7188307 3.6188793 | 0.4236018 0.4237491 | 15 |
| 16 | 33.0140928 | 19.9151931 | 10.1166708 | 3.6189283 | 0.4239015 | 14 |
| 17 | 32.8141090 32.5141253 | 19.7152140 19.5152350 | 9.9167002 9.8167298 | 3.5189780 3.4190282 | 0.3240594 0.3242233 | |
| ., | 32.3141417 | 19.3152561 | 9.7167597 | 3.3190790 | 0.3242233 | 13 |
| 18 | 32.0141581 | 19.1152774 | 9.5167897 | 3.2191303 | 0.3245709 | 12 |
| 19 | 31.8141745 31.5141911 | 18.9152987 18.7153201 | 9.4168200 9.3168505 | 3.2191824 3.1192350 | 0.2247558 0.2249488 | 11 |
| | 31.3142077 | 18.6153417 | 9.1168811 | 3.0192883 | 0.2251508 | |
| 20 | 31.1142243 30.8142411 | 18.4153633 18.2153851 | 9.0169121 8.9169432 | 2.9193422 2.91939 6 9 | 0.2253627 0.2255855 | 10 |
| 21 | 30.6142579 | 18.0154070 | 8.7169745 | 2.8194522 | 0.1258203 | 9 |
| | 30.4142747 | 17.8154290 | 8.6170061 | 2.7195082 | 0.1260685 | |
| 22 | 30.1142916 29.9143086 | 17.6154511 17.5154733 | 8.5170379 8.4170700 | 2.7195650 2.6196225 | 0.1263318 0.1266121 | 8 |
| 23 | 29.6143257 29.4143428 | 17.3154956 17.1155180 | 8.2171023 8.1171348 | 2.5196808 2.4197399 | 0.1269118 0.1272336 | 7 |
| 24 | 29.2143600 | 16.9155406 | 8.0171676 | 2.4197998 | 0.1275812 | 6 |
| | 28.9143773 | 16.8155633 | 7.9172006 | 2.3198605 | 0.1279591 | |
| 25 | 28.7143946 28.5144120 | 16.6155861 16.4156090 | 7.8172339 7.6172674 | 2.3199221 2.2199846 | 0.0283730 0.0288306 | 5 |
| 26 | 28.3144295 | 16.2156320 | 7.5173012 | 2.1200480 | 0.0293421 | 4 |
| 27 | 28.0144470 27.8144646 | 16.1156552 15.9156784 | 7.4173352 7.3173696 | 2.1201124 2.0201777 | 0.0299221 0.0305915 | 3 |
| | 27.6144823 | 15.7157019 | 7.2174042 | 1.9202440 | 0.0313833 | L |
| 28 | 27.4145000 27.1145179 | 15.6157254 15.4157490 | 7.1174391 6.9174742 | 1.9203113 | 0.0323524 | 2 |
| 29 | 26.9145358 | 15.4157490 15.2157728 | 6.9174742 6.8175097 | 1.8203797 1.8204492 | 0.0336018 0.0353627 | , |
| | 26.7145538 | 15.1157967 | 6.7175454 | 1.7205198 | 0.0383730 | |
| 30 | 26.5145718 A B | 14.9158208 | 6.6175814 | 1.7205916 | 0.0 | <u> </u> |
| | | A B | A B | A B | A B | ł |
| , | 92 [°] 00′ | 91 [°] 30′ | 91 [°] 00′ | 90 ₀ 30, | 80 ₀ 00₁ | |

GLOSSARY

a' prime (used to indicate a variable under different situations)

ACR armored cavalry regiment amplitude modulated approx approximately

ARDF airborne radio direction finding

b" double prime (continuation of the variable)

bearing The angular measurement in degrees from north (true, magnetic, or grid) of an arriving radio wave

with relation to the DF site.

BM bearing mean
BO bearing observed
BPE best point estimate
BT bearing true

c certain

CADF commutated-antenna direction finder

CCR corrected compass rose

CDAA circularly disposed antenna array

CEP circular error probability collection and jamming

c o company **Col** column

COMSEC communications security

Cos cosecants/cosine cot cotangent CRT cathode ray tube

cut The point of intersection of two DF lines of bearing.

CW continuous wave

D doubtful

DA Department of the Army direction finding difference division

DWDF direct wave direction finding

E east

E field electrical field
EAC echelons above corps
EEP elliptical error probability

EF SSL term

EHF extremely high frequency

EL The elevation angle of arriving signal measured from the horizontal plane of the earth.

EM electromagnetic EW electronic warfare FE SSL term FEF SSL term

fix The most probable location of a target transmitter's antenna when three or more DF lines of bearing

have been plotted on a chart or map.

flash A high priority message from NCS to the DF sites. The message, usually sent on a restricted radio

circuit, provides the basic target information and requested DF support.

FLOT forward line of own troops

F M field manual; frequency modulated

FORTRAN formula translation

freq frequency

GCAD great circle azimuth and distance

GHz gigahertz **GN** grid north

GPS global positioning system

h height

h' Virtual height of the ionospheric layer (where the target signal is reflected) from the surface of the

earth. (H prime)

H field magnetic field high frequency

Hz hertz

IEWSE intelligence and electronic warfare support element United States Army Intelligence and Security Command

I R information requirements

kHz kilohertz km kilometer(s)

L or LAT latitude

LCSS lightweight camouflage screen system

LF low frequency
LOB line of bearing(s)
log logarithm
long longitude
LOP line of position
LOS line of sight

maint maintenance

MBG mean bearing grouping

METT-T mission, enemy, terrain, troops and time available

MF medium frequency

MHz megahertz

MI military intelligence

minute A subdivision of angular measure. One degree equals sixty minutes.

MOS military occupational specialty

MRDFS man-transportable radio direct ion finding system

N north seeking; north

NADF narrow aperture direction finding

NCS net control station Nm nautical miles

NSA National Security Agency

NSACSS National Security Agency/Central Security Service

OB order of battle

OIS oblique incidence sounder

op operator

PIR priority intelligence requirements

plot The placing of DF bearings on a chart or map so that a target's location can be determined by

reference to grid or geographic coordinates. Also called plotting.

POL petroleum, oils and lubricants

QUMP quasi uni-modal propagation

RDF radio direction finding

RF radio frequency; radiated frequency

s south

S3 Operations and Training Officer (US Army)

SD standard deviation
SE systematic error
SF Special Forces
SHF super high frequency
SIGINT signals intelligence

sin sine

Sm statute miles

SOP standing operating procedures

SSB single side band SSL single station locator STP soldier training publication SWDF sky wave direction finding

TA traffic analysis tan tangent

TC training circular

TCAE technical control and analysis element time-difference direction finders
TEC Training Extension Course

tip-off A message, usually initiated by an intercept position, requesting DF action on selected

transmitter(s). A tip-off will include, as a minimum, the target activity and frequency and any

identifying call signs.

TM technical manual TN true north

TOC tactical operations center

FM 34-40-9

TO&E table of organization and equipment

tracking Real-time identification of the target activity to ensure that the DF sites acquire the correct target.

Tracking is usually performed by the NCS on the flash circuit.

TRADOC United States Army Training and Doctrine Command

UHF ultra high frequency United States

USA United States of America

USAISD United States Army Intelligence School, Fort Devens

USSID United States Signals Intelligence Directive

UTM universal transverse mercator

VHF very high frequency
VIS vertical incidence sounder
VLF very low frequency

W west

WADF wide aperture direction finding

WFA wavefront analysis
WFT wavefront testing
WWII World War II

∠ angle (geometric symbol)

o degrees (1 degree equals 60 minutes)

minutes (1 minute equals 60 seconds)

" seconds

≤ summation operator for calculus

o variance

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